

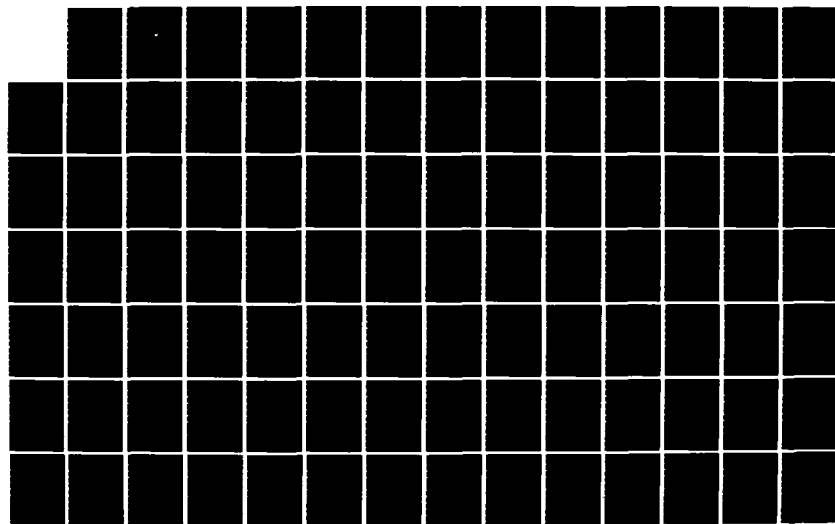
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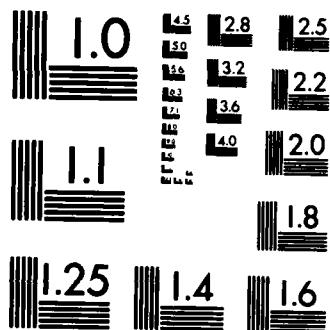
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Monterey, California



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## THESIS

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MASK:  
A TACTICAL AID FOR PLANNING AIR STRIKES  
AGAINST RADAR DEFENDED LAND TARGETS

by

Dana Bruce McKinney

September 1983

Thesis Advisor:

A. F. Andrus

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REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER	2. GOVT ACCESSION NO. AD A136771	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) MASK: A Tactical Aid for Planning Air Strikes Against Radar Defended Land Targets		5. TYPE OF REPORT & PERIOD COVERED Master's Thesis September 1983
7. AUTHOR(s) Dana Bruce McKinney		6. PERFORMING ORG. REPORT NUMBER
9. PERFORMING ORGANIZATION NAME AND ADDRESS Naval Postgraduate School Monterey, California 93943		8. CONTRACT OR GRANT NUMBER(s)
11. CONTROLLING OFFICE NAME AND ADDRESS Naval Postgraduate School Monterey, California 93943		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		12. REPORT DATE September 1983
		13. NUMBER OF PAGES 181
		15. SECURITY CLASS. (of this report)
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		Accession For NTIS GRAFT <input checked="" type="checkbox"/> DTIC TAB <input type="checkbox"/> Unannounced <input type="checkbox"/> Justification
18. SUPPLEMENTARY NOTES		By Distribution/ Availability Codes Avail and/or Dist Special
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) DTED Radar Coverage Terrain Masking Strike Warfare Mission Planning Digital Terrain Data Base		A-1
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This thesis presents an interactive computer program called MASK which generates radar and optical line-of-sight coverage envelopes based on terrain masking and refractive propagation effects. MASK is designed primarily as an aid in planning air strikes against radar defended land targets and has additional applications to air defense network planning. A large digital terrain data base provides extensive coverage of potential areas of interest to the tactical planner.		

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A Tactical Aid for Planning Air Strikes  
Against Radar Defended Land Targets

by

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Commander, United States Navy  
B.A., University of California, Berkeley, 1969

Submitted in partial fulfillment of the  
requirements for the degree of

MASTER OF SCIENCE IN OPERATIONS RESEARCH

from the

NAVAL POSTGRADUATE SCHOOL  
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## ABSTRACT

This thesis presents an interactive computer program called MASK which generates radar and optical line-of-sight coverage envelopes based on terrain masking and refractive propagation effects. MASK is designed primarily as an aid in planning air strikes against radar defended land targets and has additional applications to air defense network planning. A large digital terrain data base provides extensive coverage of potential areas of interest to the tactical planner.

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## I. INTRODUCTION

### A. HISTORICAL PERSPECTIVE

In the last decade, tactical planners have witnessed a revolution in the development and deployment of air defense systems. The increasing number and effectiveness of the weapons introduced into the inventories of potential adversaries have greatly complicated the task of today's tactical strike planner. The primary objective of timely delivery of ordnance on target has been increasingly challenged by the ability of an adversary to impose an unacceptably high attrition rate on the attacking forces. The deployment of modern air defense systems in some areas of the third world has contributed to instability by calling into question the ability of the Carrier Battle Group to project power ashore.

Due to the risk involved in directly engaging a modern air defense network, additional emphasis has been placed on methods of reducing the amount of time that attacking aircraft must spend in the threat weapon envelope. These methods generally include the use of stand-off weapons, electronic countermeasures and low altitude penetration tactics. The success of low altitude penetration tactics rests on the ability of the attacking force to use terrain masking to delay initial detection and thereby reduce the time for the defense to effectively react. Effective employment of terrain masking is a concept which is likely to play an important role in future strike planning regardless of the air defense threat.

The increasing threat to our strike forces has spurred the development of more effective methods of neutralizing enemy defenses. Attacking aircraft



have more capable weapon systems, electronic warfare support has increased and real-time intelligence and surveillance capabilities have improved. However, our ability to accurately and rapidly assess the effect of terrain on the strength of enemy defenses has not progressed. This shortcoming limits the ability of the planner to employ his assets to the maximum advantage. This is especially true in situations requiring a quick reaction to a present threat. In such a situation, the tactical planner is forced to make extremely important decisions based on a gross estimation of the effects of terrain masking. The current state of the art is limited to the use of aeronautical or topographic charts to get an estimation of the threat system coverage envelope. Lines of sight, if plotted, are manually computed and based on the most rudimentary calculations. In short, the process is tedious, time consuming and inadequate. The importance of an accurate estimation of the enemy defensive coverage cannot be overstated. This information will ultimately determine the mission profile of the entire strike including cruising altitudes, routes of flight, low altitude penetration descent points, electronic countermeasures employment, fuel requirements and carrier aircraft launch position. In the absence of better information, the planner often assumes "worst case" conditions and limits the aggressive employment of his assets. Overly optimistic assumptions have more serious consequences.

#### B. RECENT DEVELOPMENTS

The need to upgrade tactical planning capabilities has been recognized by the fleet. The introduction of the Integrated Refractive Effects Prediction System (IREPS) into the fleet was a major step in improving the tactical planning process, especially in the War-at-Sea scenario. IREPS provided a real-time onboard capability to predict radar coverage and propagation anomalies

caused by the atmosphere. In particular, identification of the effect of surface based ducting on low altitude radar effectiveness was of great tactical importance. In many situations it became apparent that the selection of extremely low altitude attack profiles increased, rather than decreased, detection ranges against attack aircraft over water. The potential of IREPS and the nearly simultaneous development of a program by the Defense Mapping Agency Aerospace Center (DMAAC) to produce a world-wide Digital Terrain Elevation Data (DTED) base led logically to an idea called the Radar Detection Analysis System (RDAS). RDAS was put forth as an operational requirement from the fleet in June 1981 and envisioned a system incorporating the capabilities of IREPS, the data resources of the DTED and radar order-of-battle information supplied by already existing intelligence sources. Although several candidate systems have been developed to date, the fleet is still without the capabilities described in RDAS. At present, the most promising system is the Computer Aided Mission Planning System (CAMPS). Current information is that some CAMPS units are included in POM 85, but it is not possible to forecast the point at which this crucial capability will become operational throughout the fleet.

One final development should be mentioned. This is the impressive growth in computing power afforded by the introduction of the modern "desktop" computer. Units scheduled for near term fleet introduction, such as the Hewlett-Packard HP 9000, have a vastly greater capability for executing complex programs than did their immediate predecessors. In light of this imminent leap in shipboard computing power, it is now feasible to develop sophisticated computer programs for future fleet use.

### C. THESIS OBJECTIVE

The objective of this thesis is to develop a computer program to provide a shipboard terrain masking prediction capability pending the introduction of systems such as CAMPS. The program, MASK, incorporates terrain masking calculations based on DTED and includes anomalous propagation effects based on data derived from IREPS outputs. The design of MASK will allow it to be easily modified to run on systems such as the HP 9000 which have a baseline 500 KBYTE core memory and the ability to run a FORTRAN program using the UNIX operating system. MASK is currently running on the IBM 3033 using FORTRAN IV and the CMS operating system.

It is worth pointing out at this time that MASK is not a radar range prediction device. Radar detection range determination is dependent on many variables, some of which are time and route dependent (radar cross section as a function of relative aspect angle) or are dependent on operator fatigue or alertment. MASK is a deterministic model which calculates the ability of a given threat to have a clear line-of-sight in the direction of a target at a given altitude and range under specified atmospheric conditions. A predetermined flight path is neither required nor desired for MASK to carry out its calculations. The output from MASK graphically shows the vulnerable areas in the enemy defense network. Identification of these areas forms the basis upon which the rest of the planning evolution must ultimately rest.

### D. APPLICATIONS

The primary application of MASK is in air strike planning. A brief examination of the MASK output will reveal any areas of inadequate enemy radar coverage. By choosing routes of flight which take advantage of these areas, the planner will increase the survivability and effectiveness

of his attacking aircraft. MASK will allow attacking forces to choose descent points so as to take advantage of efficient cruising altitudes for as long as possible, descending only when required to remain "unseen". Preflight coordination of jamming and anti-radiation missile assets will also be enhanced by having a more realistic idea of the radar envelope, rather than just a circle of coverage centered on the victim radar.

A change of viewpoint leads to MASK's application to improving the air defense posture of friendly forces. MASK will allow the air defense network planner to easily assess his area coverage and to relocate or add assets to fill any voids. In the amphibious assault scenario, MASK will permit the planner to survey potential defensive missile battery locations prior to landing and allow rapid deployment of an air defense perimeter "tailor-made" for the local terrain. The time saved in setting up an organic land-based air defense system will mean that supporting missile ships can leave the landing area sooner, decreasing their vulnerability to attack and increasing overall tactical flexibility.

## II. PROBLEM STATEMENT

### A. GENERAL

The central problem in the terrain masking calculation is to define the position of an observer (the radar) and a candidate point and then to ask the question, "Is there any part of the earth's surface which interrupts the line of sight between the two?". Once this question is answered, an adjacent candidate point is chosen and the question is repeated and so on. Eventually, all candidate points are investigated and all those points for which the answer is "yes" form the set of masked points. All other points are unmasked and the boundary between the two sets defines the terrain masking envelope.

It should be understood that this model is not designed to include propagation loss factors or radar maximum detection range limits. The only range limit imposed which is not related to terrain masking is the maximum unambiguous range as a function of pulse repetition frequency (PRF).

### B. OBSERVER POSITION

The first consideration is to define the position of the observer. In this case the observer is a radar site with a known geographic location in terms of latitude, longitude and elevation. The observer's latitude and longitude are defined in terms of position (I,J) in a square matrix and the observer's elevation is the value of that matrix element. The observer will then be located at or above the matrix element (I,J) depending on the local terrain elevation value. For simplicity in this

discussion it is assumed that when locating an observer in the matrix, all observers are well behaved and only exist in the real world at the exact location where a matrix element exists in the model. In practice, allowances must be made for perverse observers who violate this assumption.

### C. PLANE EARTH LINE-OF-SIGHT

Given an observer location and the location of a candidate point (CP) above matrix element (M,N), the line-of-sight can be defined. In a simple world, line-of-sight would be a straight line between the observer and the CP. The real world is not so simple, but for now it is assumed that the earth's surface is a plane and that it exists in a vacuum. This allows the curvature of the earth and the effects of atmospheric refraction on the propagation of radar and light waves to be ignored. In this initial model the line-of-sight between the observer and the CP can be defined by two values. The first value, which is called horizontal slope (SH), is the geometric slope of the line from (I,J) to (M,N). Determination of the horizontal slope is shown in Figure 2.1. The second value, which is called vertical slope (SV), is the angular (radian) measure of the "look up" or "look down" when the observer points at the CP. For example, if the observer were located in a valley and the CP were on a hill SV would be positive. If the observer and CP exchanged places SV would be negative, and if they were at the same elevation SV would equal zero. Determination of the vertical slope is shown in Figure 2.2.

### D. OBSTRUCTIONS

Having defined line-of-sight, the location of any obstructions between the observer and the CP must be determined. One method of accomplishing

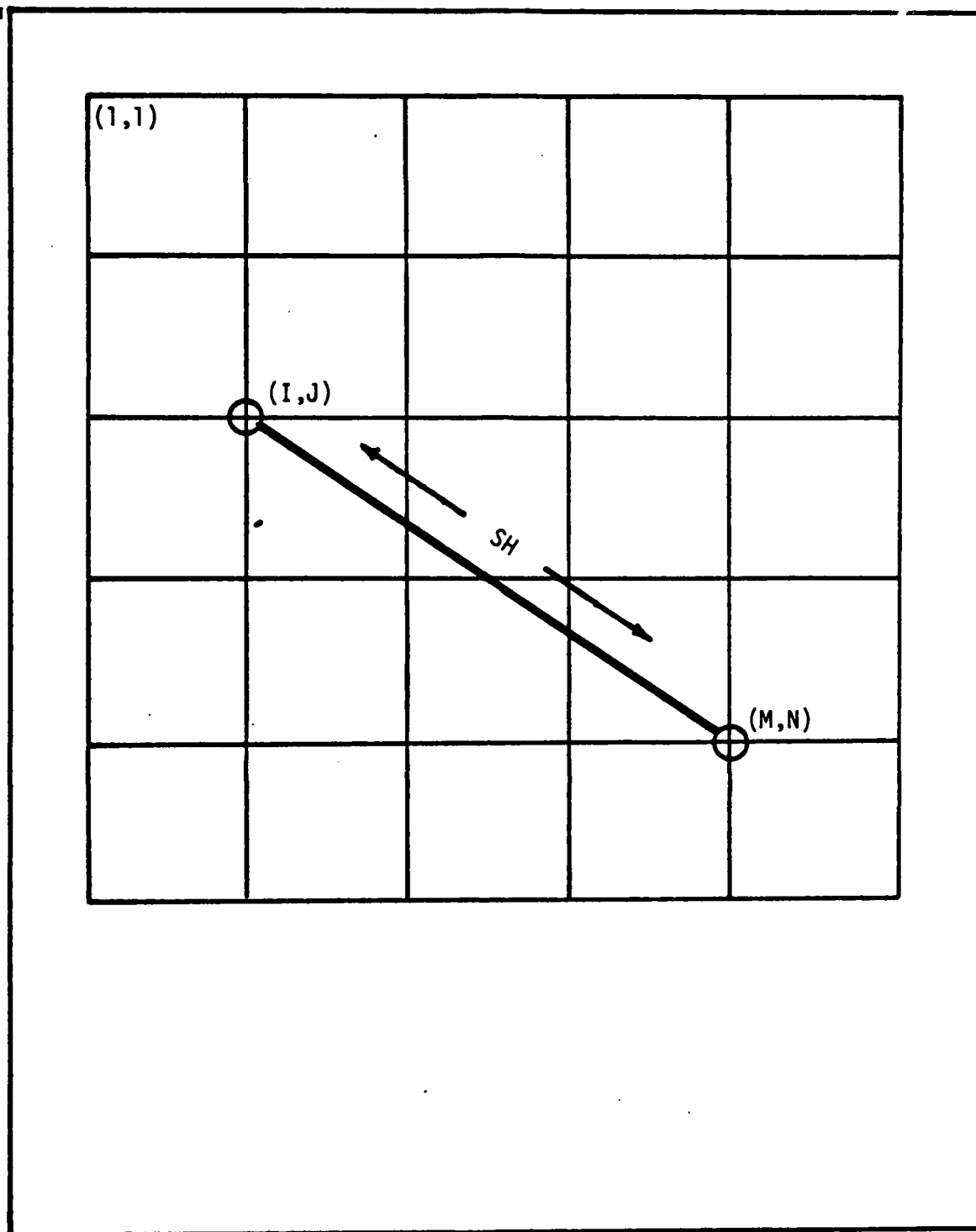


Figure 2.1 Determination of Horizontal Slope

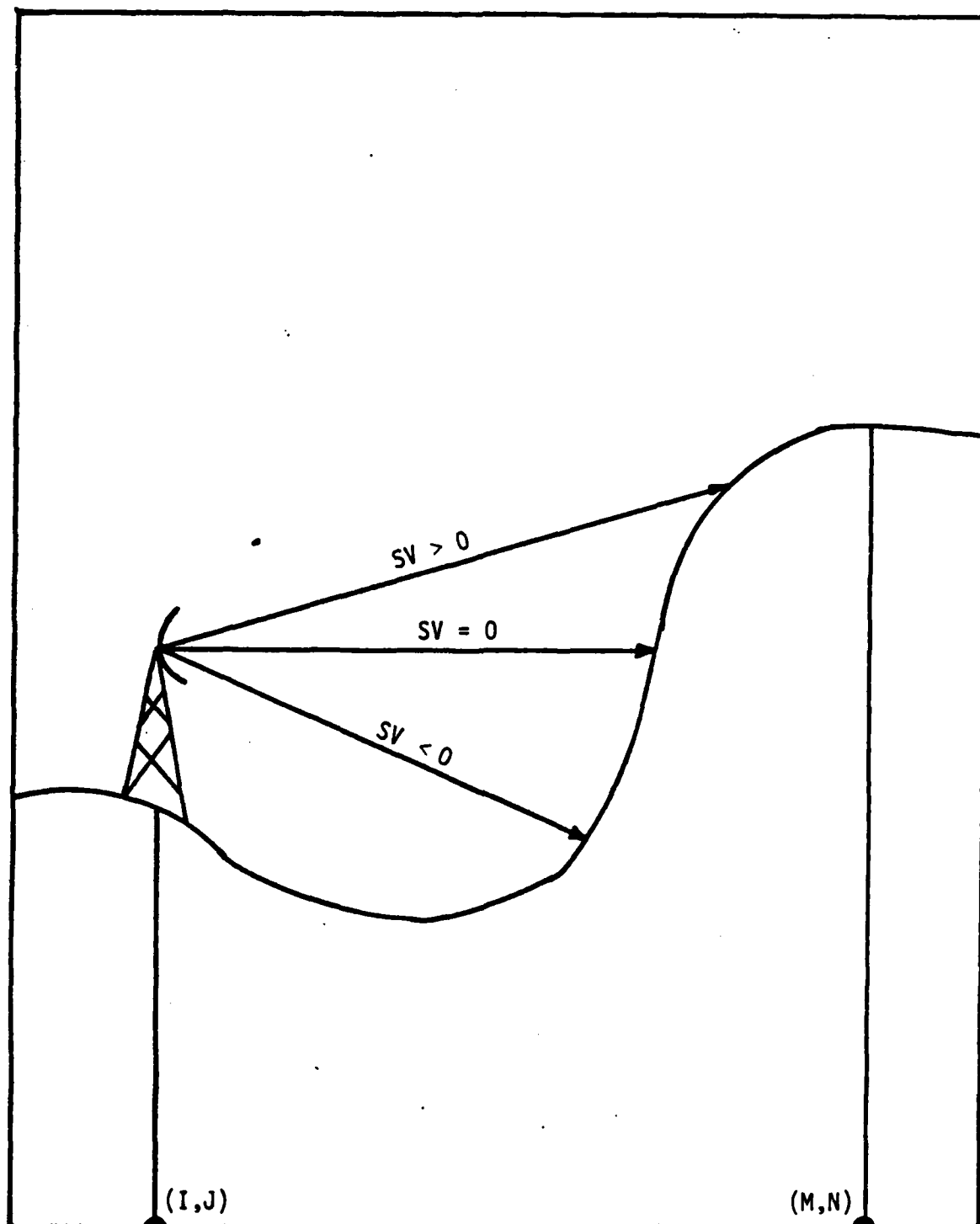


Figure 2.2 Vertical Slope Determination



this is to travel along the line from (M,N) to (I,J), sampling matrix elevation values to determine the SV at each sampling point (X,Y). As sampling progresses, only the largest (i.e., most positive) angle is saved. The largest value of SV for all sample points along the line is called the maximum vertical slope angle (MAXV) and is the elevation angle from the observer to the top of the (apparently) tallest object on the line from (I,J) to (M,N). This is illustrated in Figure 2.3. If a line is extended outward from the observer with elevation angle MAXV it will pass over (M,N) at some height above the plane of the matrix. This "masking height" is then compared with the specified height of a given target above (M,N). If the target height is below the masking height the target is masked by terrain. Otherwise, the target is visible to the observer. Once the condition of a target above (M,N) is determined, an adjacent element is chosen as the next CP. This process is duplicated for each matrix element.

#### E. EXTENSION TO SPHERICAL MODEL

Now that the problem has been defined in the simple case, two major complications must be introduced to provide a realistic model.

##### 1. Refractive Effects

The first complication is the phenomenon of the refraction of radar (and to a lesser extent, light) waves by the atmosphere. The result of refraction is that waves in the atmosphere tend to follow propagation paths which are curved rather than straight lines. The magnitude and direction of path curvature is determined by the rate of change with respect to height of the refractive index of the atmosphere ( $dn/dh$ ). The index of refraction,  $n$ , is a function of pressure, temperature and humidity and, in

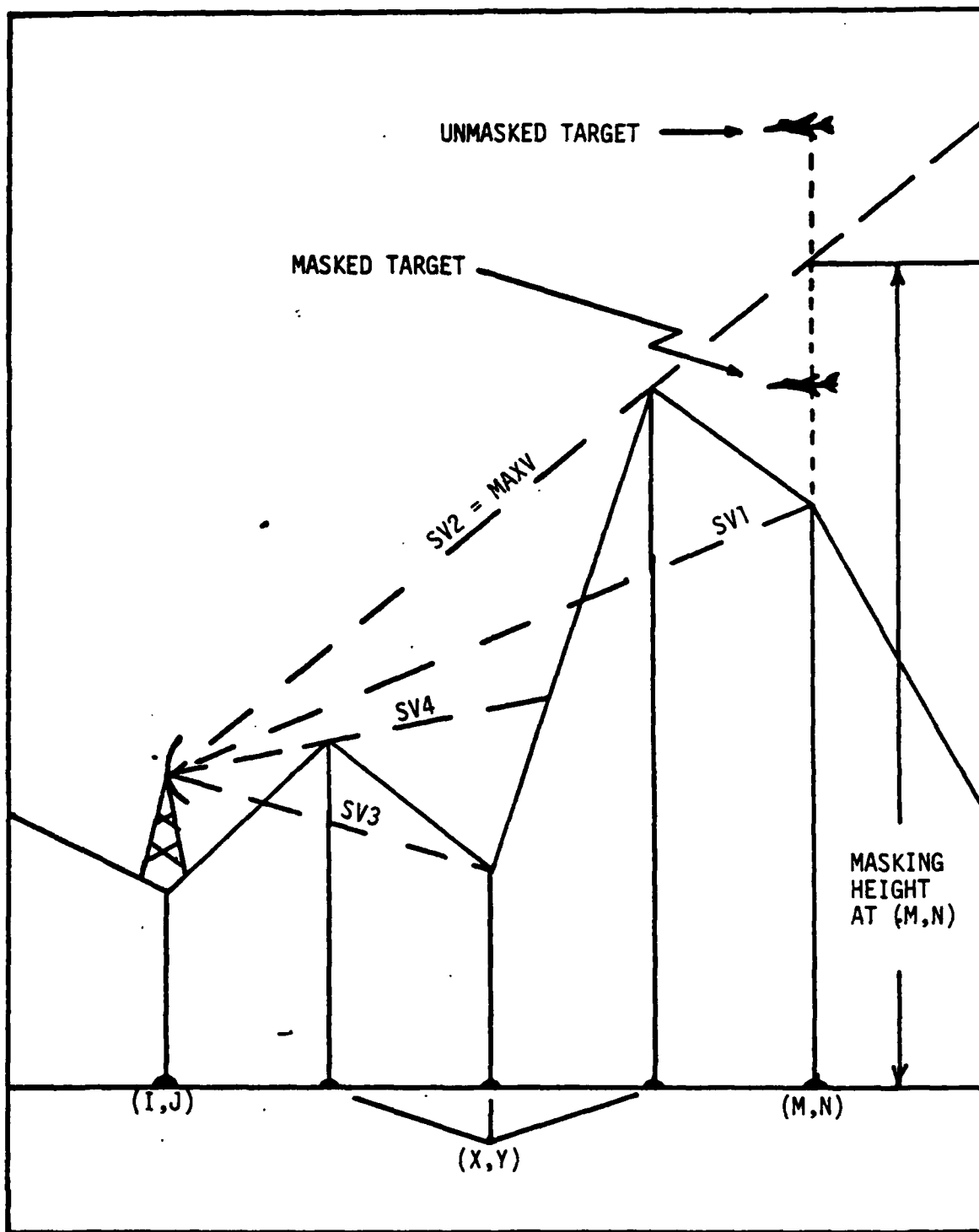


Figure 2.3 Masking Height Determination

most cases, is a decreasing function with respect to height. By using Snell's Law it can be shown that the radius of curvature,  $R$ , of the refracted wave path is given by equation 2.1.

$$R = -1/(dn/dh) \quad (\text{eqn. 2.1})$$

The derivation may be found in [Ref. 1: p 48]. For standard values of  $dn/dh$  (approximately  $-0.0000392$  per kilometer),  $R$  has a value of 25510 kilometers or about four times the radius of the earth. This results in radar waves propagating along paths which usually curve in the same direction as the curvature of the earth's surface, but which do not intersect it.

Certain atmospheric conditions generate values of  $dn/dh$  which can produce anomalous propagation paths. In extreme cases,  $R$  takes on values which are less than the earth's radius, causing the waves to curve back and intersect the surface. The wave is then partially reflected back into the atmosphere and continues in this way to "skip" along the surface of the earth for long distances. This effect is called ducting and can result in greatly extended radar ranges, especially over water. In less extreme cases, the ray paths may have greater than normal curvature but fail to return to earth. This condition, called superrefraction, can still produce over-the-horizon radar ranges. A value of  $dn/dh$  equal to zero equates to a radius of curvature which is infinite, producing straight line propagation and positive values of  $dn/dh$  actually yield ray paths which curve away from the earth. This latter condition is called subrefraction and is very rare.

For convenience the term,  $N$ , has been used to equal  $(n-1) \times 1,000,000$ . For example, the use of this transformation gives a value for  $dN/dh$  of  $-39.2$  'N' units' per kilometer of altitude on a standard day.

Figure 2.4 shows a graphic representation of the types of refractive effects discussed and a table relating  $dn/dh$  to the refractive types.

It should be obvious from this discussion that refractive effects must be accounted for in terrain masking calculations due to their influence on the curvature of the line-of-sight.

## 2. Earth Curvature

The second complication is that the earth's surface is not a plane. It has a complex elliptical shape which can be approximated in this application by a sphere with a radius equal to roughly 6370 kilometers. The resulting curvature causes the apparent line-of-sight (as viewed from a "plane earth" perspective) to bend away from the surface. As a result, the use of a spherical earth model profoundly affects the determination of the elevation angle, MAXV.

The introduction of refraction and earth's curvature naturally complicates the problem at hand. While the simpler model involved straight line ray propagation over a plane, the more complex one deals with curvilinear propagation over a spherical surface. Fortunately, there is a method of combining these two problems and obtaining a simplified equivalent one. The derivation of this method is not presented here, but the end result will be used (for the complete derivation, see [Ref. 1: pp 45-48]). The method allows plotting the line-of-sight as a straight line provided a larger "equivalent radius" is used in place of the actual earth radius. This is illustrated in Figure 2.5. This method also assumes that the atmosphere is homogeneous with a constant value of  $dn/dh$ . The equivalent radius,  $R_E$ , is given by equation 2.2,

$$R_E = a / (1 + (a \times (dn/dh))), \quad (\text{eqn. 2.2})$$

where  $a$  is the actual earth radius. This equation allows the use of  $dn/dh$  to arrive at an equivalent earth radius which accounts for both refractive

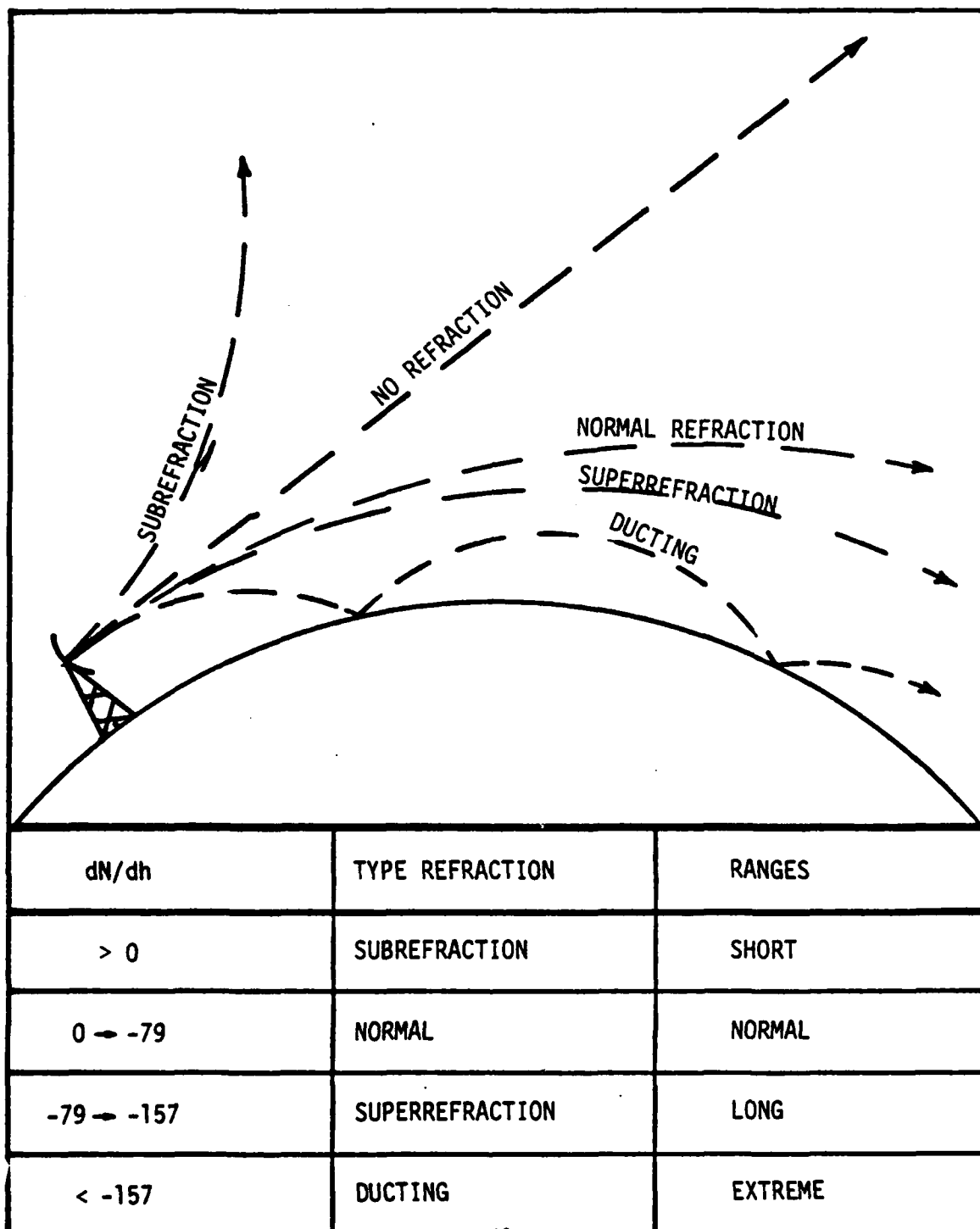


Figure 2.4 Refractive Propagation Paths

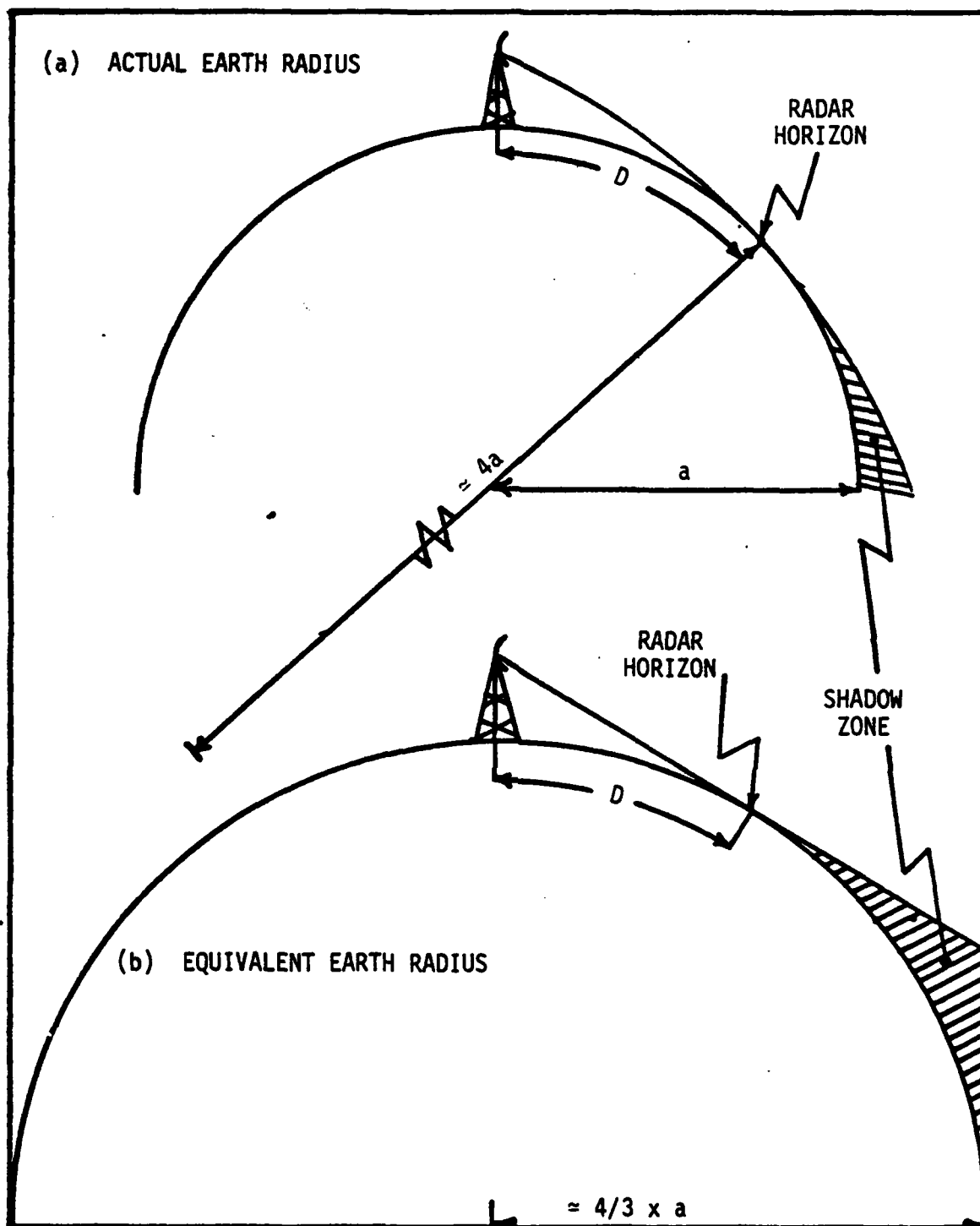


Figure 2.5 Actual and Equivalent Earth Comparison

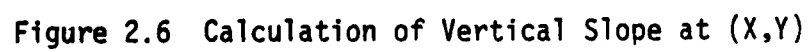
and earth curvature effects and which leads to a convenient way of modifying the flat earth model.

### 3. Spherical to Planar Transformation

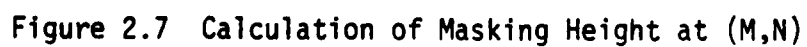
The use of equivalent earth radius provides a means of accounting for the effects of refraction and earth curvature at the same time. However, it introduces the problem of dealing with a spherical earth's surface. As a result, determination of the angle, SV, is made more difficult than in the flat earth model. One way to retain the benefits of the equivalent earth radius model and still deal in planar coordinates is to transform the spherical surface into an equivalent plane while preserving the angular relationships. During the following discussion, it will be helpful to refer to Figure 2.6.

The transformation to planar coordinates essentially involves a reduction in the height of the radar antenna ( $h_1$ ) and the sample terrain height ( $h_2$ ) above  $(X,Y)$ , as well as increasing the distance between  $(I,J)$  and  $(X,Y)$ . The cosine of ALPHA yields the reduced heights,  $h_1'$  and  $h_2'$ , while the sine of ALPHA leads to the calculation of the increased distance,  $D'$ , between  $(I,J)'$  and  $(X,Y)'$ . The signed difference between  $h_2'$  and  $h_1'$  is then divided by  $D'$  and the arctangent of the result is the angle SV. The angle  $SV'$  is obtained by adding  $\pi/2$  to SV and subtracting ALPHA.  $SV'$  is the radian measure of the elevation of the line of sight between the radar antenna, A, and the obscuring terrain, O, relative to the vertical line from  $(I,J)$  to the earth's center, C. The determination of MAXV is performed just as in the flat earth model except that the maximum value of  $SV'$  is retained as the sampling proceeds from  $(M,N)$  to  $(I,J)$ .

At this point all of the information required to determine the masking height, MHM, above  $(M,N)$  is available. Figure 2.7 shows the pertinent relationships. MAXV has already been found, and BETA is calculated







by dividing  $D$ , the ground distance from  $(I,J)$  to  $(M,N)$ , by the equivalent radius,  $RE$ .  $GAMMA$  is obtained by inspection and the Law of Sines is applied to the side  $AC$  to obtain the length of  $BC$ . The comparison of  $MHM$  is performed as in the flat earth model and the masking indicator variable is saved for later display.

The process described above is systematically applied to the entire matrix, producing the masking envelope for the first observer. The sequence is then repeated for each additional observer located in the matrix. Figure 2.8 shows a simplified flow chart of the required steps in the masking calculation process.

#### 4. Reflection

A final point should be mentioned in passing. In radar propagation models for shipboard systems one of the primary concerns is the modification of the received signal energy due to reflection from the sea surface. This effect is primarily caused by constructive and destructive interference resulting from phase differences in the received signal at the antenna. This interference causes the formation of lobes of increased and decreased detection ranges and can significantly affect the performance of shipboard weapon systems. However, since this model is primarily concerned with landbased systems, reflective effects have been ignored. Overwater propagation effects, including reflection, have been treated extensively in the IREPS model which is already widely deployed.

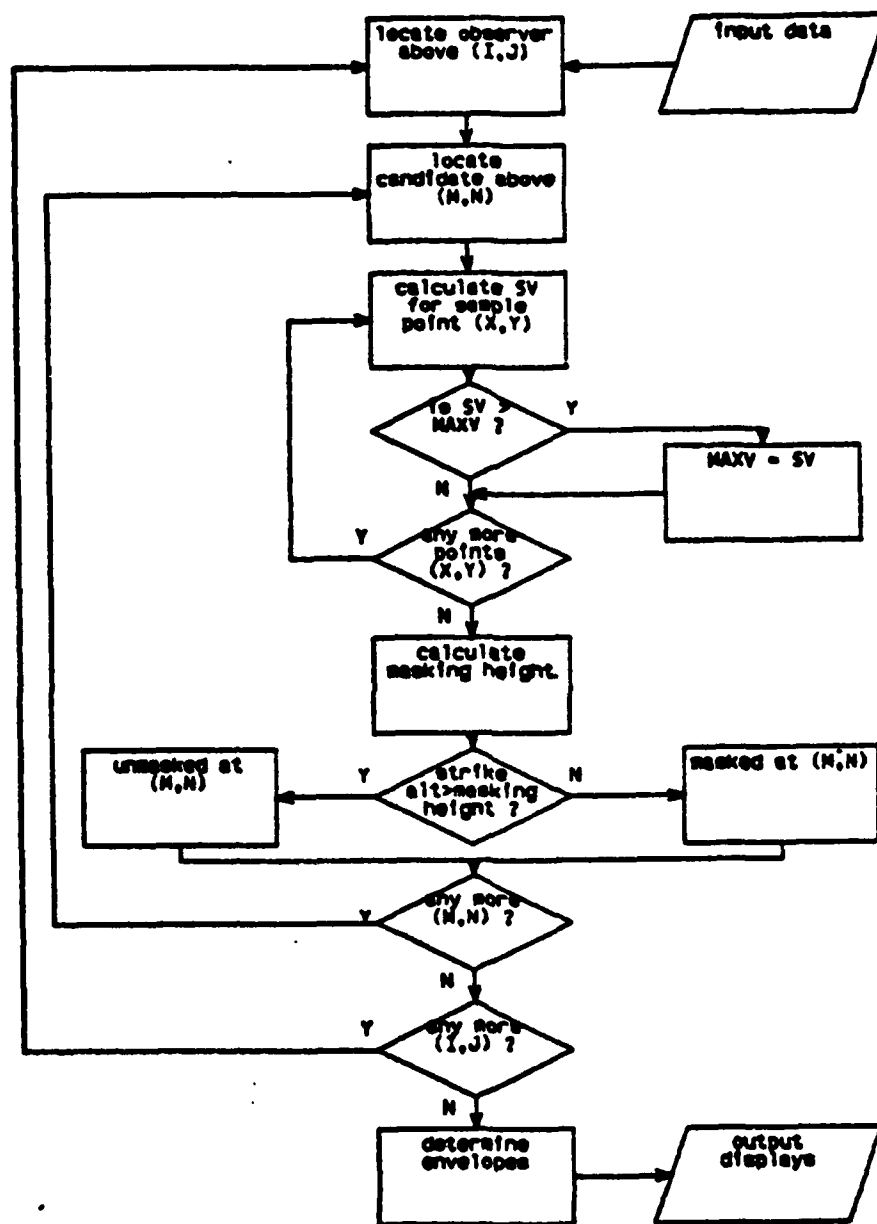


Figure 2.8 Flow Chart of Masking Calculation Process

### III. PROBLEM SOLUTION

#### A. OVERVIEW

This chapter will present an overview of the steps used in MASK to derive terrain masking envelopes. The steps involved are best examined by separating them into the three general areas of input, mathematic calculations and output.

Input starts with the standard DTED description, follows through data base transformations and concludes with determination of the relative positions of the radar sites and targets. In addition, inputs related to radar system characteristics, strike variables and atmospheric conditions are included.

The mathematic model phase begins with all initial conditions established. The math model takes the input data and performs the calculations required to determine whether or not a given point in space is in an unobstructed line of sight from the radar site. The end result is a binary indicator variable which is used in the output phase to display a masked or unmasked condition.

The output phase is concerned primarily with three map displays. The first is a topographic picture of the area in question and is alphabetically coded by elevation. This display is the link between the planner's view of the world and the masking envelopes which follow. It provides the geographic landmarks and scale indicators which make the masking envelopes useable as planning tools. The final two displays are the actual masking envelopes. There is one display based on a selected strike cruising altitude referenced to mean sea level (MSL) and one for the strike in the terrain following mode whose altitudes are referenced to height above ground level (AGL).

## B. INPUT PHASE

### 1. Terrain Data

The data base for all terrain elevation values used by MASK is the DTED produced by DMAAC. The objective of the DTED program is to digitally map the entire terrain surface of the earth. The current status of completed mapping is available in [Ref. 2].

The elevation reference for the DTED is Mean Sea Level (MSL) and the horizontal location of terrain is referenced to the World Geodetic System. All terrain elevation values are signed magnitude, sixteen-bit (two word) binary integers representing elevation in meters above MSL. The DTED is distributed on a subscription basis to a number of DOD users and is unclassified. Standard tapes are nine track, 1600 FPI/phase encoded and use ASCII code for tape labels. Complete tape specifications are contained in [Ref. 3].

The basic unit of DTED is the data file. Each data file contains the elevation data for a one degree square of the earth's surface. The reference for all data in the file is the latitude and longitude of the southwest corner of the degree square. Within the file, data is divided into records of constant longitude. Each record contains a record location identifier and the terrain elevation values which span the degree square from south to north at the given longitude. The interval between elevation values for the standard DTED is three arcseconds. In order to provide overlap between adjacent data files an extra elevation value is added to the top of each record. Accordingly, each record contains 1201 individual values (3600 arcseconds per degree divided by three arcseconds per value, plus the overlap). The records

are arranged within the file in a similar manner from west to east so that there are 1201 records spanning the width of the data file including one for overlap. The file is thus arranged so that elevation values are read from south to north within each record and records are read from west to east within the file. Figure 3.1 illustrates the internal structure of a typical data file.

For any location on the earth the standard three arcsecond interval is equivalent to approximately 300 feet (93 meters) of ground distance between elevation values when measured along a meridian (i.e., north to south). At the equator, the longitudinal (east to west) measurement is identical. However, as latitude increases, the distance between elevation points decreases when measured longitudinally. At the poles, of course, this distance shrinks to zero. The effect of this shrinkage is to increase the longitudinal density of the terrain elevation points as they depart from the equator. The relationship between the width (in distance) of a degree square at the equator and one at some other latitude is given by equation 3.1,

$$DL = 60 \times \cos(L), \quad (\text{eqn. 3.1})$$

where DL is the width in nautical miles at a given latitude and L is the specified latitude in degrees. This relationship is illustrated in Figure 3.2. Because of this decreasing longitudinal distance at the higher latitudes, the DTED changes the longitudinal interval between values. The first change occurs at 50 degrees north and south where the interval is doubled to six arcseconds. A second change takes place at 75 degrees as the interval again doubles to twelve arcseconds. These changes reduce the number of records in each data file to 601

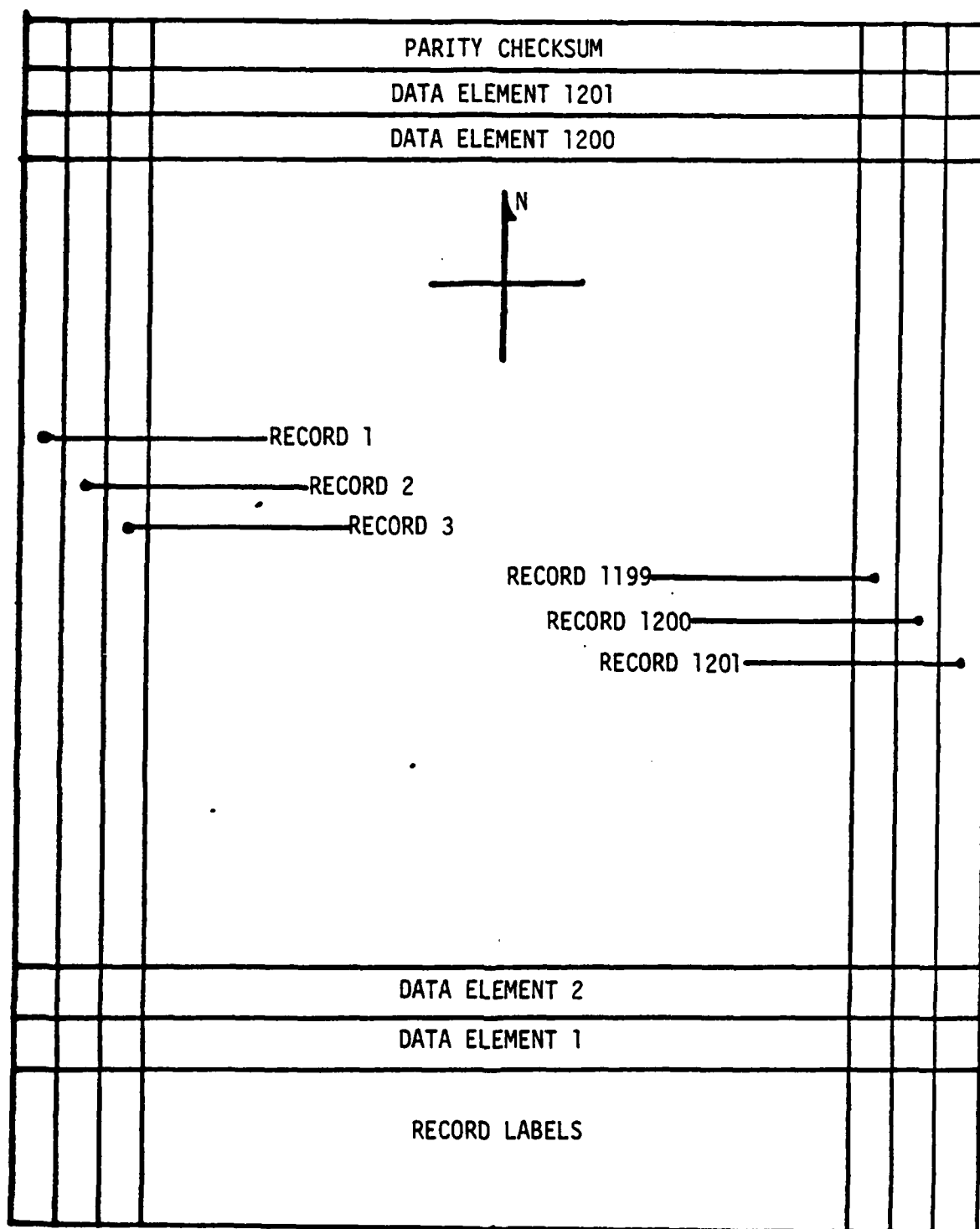


Figure 3.1 Internal Structure of a DTED Data File

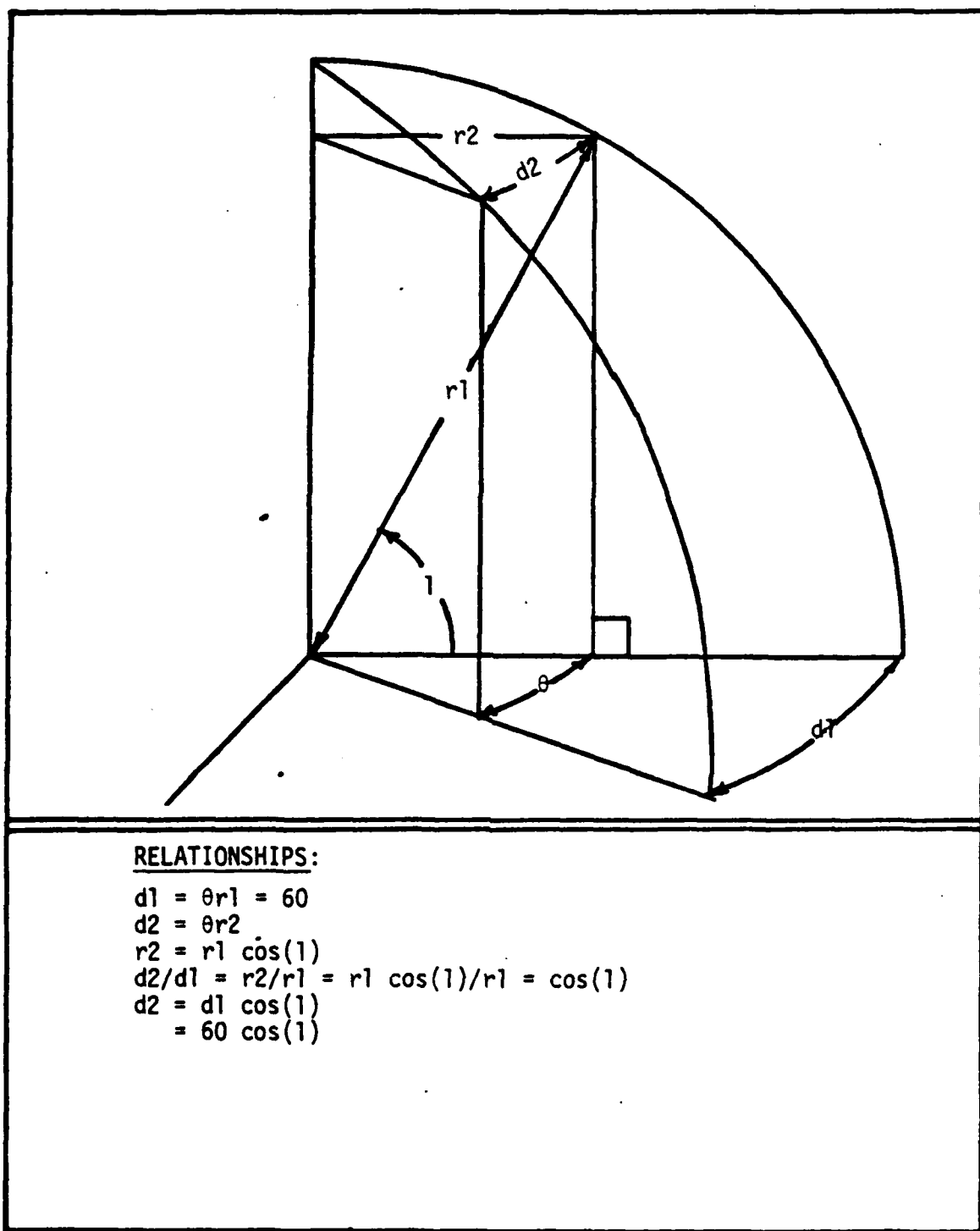


Figure 3.2 Variation of Longitudinal Distance



above 50 degrees and 301 above 75 degrees. No change is made to the number of elevation values per record, since the meridian distance remains constant for all locations.

In addition to terrain elevation data, each file contains a label identifying its location within the DTED and other administrative information including the accuracy of the data. Accuracy is in terms of a 90 percent probability that elevation errors will not exceed a given value in meters. For a complete explanation of DTED data file structure, see [Ref. 3].

## 2. Transformations

### a. General

An artificial limit was set on the core memory requirements of MASK during its development. This limit is 500 kbytes and was chosen to represent the anticipated capability of desk-top computers projected to be available in the fleet in the near term. The design of MASK requires that a large elevation data matrix and two smaller display matrices be accessible during processing. In order to remain below the core limit the data matrix size was fixed at 400 by 400 elements. Since each element is two bytes long, the data matrix alone requires 320 kbytes of core storage. The storage requirement for a complete DTED data file at the three arcsecond resolution is about 2900 kbytes. It is therefore impossible to access anything more than a fraction of a DTED file at full resolution using MASK.

Obviously, a data transformation of some kind is required for MASK to use the DTED. This transformation is normally accomplished in two steps. First, the DTED file is located and loaded from tape via

MVS to the user's diskfile. This is accomplished using the GETTAPE program which retrieves a specified DTED file and sends it to an MVS file under the name of TAPE DATA. The MVS file is then accessed and TAPE DATA is loaded onto the user's disk. Due to the size of the file a temporary disk must be defined prior to the transfer of TAPE DATA. The second step is to process TAPE DATA through a transformation program called TRANS which produces an output file called MASK DATA. MASK DATA is the 400 by 400 element square data base required by MASK. A third step, which is required if an area larger than one degree is needed, uses a program called COMBIN.

b. Transferring DTED From Tape

The GETTAPE program is a short batch program which retrieves a specified DTED file from tape and transfers it to MVS under the name TAPE DATA. The user must identify the desired file by tape label and file number prior to submitting the GETTAPE program. Each tape contains several miscellaneous administrative files interspersed with the elevation data files. Desired data files may be more easily located by using a program called TSCN, which scans the tape and prints out the contents by file number.

The tapes used in developing MASK cover an area from 46 to 51 degrees north latitude and from 118 to 124 degrees west longitude. This includes most of Washington State and part of southern British Columbia. The tapes are arranged primarily in latitude bands with each tape containing six adjacent one-degree squares. The elevation data files on each tape are numbered, from west to east, 2, 5, 8, 11, 14 and 17. Figure 3.3 shows the areas covered by tape label and file number.

FILE NUMBER	2	5	8	11	14	17
TAPE LABEL	LATITUDE AND LONGITUDE OF SOUTHWEST CORNER					
S-795	50 N 124 W	50 N 123 W	50 N 122 W	50N 121W	50N 120W	50N 119W
S-837	49N 124W	-	-	-	-	49N 119W
S-796	48N 124W	-	-	-	-	48N 119W
S-798	47N 124W	-	-	-	-	47N 119W
S-797	46N 124W	46N 123W	46N 122W	46N 121W	46N 120W	46N 119W

Figure 3.3 Geographic Areas by Tape and File Number

c. TRANS

TRANS is the workhorse of the transformation process. It accepts user defined inputs and the TAPE DATA file and produces a 400 by 400 square matrix called MASK DATA which is used by MASK. TRANS prompts the user to input certain required values. These include the latitude and longitude of the southwest corner of TAPE DATA, the southwest corner of the area within TAPE DATA to be transformed and the desired transformation interval.

Since MASK DATA can only hold a 400 square matrix the user must make a tradeoff between resolution and area coverage. If high resolution is required then MASK DATA will use the same three arcsecond interval as TAPE DATA. This necessarily limits the geographic coverage of MASK DATA to twenty minutes on each side. The next larger area covered is 40 minutes square and is obtained by selecting a transformation interval of six arcseconds. During this transformation TRANS deletes half of the elevation values in each record and half the records in the data file. This is equivalent to increasing the distance between elevation data points to about 600 feet. If the entire data file is to be transformed a similar process takes place, except that the interval is increased to nine and more points are deleted.

As previously mentioned, the user must enter the location of the southwest corner of the area to be transformed. If an entire degree is to be transformed this location must necessarily be the same as the southwest corner of the TAPE DATA file. When smaller areas are desired, the user has some flexibility in the selection of the corner point as long as it is not chosen so that TRANS runs out of data before the MASK

DATA file is filled. For example, when transforming a 20 minute square the user may locate the corner point anywhere in TAPE DATA as long as 20 minutes of data remain to the north and to the east of the location. This feature allows the user to position the MASK DATA file to best advantage in relation to terrain features or radar site locations.

In addition to transferring data based on a specified interval and origin, TRANS deletes all nonelevation information from TAPE DATA including labels, parity checks and the overlap values discussed before. The format of the data is also rearranged so that MASK can read MASK DATA as a FORTRAN matrix from right to left and top to bottom, equating this with west to east and north to south. A header is added in the first five data blocks of MASK DATA identifying the southwest corner of the file in degrees, minutes and seconds and listing the data interval specified during the transformation.

Transformation of data at latitudes greater than 50 degrees is handled within TRANS by a special algorithm. When a southwest corner latitude is greater than, or equal to, 50 degrees north or 51 degrees south a temporary file is created. TRANS then reads the TAPE DATA file and duplicates the records required to "pad" the data and make the file 1200 records wide. During this process, the padded information is stored in the temporary file. The file is then treated identically to a file from lower latitudes.

#### d. COMBIN

Thus far, MASK DATA has been limited to the size of one DTED file. While useful for fire control radars, the area of a single degree square is inadequate for evaluating the envelopes of longer range

acquisition and early warning radars. A program called COMBIN was written to increase the area coverage of the MASK DATA file. As previously stated, increasing the area of MASK DATA results in a commensurate degradation in resolution due to deletion of data points. In practice, this degradation has been slight but noticeable and is likely to be dependent on local terrain roughness and radar location as well as decreased resolution.

The concept of COMBIN is to create a mosaic of several files previously transformed by TRANS. Of necessity, the output from COMBIN will still be limited to the size of the MASK DATA file and the caveat regarding resolution applies. To form the "tiles" of the mosaic, individual DTED files are transformed using intervals greater than nine and are stored in separate numbered files. When all of the required files are transformed and properly assigned by file definition (FILEDEF) to their positions in the mosaic, COMBIN systematically accesses the files by number and combines the data into the standard MASK DATA format. For example, if an area two degrees by two degrees were required, four separate DTED files would have to be processed by TRANS at an interval of 18. They would then be assigned by the user to FILEDEFs 11-14 according to their relative geographic positions with the northwest file assigned to 11, the northeast to 12, the southwest to 13 and the southeast to 14. COMBIN would then be run and would access each file in turn, placing the appropriate data in the mosaic. The product of COMBIN would be a MASK DATA file which would be identical to one produced directly by TRANS, except that it would cover four times the area at a reduced resolution. The same general procedure applies to larger areas.

At present, the largest area which COMBIN will process is a square mosaic of twenty-five individual DTED files. This equates to an area of about 200 by 300 nautical miles at 48 degrees of latitude. The five by five degree square was chosen as a limit for two reasons. First, the interval at this resolution is 45 arcseconds (three-fourths of a nautical mile) and that is a significant distance between elevation data points, especially in rough terrain. The second reason is that the process is largely manual, since the user must load and transform twenty-five DTED files and then assign each to a specific location in the mosaic. The next larger square would contain 36 files and that is considered excessively time consuming. An example using COMBIN will be presented in Chapter V.

### 3. Radar Parameters

#### a. Location

In addition to the data provided by the DTED, MASK prompts the user to provide specific information about the radar site or sites to be used. At a minimum, the latitude and longitude in degrees, minutes and seconds is required for each site. If no information about the radar site elevation is provided, MASK will determine elevation based on the location entered by the user. A separate entry must be made giving the antenna height above the ground. If this information is not known, a default entry will assign a value of five meters to the mast height. It is, of course, preferable to use the actual antenna elevation but MASK will perform the calculations using only the latitude and longitude if necessary.

Since site location is a critical variable in computing the masking envelope, an effort has been made to provide as accurate a site location as possible within the MASK DATA matrix. Some mention was made

in Chapter II of the requirement to cope with observers who fail to exist exactly at matrix element locations. This requirement is not as critical with a high resolution matrix as with one which has a large interval between data points. Positional errors in the large area data bases could be on the order of half a mile if site locations within the matrix were restricted solely to matrix element locations.

In general, geographic location in MASK is represented by the position of a subscripted element in the MASK DATA matrix. The point (1,1) defines the northwest corner of the matrix and (400,400) is the southeast corner. When MASK DATA is read by MASK the latitude and longitude of the southwest corner is used as the geographic reference point for the rest of the points in the matrix. By reading the transformation interval on the MASK DATA file header, MASK has all of the information necessary to compute the latitude and longitude of any element in the matrix. The actual location of any element in MASK DATA is completely determined by the data point location originally used in preparing the DTED file. These locations are used for the positions of the candidate points (CP) discussed in Chapter II. Location of the radar site is a more complex problem, since these sites will most likely be placed in locations which do not correspond exactly to the location of any DTED elevation data point. Note that in the following discussion (I,J) refers to the actual site locations, while (II,JJ) describes the closest MASK DATA element to the northwest of (I,J). A method was devised for MASK which allows for representing the exact site location in terms of a matrix element (II,JJ) and an incremental displacement (DI,DJ) from that element. This relationship is illustrated in Figure 3.4. Whenever MASK performs a measurement in relation to a site,



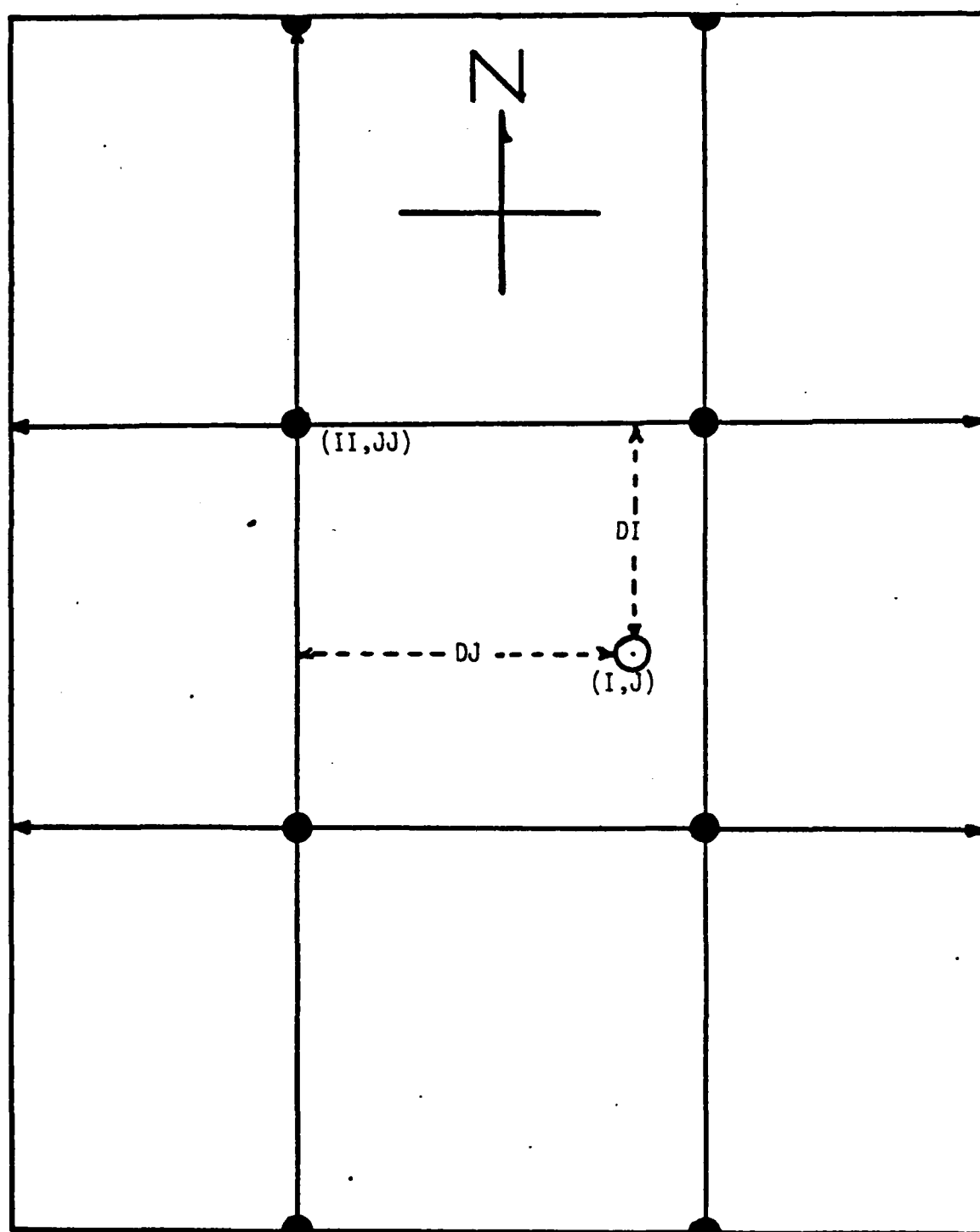


Figure 3.4 Radar Site Location Method

the distance is in terms of the distance to (II, JJ) and then an additional incremental distance is either added or subtracted to compensate for the offset location of the site.

b. Elevation

One of the applications of the method just described is in determining a given site elevation in the absence of specific user information. If the site were located exactly at a position corresponding to (II, JJ) it would only be necessary to dereference the value of (II, JJ) to obtain the site elevation. In most cases, however, an interpolation must be performed to derive an approximate elevation value. Since MASK keeps track of the exact position of the site within a four element square, a weighted interpolation is performed based on the relative proximity of the site to each of the four surrounding elevation data points. Consequently, the interpolated elevation value derived by MASK is more accurate than a simple average of the elevations of the surrounding points.

It should be noted that although the internal manipulation of data in MASK is in terms of meters, the input values are specified in terms of feet to comply with common usage in the Navy.

c. Pulse Repetition Frequency

The final site parameter is the pulse repetition frequency (PRF) of the radar. MASK accepts a value up to 9999 pulses per second. This is used to compute the radar's maximum unambiguous range (MUR) according to equation 3.2,

$$MUR = C / (2 \times PRF), \quad (\text{eqn. 3.2})$$

where C is the speed of light in a vacuum. If there is a range of PRF the user should enter the lowest value which is operationally employed.

Some radars use two simultaneous PRFs to extend the MUR. In this case, the user should enter the difference between the two. The MUR is used in MASK to reduce run time by limiting masking calculations to those points in the matrix whose slant range from the radar is less than the MUR. Points outside the MUR are automatically classified as masked. If the user does not desire the MUR limit imposed, a default value of -999 will set the PRF value so low that the MUR is beyond the display capabilities of MASK. In particular, deletion of the MUR limit would be applicable to all non-pulsed radars.

#### d. Multiple Sites

MASK is capable of processing and displaying the combined envelopes of up to nine different radar sites on any given run. After completing all required entries for sites one through eight, MASK will prompt the user to input additional sites as desired. If more sites are required, the user so indicates and then supplies inputs for the next site as previously discussed. After the ninth site has been entered MASK will not accept further site information.

#### 4. Refractive Effects

One of the features of MASK is the modelling of the effects of refraction on radar and optical propagation paths. The concept outlined in Chapter II requires that an equivalent earth radius be calculated as a function of the refractive gradient,  $dn/dh$ . MASK uses the scaled-up gradient,  $dN/dh$  for this purpose. The value of  $dN/dh$  must be computed and input by the user if non-standard propagation is to be modelled. In the standard case, the user enters a value of -039 which results in the conventional four-thirds earth radius model. Land based systems

will not normally be subject to effects such as superrefraction or ducting, since these phenomena are caused primarily by the formation of evaporation layers over large bodies of water. If, however, a land based system is located in an essentially marine atmospheric environment significant anomalous propagation can result. An example of such a situation is the use of radar for coastal defense and surveillance. If the radar is placed sufficiently close to the coast it will be immersed in a marine air mass and is likely to be subject to the refractive anomalies normally associated with shipboard radar propagation. In these cases a non-standard value of  $dn/dh$  should be used to determine the equivalent earth radius.

The best available source of information on the value of  $dn/dh$  is the IREPS computer program, which is installed on all CVs. One of the outputs of IREPS is a table of  $N$  values for various heights in kilometers above MSL. In addition, IREPS predicts a radar ducting height if conditions would produce one. To compute  $dn/dh$ , the user chooses an altitude above MSL and subtracts the value of  $N$  at the radar antenna height from the value of  $N$  at the specified altitude (the result will normally be negative). This number is then divided by the difference between the two altitudes in kilometers. The altitude should be chosen to include the proposed strike altitude. For example, if the strike altitude were 5000 feet MSL the user would choose an  $N$  value at an altitude of about 1525 meters, interpolating as necessary from the available altitude readings. The value of  $dn/dh$  obtained in this manner would be the average gradient from the surface to 5000 feet MSL. If ducting is predicted by IREPS, this indicates that an average value is probably not appropriate, since there will be a significant difference in  $dn/dh$  values at various altitudes.

In these cases, the predicted ducting height should be used to calculate  $dN/dh$ . If the radar and the aircraft are both below the ducting height, MASK will use the non-standard value of  $dN/dh$ . Otherwise, standard four-thirds earth radius will be used. It is recommended that the value of  $dN/dh$  be computed whenever the information is available, since even normal refractive conditions cover a wide range of values for  $dN/dh$ .

MASK does not model atmospheric effects at the same level of sophistication as the IREPS program. Consequently, there is one case in which MASK will not produce accurate results. This occurs when ducting is present and the radar is located inside the duct but the aircraft is located above the duct. MASK contains no algorithm to predict the radar's ability to "see through" the top of the duct. In this case, MASK uses the four-thirds earth radius model and produces coverage envelopes which are likely to extend well beyond the radar's actual coverage. The terminal prompt message for entering ducting height contains a specific warning to this effect. In such situations the user should consult the IREPS vertical coverage diagram for the radar in question to determine the severity of predicted radar coverage loss.

One special use of the refractive effects inputs is to model the coverage of optical systems. Under standard conditions the distance to the optical horizon is approximately seven percent greater than the geometric horizon and seven percent less than the radar horizon [Ref. 4: p 48]. The reason that the optical horizon is less than the radar horizon is that light refraction depends only on temperature and pressure and not on humidity as in the case of radar. The result is that the values of  $dN/dh$  obtained from IREPS cannot be used to account for optical

refraction. It is possible, however, to model standard day optical refraction in MASK by entering a  $dn/dh$  of  $-020$ , which equates to the correct equivalent earth radius for optics. This value has no relation to the actual optical refractivity but is merely a means of tricking MASK into producing standard day optical conditions. The appropriate ducting height value in this special case is 99999.

#### 5. Strike Altitudes

MASK is able to process two types of strike profiles simultaneously. The first type is a cruising profile in which the aircraft maintain a given altitude above MSL. This profile is applicable to transiting to and from a low altitude descent point or for strike elements whose mission requires that they remain at higher altitudes. The second type is a terrain following profile which is applicable to strike aircraft attempting to remain below the terrain masking altitude during the terminal portion of the attack. MASK requires that the user enter a value in terms of feet above ground level (AGL) and one in terms of feet above MSL. There is no requirement for any dependence between the two values, thus allowing for simultaneous processing of coverage envelopes for widely separated strike elements. A special value is required by MASK if the user does not want one or the other of the coverage displays to be output.

#### 6. Topographic Display Selection

The user must choose whether or not to display a topographic map of the area covered by MASK DATA. It is necessary to have a copy of the topographic display in order to interpret the masking envelope displays. However, the topographic display will not change unless MASK DATA is changed, so one initial copy will suffice for any number of envelope displays as long as the same MASK DATA file is used.

## 7. Input Errors

If, at any time during the input phase, an entry is made in error it cannot be changed. The only corrective action is to press the ENTER key twice which causes the program to abort. All previous inputs are automatically erased and the program must be run again from the beginning.

Since the inputs for MASK are all integers, it is vital that the user enter them in the correct format using right justification. Each prompt message specifies the exact format of the required response, including sign if negative values are appropriate. The only exception is a value of zero, in which case the format is irrelevant. Failure to comply with the specified input format will produce results ranging from inaccuracy to program abort.

## C. MATHEMATIC MODEL

### 1. General

This section discusses the mathematic model which manipulates the input data and creates the output displays. The model is composed of the main program, MASK, five subroutines and three short functions. All program elements are written in FORTRAN IV and use the IBM 3033 FORTHX compiler. Calculations are primarily done in single precision with the exception of some of the angle computations which use double precision. In addition to the MASK program elements, there is an executive program called FLY EXEC which defines certain files and compiles, loads and runs either MASK, TRANS or COMBIN. Other functions related to acquiring temporary disk space and moving files from MVS to disk are performed by a profile executive program during the log-on procedure. In the sections which follow, each of the program elements is discussed, emphasizing the

the concepts used to solve the masking calculation problem. Detailed discussion of the program code is only used when required to explain the method used by a particular routine.

The main program is presented first from start to finish, followed by each subroutine in order and then the functions. Flow charts are interspersed in the text to provide a graphic display of the program structure. It will be helpful for the reader to briefly review the flowcharts prior to reading the explanations in the text. The flowchart for the main program, MASK, is shown in Figure 3.5.

## 2. MASK

The first portion of MASK is devoted to reading the input data discussed in the previous section. At the end of this phase MASK knows the position and elevation of each element in MASK DATA, the southwest corner of MASK DATA, the transformation interval, the latitude, longitude, elevation, mast height and PRF of each site, the number of total sites, strike altitudes in AGL and/or MSL terms, dN/dh, ducting height and topographic display selection.

The next operation is initialization of variables. These include actual earth radius, resolution of the output displays, the value of pi, the relation between meters and feet and the dimensions of the output displays. At this time the AGL and MSL output displays are initialized to the masked condition.

If the user has requested a topographic display, the LOOK subroutine is called and generates the display which is stored in the output file. This operation is essentially "off line" and does not require any core storage in MASK.



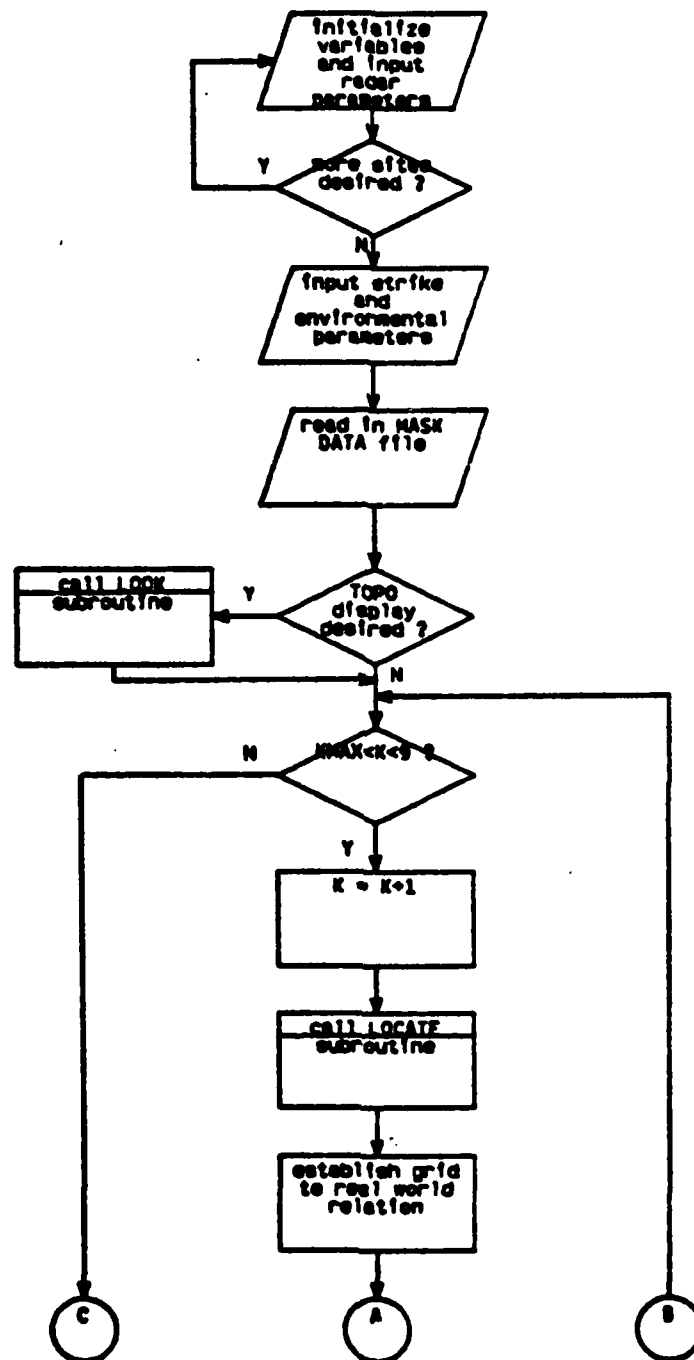


Figure 3.5a Flow Chart for MASK

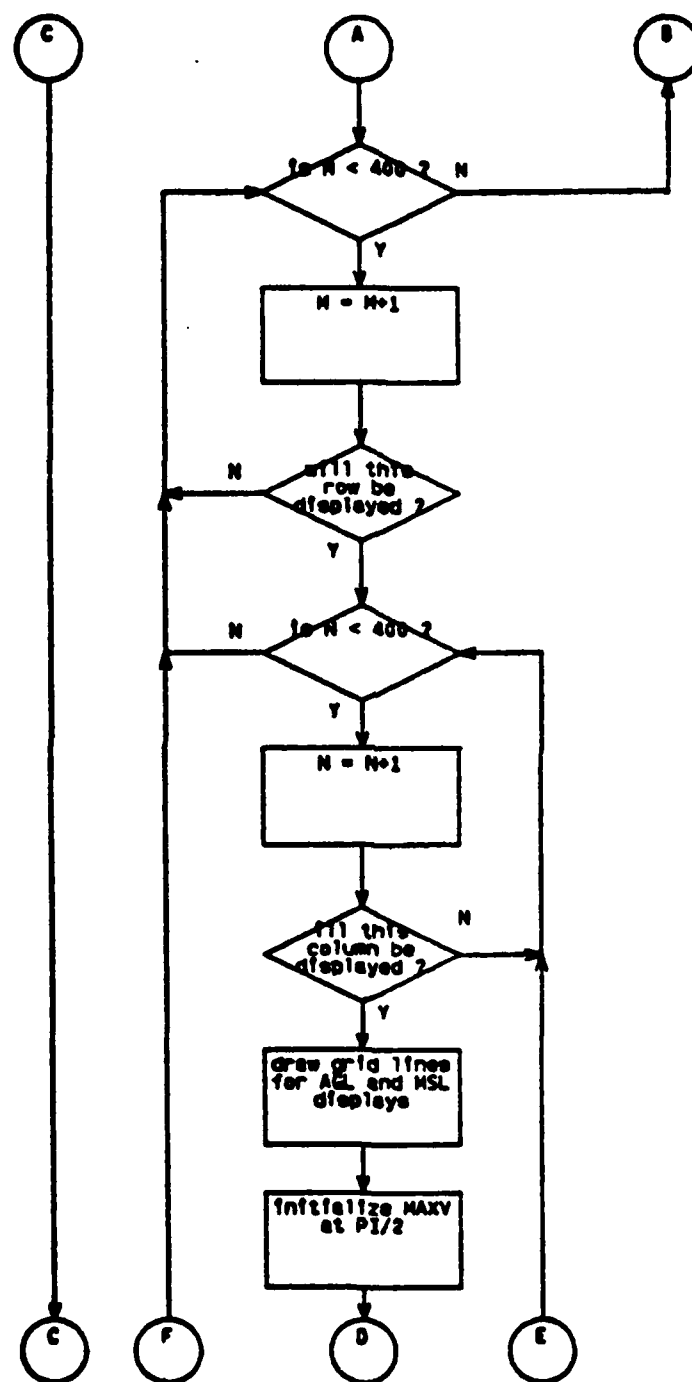


Figure 3.5b Flow Chart for MASK

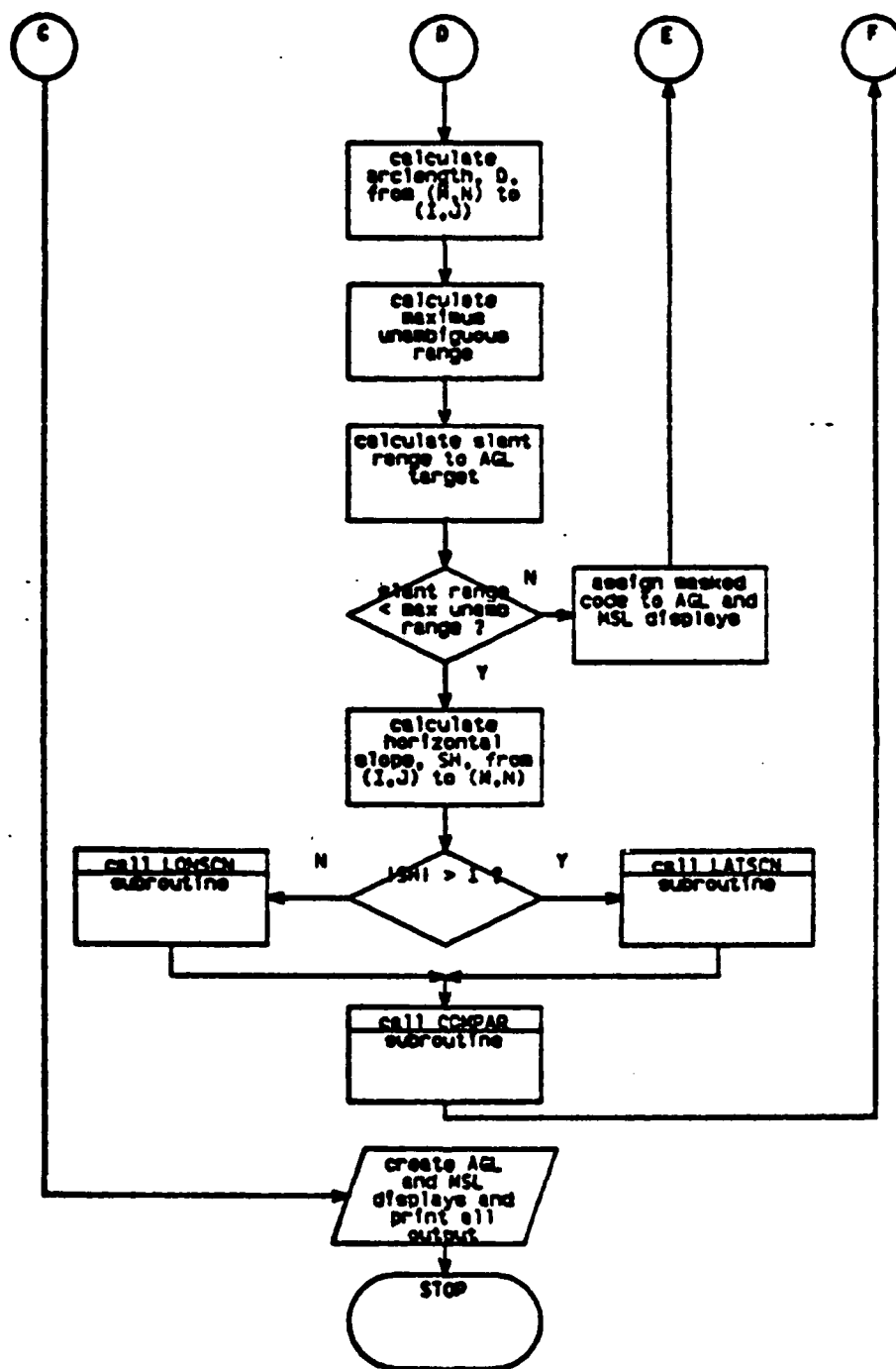


Figure 3.5c Flow Chart for MASK

The next operation is to initiate the loop which calls up each radar site in sequence. The description which follows applies to all sites as they are processed.

The first step is to compute the radar maximum unambiguous range which is stored for later comparison with the slant range from the site to each CP. Next, the LOCATE subroutine is called and returns the position (I,J) of the site and the antenna mast height if the default value is used. MASK then takes the integer value (II,JJ) of the site and subtracts (II,JJ) from (I,J) to obtain DI and DJ. These two variables describe the site offset from (II,JJ) to the south and east, respectively. If site elevation has not been explicitly input, MASK then performs the previously described interpolation of site elevation. Mast height is then added to the elevation to obtain the antenna height above MSL.

The calculations performed so far have all been in terms of matrix position or elevation. In order to measure horizontal distances along the ground a relationship must be established between the matrix dimensions and real world. As previously mentioned, the distance between elevation data points decreases as latitude increases according to the cosine of the latitude of the positions in use. In this case the latitude value used is that of the radar site. The number of meters between points in latitude (MPPLAT) is computed based on the number of meters per arcsecond of latitude (approximately 30.87) and the number of arcseconds of interval used between points. For example, if an interval of three were used MPPLAT would be approximately 92.6. The number of meters per point in longitude (MPPLON) is obtained by multiplying MPPLAT by the cosine of the radar site latitude. MPPLAT and MPPLON define the north-south and

east-west dimensions, respectively, of an imaginary rectangle formed by any four adjacent elements of MASK DATA. Another way to visualize this relationship is to think of MPPLAT as the ground distance between any two matrix elements  $(M,N)$  and  $(M+1,N)$  and MPPLON as the distance between  $(M,N)$  and  $(M,N+1)$ . All horizontal distance measurements in MASK are in terms of these two basic values.

The next event is the initiation of the nested loops which scan MASK DATA from west to east and north to south. The outer loop is the north to south one and uses the index variable,  $M$ , while the inner loop uses  $N$  as an index variable and scans from west to east. These two loops scan the entire MASK DATA matrix, but only a fraction of the elements  $(M,N)$  are actually processed as CPs. The reason is that although MASK DATA is a 400 by 400 matrix, the output matrices are only 80 characters square and will therefore only display one element in five horizontally and one in five vertically. There is no sense in processing elements which will not be displayed, so only one in twenty-five elements  $(M,N)$  is chosen as a CP. The twenty-five to one ratio is solely a function of the output display size relative to the size of MASK DATA; use of larger output displays would increase the number of CPs processed. It should be emphasized that although only a fraction of the MASK DATA elements are used as CPs, none of the matrix elements are excluded from the terrain masking calculations since the computations performed at each CP use every MASK DATA element between the CP and the site.

The first event within the  $(M,N)$  loops is to establish the five to one ratio of  $M$  and  $N$  to the display matrix indices,  $DM$  and  $DN$ . In contrast to the elements  $(M,N)$ , every element  $(DM,DN)$  will be used as a CP and will be displayed during output.

At this point the display matrices are accessed and a grid network is superimposed so that the matrices have horizontal and vertical lines printed on all four borders and at the points corresponding to DM or DN equal to 20, 40, and 60. This grid is identical on all output matrices and is used as an aid in correlating the information contained in the various displays.

The first displayable element ( $M,N$ ) is now dereferenced and its value becomes the height above MSL of the first CP. The value of MAXV is initialized at its minimum value of  $-\pi/2$  to begin the loop. The maximum unambiguous range (MUR) is compared with the slant range between the site and the CP. If the slant range is greater than the MUR the CP is considered masked. If not, the horizontal slope (SH) is computed according to equation 3.3.

$$SH = (M-I)/(J-N) \quad (\text{eqn. 3.3})$$

If J is exactly equal to N (both have the same longitude) SH is set to an arbitrarily large positive value.

The next section of MASK is devoted to sampling all intermediate points (X,Y) between (I,J) and (M,N) as described in Chapter II. The sampling value used depends on the value of SH. Logically speaking, MASK can be divided into four quadrants defined by two perpendicular lines intersecting at (I,J) with slopes of one and negative one. All those CPs which fall into the upper and lower quadrants have an SH whose absolute value is greater than one. The CPs in the left and right quadrants have slopes whose absolute value is less than or equal to one. If the MASK DATA matrix is envisioned as a network of horizontal and

vertical lines whose intersections define the individual element locations, the horizontal lines can be thought of as lines of equal latitude and the vertical ones as lines of equal longitude. If a CP is in an upper or lower quadrant, a line connecting it to the site will intersect more latitude lines than longitude lines. The opposite holds if the CP is in a left or right quadrant. All sampling for the CPs in the upper and lower quadrants is done at the points  $(X,Y)$  where the line from  $(I,J)$  to  $(M,N)$  intersects one of the horizontal lines. Conversely, the  $(X,Y)$  points for CPs in the left and right quadrants are located at the intersections of the vertical lines and the line from  $(I,J)$  to  $(M,N)$ . This method is illustrated in Figure 3.6.

Two separate subroutines handle the sampling in MASK. The LATSCN subroutine is used for CPs in the upper or lower quadrants and LONSCN is used if the CP is in the left or right. Both routines perform the necessary calculations outlined in Chapter II in order to determine a value for MAXV at each CP and return the value to MASK.

The last subroutine called by MASK is COMPAR. It is given MAXV and other inputs which it uses to compute the masking altitude, MHM, above  $(M,N)$ . The output from COMPAR is a variable for each CP, indicating whether or not a target is masked at the specified strike altitude above the CP. As each CP is processed the indicator variables are stored in the output matrices for later display as discussed in section E.

### 3. LOOK

The LOOK subroutine provides a topographic display of the contents of MASK DATA. This display is the key to interpreting the AGL and MSL displays. An alphabetic code is used to denote the elevation of each

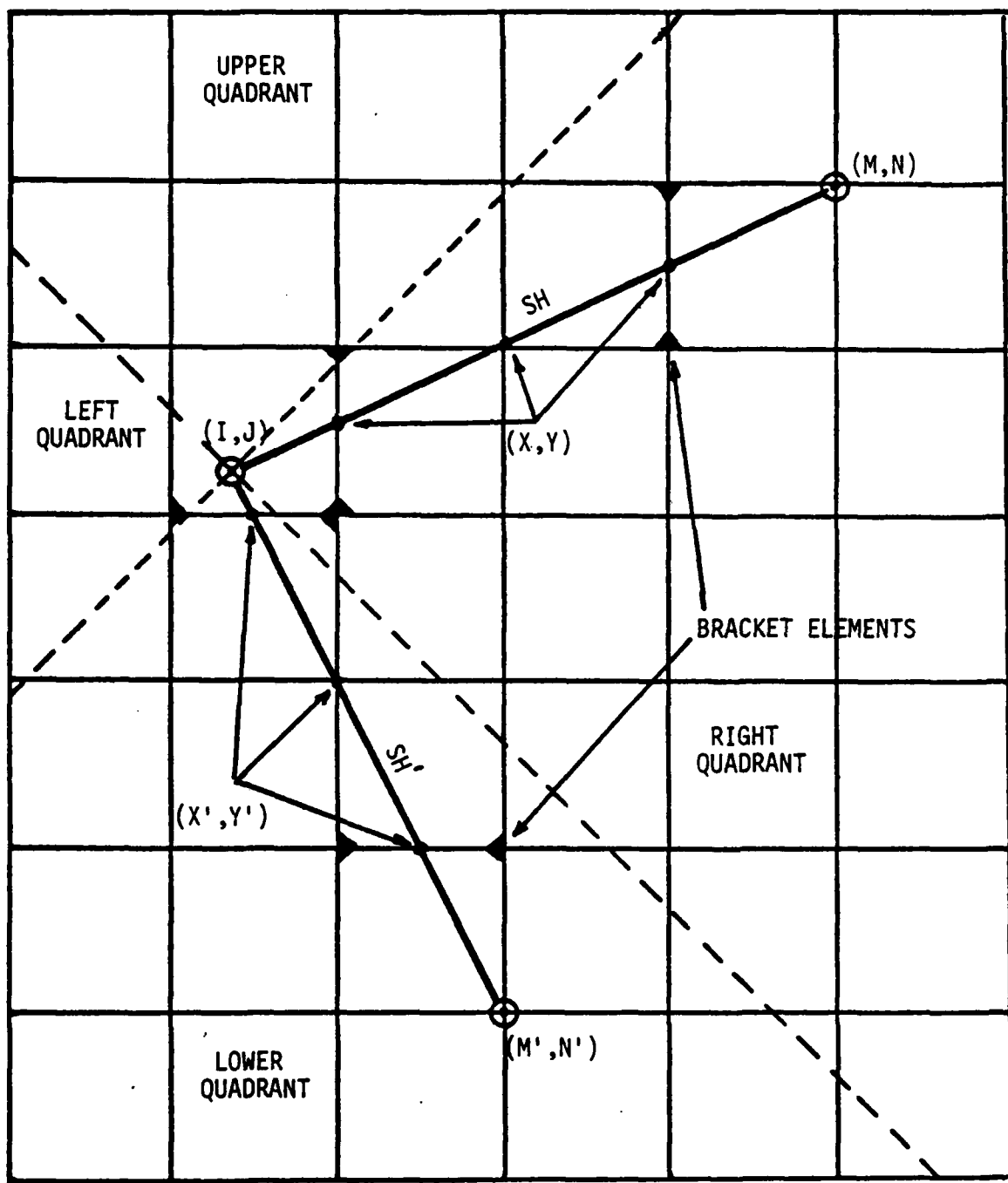


Figure 3.6 Sampling Technique for Various Quadrants



element. By comparing adjacent codes, LOOK "blanks out" all codes which are not part of a boundary between one elevation value and the next higher value. The result is that only boundary elements are displayed and these form contour lines of equal elevation. Grid lines identical to those on the AGL and MSL displays are superimposed on the LOOK output matrix to aid in display correlation. The output is annotated with the latitude and longitude of the southwest corner of MASK DATA and with a legend providing the relation between the alphabetic codes and the corresponding elevation bands. The flowchart for LOOK is shown in Figure 3.7.

#### 4. LOCATE

LOCATE determines the location of a given radar site in terms of a matrix position (I,J) within MASK DATA. It modifies its calculations to account for latitudes above or below the equator and west or east of 0 degrees longitude. Site position is based on the latitude and longitude relative to the southwest corner of MASK DATA and is transformed into matrix position by use of the transformation interval value. In addition, it assigns a default mast height value of five meters if no specific value is provided by the user. The flowchart for LOCATE is shown in Figure 3.8.

#### 5. LONSCN

LONSCN performs the task of sampling intermediate points (X,Y) between (M,N) and (I,J) when the CP is in the left or right quadrant relative to (I,J). At each (X,Y) point LONSCN locates the two elements of MASK DATA which bracket (X,Y) directly to the north and south. The location of these elements is determined by the slope of the line, SH, and the distance from Y to J. The elevation values of the bracketing elements are used to interpolate the elevation value of (X,Y). The interpolation is

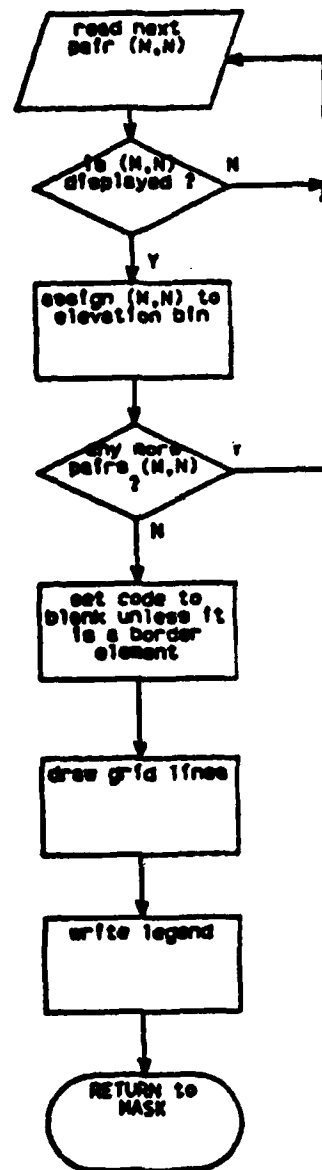


Figure 3.7 Flow Chart for LOOK

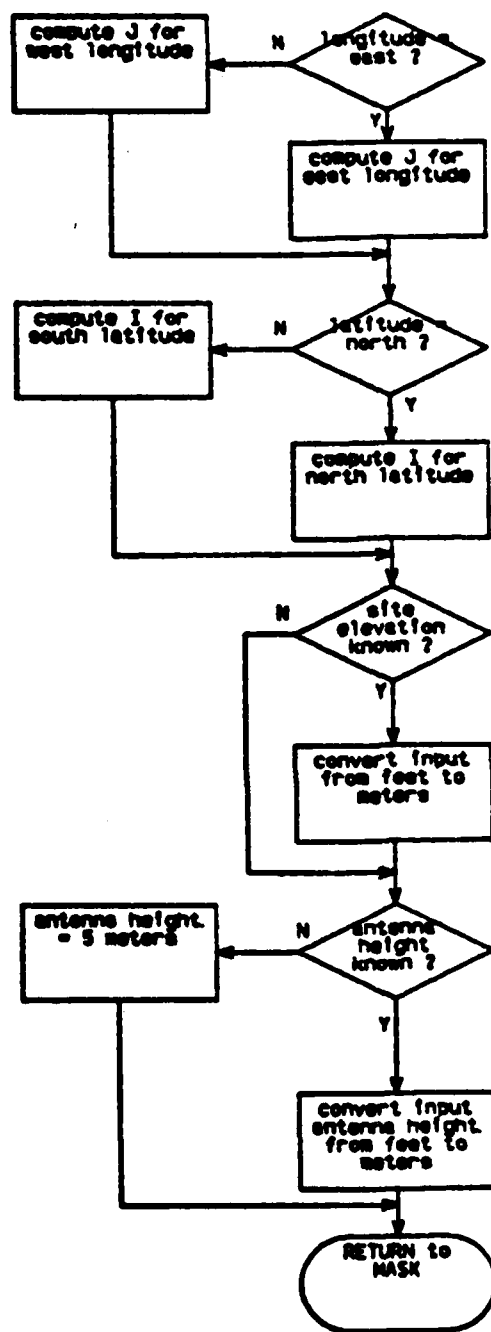


Figure 3.8 Flow Chart for LOCATE

done using a weighted value for each elevation based on the distance of  $(X,Y)$  from each element. If  $(X,Y)$  chances to fall exactly on a MASK DATA element the elevation of that element is simply assigned to  $(X,Y)$ .

LONSCN also performs the spherical to planar transformation discussed in Chapter II. The first step in this process is to find the ground distance from  $(I,J)$  to  $(X,Y)$ . This is done by first computing the length of the hypotenuse of a triangle whose base is equal to  $MPPLON$  and whose height is equal to  $SH$  times  $MPPLAT$ . This distance corresponds to the length of a segment of the line from  $(I,J)$  to  $(M,N)$  as it passes between two vertical lines separated by one  $N$ -unit. This length is then multiplied by the difference between  $Y$  and  $J$  to give the desired ground distance. The ground distance is divided by twice the equivalent earth radius to give the value for the angle,  $ALPHA$ .  $ALPHA$  is then used to compute the equivalent heights,  $h1'$  and  $h2'$ , and the increased distance  $D'$ .  $SV'$  is computed as discussed in Chapter II and is compared with the current value of  $MAXV$ . If  $SV'$  is larger than  $MAXV$ ,  $MAXV$  takes on the value of  $SV'$  for the next comparison. The next adjacent  $(X,Y)$  point is then investigated using the same process. Once all  $(X,Y)$  points along the line have been investigated the existing value of  $MAXV$  is returned to MASK for use in COMPAR. The flowchart for LONSCN is shown in Figure 3.9.

#### 6. LATSCN

LATSCN performs the same operations as LONSCN for all CPs in the upper or lower quadrants. The code is, of course, written to handle the problem with a 90 degree rotation of axes, but the concepts are identical. The flowchart for LATSCN is shown in Figure 3.10.

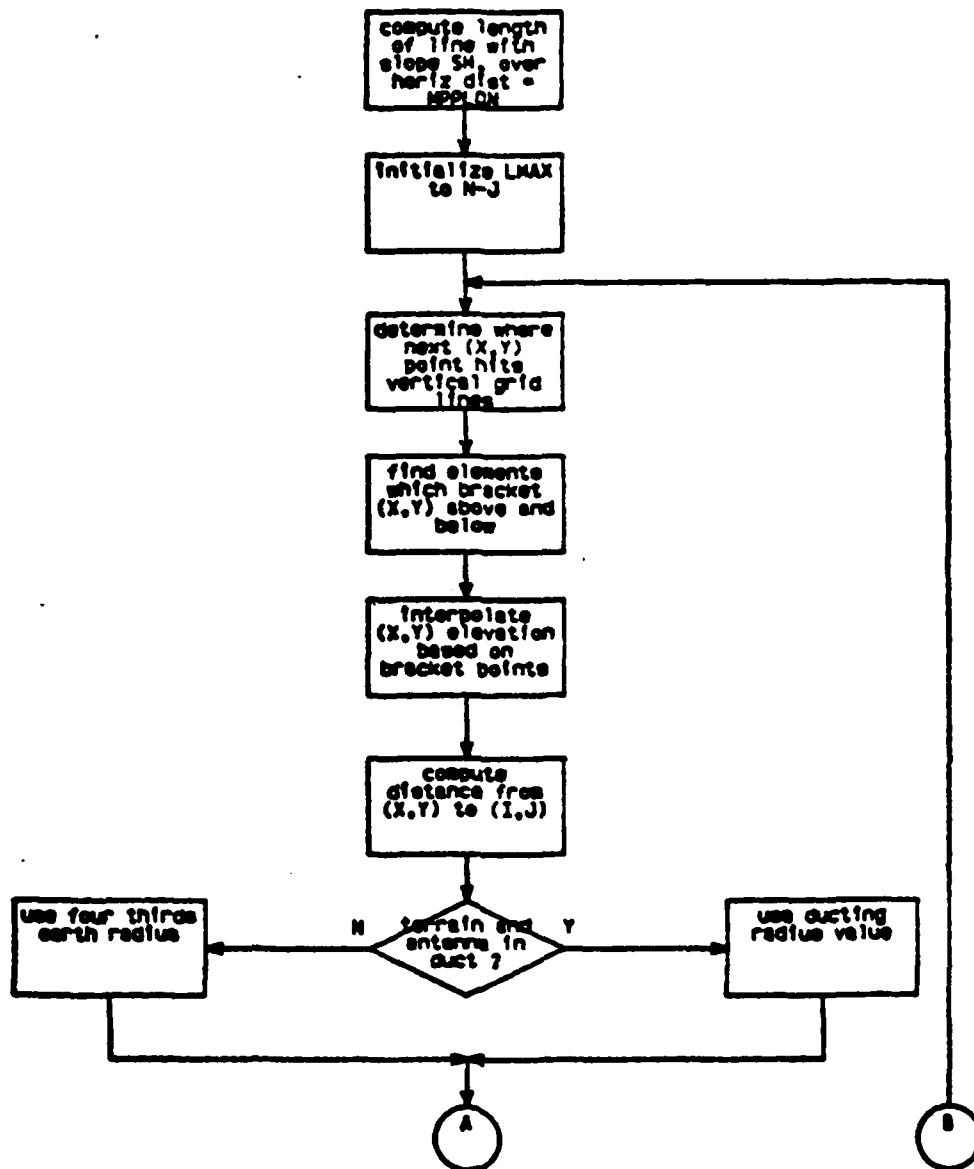


Figure 3.9a Flow Chart for LONSCN

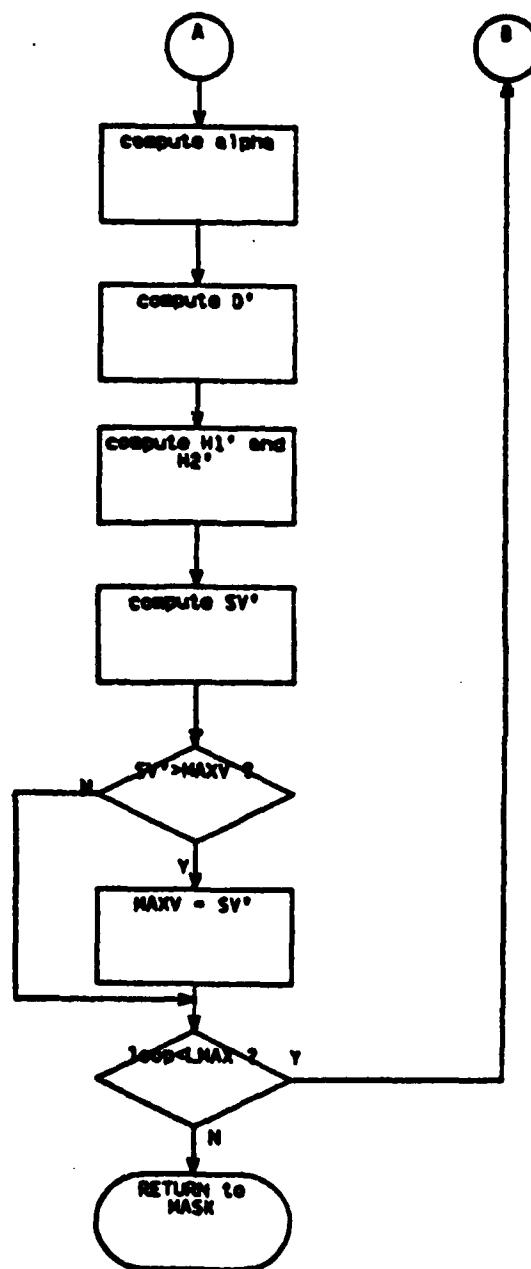


Figure 3.9b Flow Chart for LONSCN

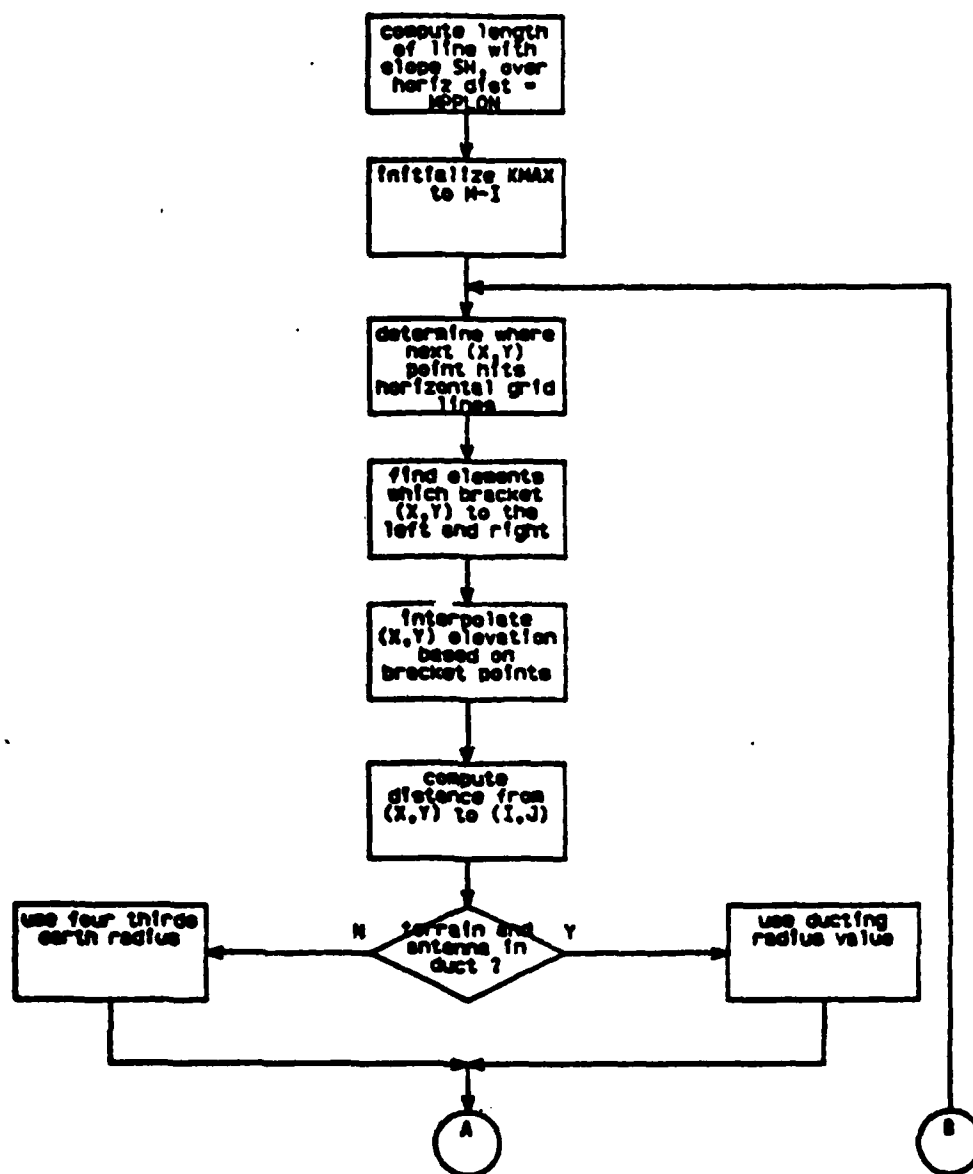


Figure 3.10a Flow Chart for LATSCN

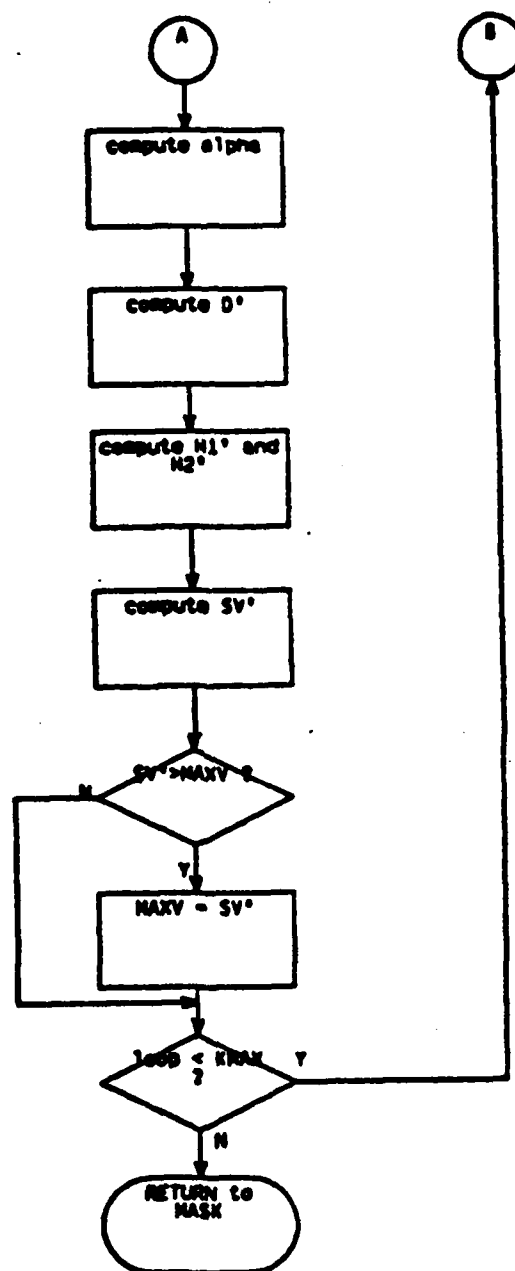


Figure 3.10b Flow Chart for LATSCN



## 7. COMPAR

COMPAR performs several functions. The first is the calculation of the masking height in meters above MSL at the CP. The problem is set up as a triangle having one apex at the radar antenna (A), one at the center of the equivalent earth (C) and one at an unknown height (B) above (M,N). The distance from (I,J) to (M,N) is the arclength separating AC and BC at the equivalent earth radius from C. The angle (BETA) subtended by this arclength is obtained by dividing the arclength by the radius. The angle between AB and BC is pi minus the sum of MAXV and BETA and is the angle opposite to AC. The length of the side AC is known to be the equivalent radius plus antenna height above MSL. By using the above information and the Law of Sines, COMPAR obtains the length of the side BC. The value of the masking height above MSL (MHM) is obtained by subtracting the equivalent earth radius from the length of BC. A corresponding value for the masking height above ground level (MHA) is obtained by subtracting the elevation value at (M,N) from MHM.

The determination of the state of the indicator variable at (M,N) is made by comparing MHM to the input MSL strike altitude and MHA to the AGL altitude. If MHM is greater than the MSL strike altitude, the indicator variable takes on a value equivalent to a masked condition. If MHM is less than the MSL altitude, the indicator variable shows that the aircraft is unmasked and within the radar maximum unambiguous range at the specified altitude. The MHA comparison performs the same function in relation to the AGL strike altitude. The MHM comparison may also result in a third state for the indicator variable. This occurs if the specified input value of the MSL strike altitude is less than or equal to the terrain

elevation at the CP, regardless of the masking calculation. This state is displayed to alert the user to the fact that the assigned MSL altitude is infeasible at that particular point. The indicator variables generated by the calculations for the point (M,N) are stored in the AGL and MSL displays at the location (DM,DN), which is identical in both displays.

As the MASK DATA matrix is sequentially investigated, the indicator variables in the AGL and MSL matrices eventually form sets of masked points, unmasked points and, in the MSL matrix, points where terrain elevation exceeds strike altitude. A procedure is employed, similar to that used in LOOK, which blanks out all masked and unmasked indicator variables except those which define the boundary between the two sets. The result is an envelope extending out from the radar site within which an aircraft at the specified altitude is in the direct line of sight and inside maximum unambiguous range. COMPAR also generates up to nine numbered site locations for display in the AGL and MSL outputs. If more than one site is placed at the same display element only the number of the last site input will be displayed on output. If envelopes from multiple sites overlap, the individual boundaries within the overlap area are deleted and the envelopes are merged into a single continuous area of coverage. This results in a much more easily interpreted output display. If individual envelopes are desired, the user must run the sites separately. The flowchart for COMPAR is shown in Figure 3.11.

#### D. FUNCTIONS

MASK uses three short functions. The IASEC function converts degrees, minutes and seconds of arc into units of seconds only. The RAD function

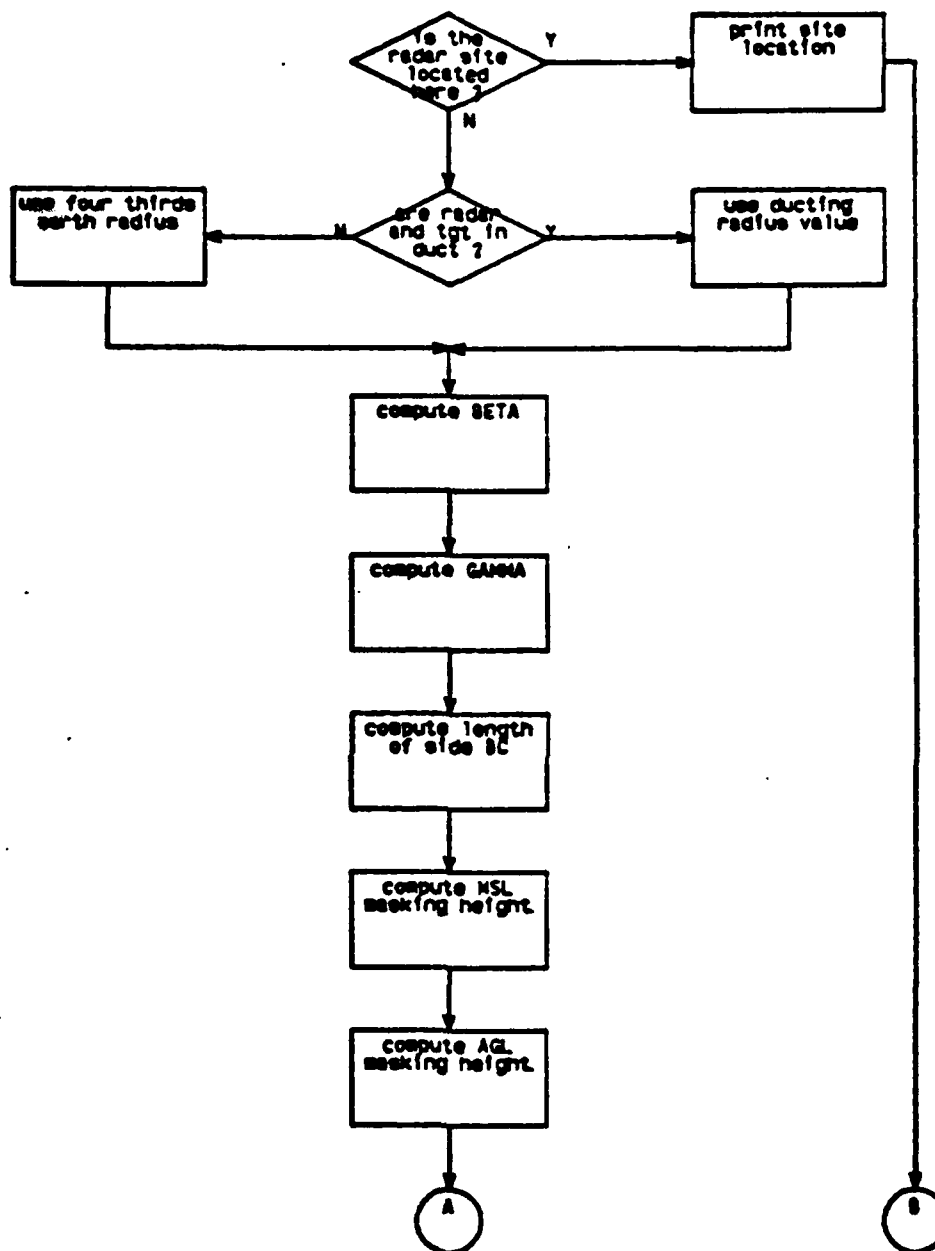


Figure 3.11a Flow Chart for COMPAR

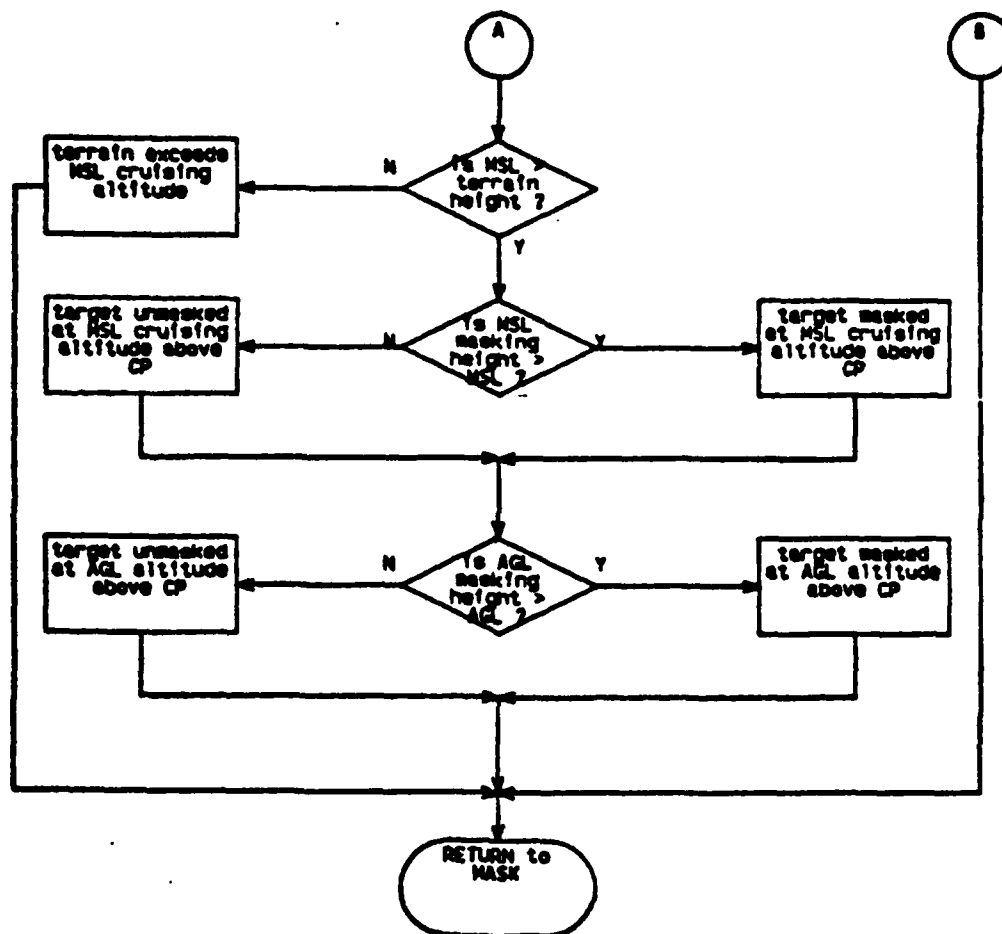


Figure 3.11b Flow Chart for COMPAR

converts degree angular measurements into equivalent radian values. IRND converts real numbers to integers by performing a round-off (instead of the normal truncation used by the library function).

## E. OUTPUT

### 1. Topographic Display

The topographic display is selected by the user during the input phase. The purpose of the display is to provide a reference to aid in relating the AGL and MSL masking displays to actual geographic features such as mountain ranges, river valleys and coastlines. The topographic display has much the same appearance as a typical topographic chart. Contourlines are spaced closely in areas of steep terrain and are more widely spaced in areas of moderate terrain variation. Coastlines are easily recognized due to the use of the special symbol (.) for sea level elevation. The grid system which overlays the elevation code provides additional cues for locating geographic features and relating them to the same features on standard aeronautical charts. In effect, the topographic display acts as the interface between the AGL and MSL masking displays, which contain almost no geographic references, and the detailed charts used in planning strike routes. Figure 3.12 shows a typical topographic display while Figure 3.13 shows the same geographic area on an aeronautical chart.

### 2. AGL Display

The AGL display shows numbered site locations and the masking envelope for the specified AGL strike altitude. The area depicted in the display is identical to the area covered by the topographic display.

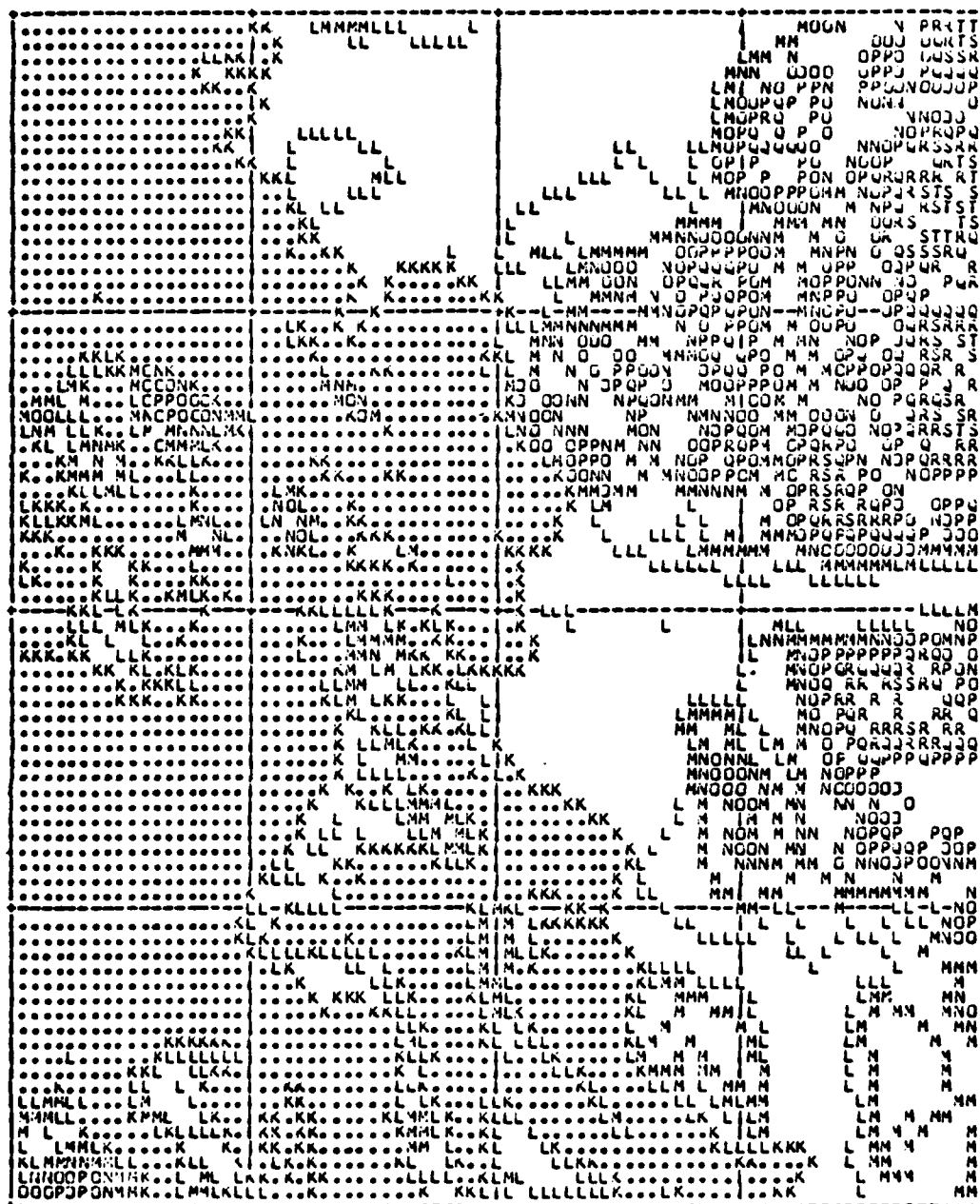


Figure 3.12 Topographic Display Example



There is, in fact, a one to one relationship between each position on the topographic display and the corresponding position on both the AGL and MSL displays. This allows the user to physically overlay one display on top of another during the correlation process. The recommended procedure is to highlight the masking envelope with a dark pen, place the topographic display on top of the AGL display and simply trace the envelope onto the topographic display. If desired, transparencies may be made of the AGL display and then used as overlays on top of the topographic display.

In addition to the graphic portion of the AGL display there is a separate printed page containing amplifying information. The information includes the latitude and longitude of the southwest corner of the display, the grid spacing in minutes, the physical dimensions represented by each display symbol,  $dn/dh$ , ducting height, the input parameters of each radar site and a legend describing the meaning of the display symbols.

One common effect shown in the AGL displays warrants some explanation. Instead of a single envelope being displayed, it is not unusual for the AGL display to contain several disjoint masking envelopes. The explanation for this is that the aircraft altitude is varying with ground elevation in order to maintain a constant AGL height. As a result, the specified AGL altitude will occasionally rise above the masking height and then fall below it closer to the site. This would occur, for example, if the aircraft had to climb over a ridge at some distance from the site. Just prior to cresting the ridge the aircraft would enter the unmasked envelope and then as the aircraft descended into the valley below it



would become masked again until it came sufficiently close to the site to be seen continuously. In this manner, several disjoint areas of clear line-of-sight are normally generated in mountainous areas, while fewer are generated in less variable terrain. This situation does not occur at all over water, nor does this effect appear in the MSL displays, since the aircraft are maintaining a constant MSL altitude.

### 3. MSL Display

The MSL display contains the same information as the AGL display except that the indicator variables are generated by comparing the masking height with the specified MSL strike altitude at each CP. The symbology, grid markings and explanatory pages are identical to those used in the AGL display with one addition. The symbol "0" is used to denote areas in which the terrain exceeds the specified MSL altitude. Flight in such regions is infeasible for obvious reasons.

#### IV. MODEL VERIFICATION

##### A. GENERAL

This chapter will briefly describe methods of verifying the accuracy of the output from MASK.

The most realistic and most costly method of verifying the results of MASK's calculations is flight testing using actual radars and aircraft. There are, however, other methods which may be used to ascertain whether or not MASK is performing properly. Two such tests are presented below. Prior to describing the tests, however, some explanation should be given regarding the data base used in the tests.

##### B. TEST DATA BASE

In order to have a simple data base of known characteristics a test data base was developed for MASK. The data base is a 400 by 400 element matrix containing three pyramids which are placed on a sea level plain. Figure 4.1 is a topographic display showing the arrangement of the pyramids. The pyramids are of varying heights with the one in the southeast area of the plain being the shortest. The northwestern pyramid is twice the height of the short one and the northeastern one is four times the height of the short one. The two to one ratio of heights between successively taller pyramids facilitates certain comparisons which are used in testing.

Some characteristics of the test data base are designed to be adjustable by changing the appropriate parameters in the program, TERR, which creates the data base. The transformation interval may be varied from 3 to 45 arcseconds, effectively changing the area coverage of the data base

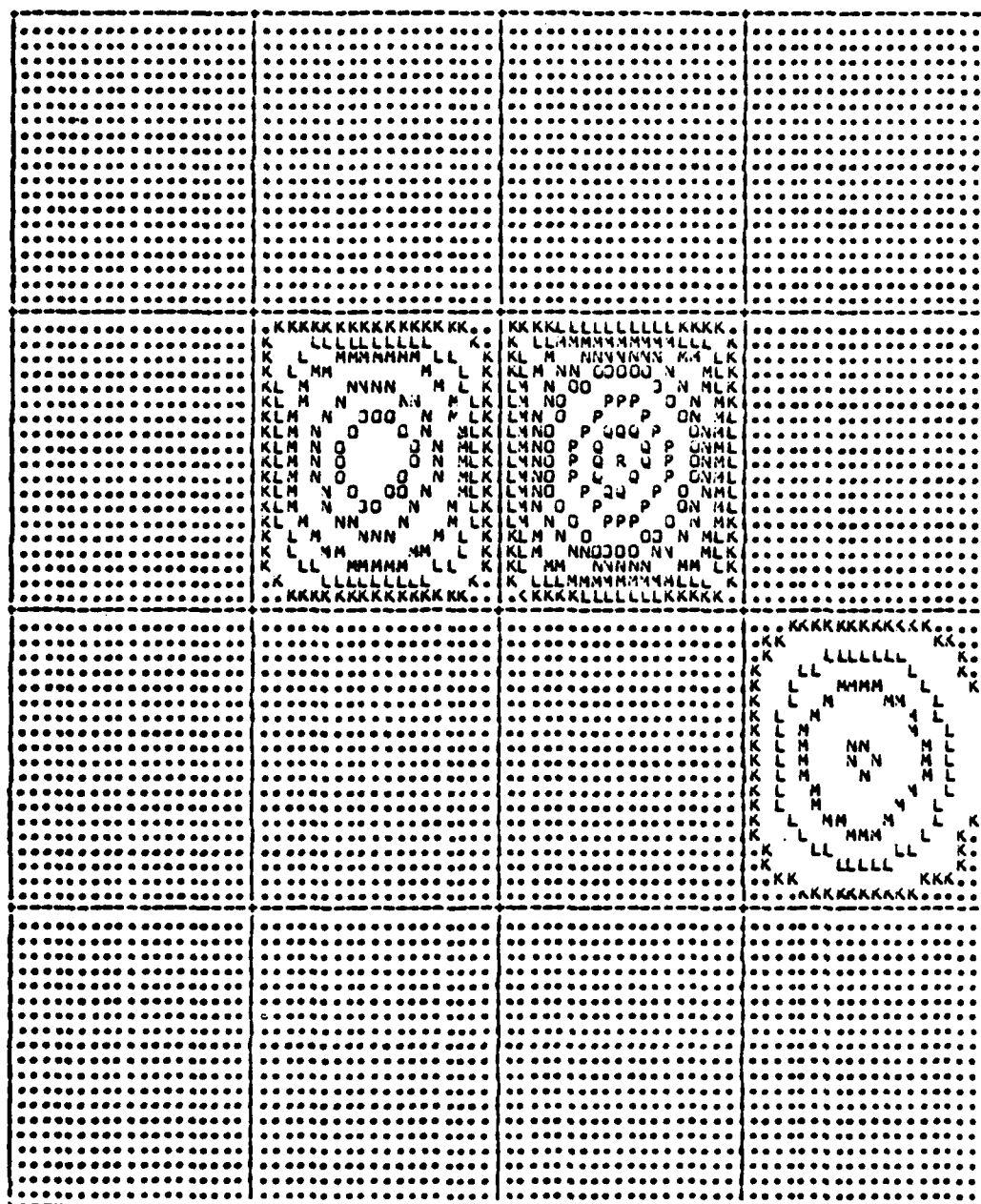


Figure 4.1 Test Data Base Configuration

and increasing distances between elevation data points. The latitude and longitude may be changed to represent changing ratios of MPPLON and MPPLAT in different latitudes. The heights of the three pyramids may be varied from zero to an arbitrarily large value as long as the ratio of heights remains as previously described. This last change is accomplished by changing the value of a height multiplier which is applied to all elements in the matrix. As originally designed, the pyramids had heights of 25, 50 and 100 meters. By using a multiplier value of ten the heights were increased to 250, 500 and 1000 meters while the sea level plane, of course, remained constant. In this manner it is possible to alter the data base to represent a level plain or ocean surface, an area of moderate terrain variation or one in which there are radical elevation changes. The obvious advantage of using this type of data base for verification is that it is a test pattern which may be easily modified by the user to suit a particular scenario.

The FLY EXEC is used to define the necessary files and execute TERR. It should be noted that FLY defines output files on a temporary "D" disk, so the user should acquire temporary storage prior to executing TERR. Once the D disk has been defined, the user need only type "FLY TERR" and press the ENTER key to execute the program. The resulting output file is a MASK DATA file identical in format to one produced by TRANS or COMBIN.

#### C. RADAR HORIZON TEST

The radar horizon test checks the ability of MASK to accurately predict the radar horizon on a smooth earth surface. This test was chosen because there is an established method, independent of any calculations used in

MASK, of determining the radar horizon for a smooth earth. Use of the smooth earth removes terrain features from the process, but does not diminish the validity of the test, since the curvature of the earth's surface serves as a replacement for terrain features. In fact, the angular and height measurements required to predict the radar horizon on a smooth earth involve the discrimination of values which are very close to one another and pose an added challenge to the model.

The independent method of predicting the radar horizon, HR, uses equation 4.1,

$$HR = \text{SQRT} (2 \times KA \times h), \quad (\text{eqn. 4.1})$$

where KA is the equivalent earth radius and h is the height of the antenna. For the test, KA will be assumed to be four-thirds earth radius. The test data base is set at an interval of 6 arcseconds at latitude 46 and the height multiplier is set to zero, producing a sea level plain 40 nautical miles by approximately 27.8 nautical miles.

For the test, MASK uses three sites with varying antenna heights. To facilitate measurement of the distances to each MASK horizon, the sites are located in the corners of the data base. The southeast site has a 200 foot antenna, the northeast has a 100 foot antenna and the southwest has a 50 foot antenna. The gradient is set to -039 and zero ducting height to simulate the four-thirds earth radius used in equation 4.1. Since the target is a point on the ground, the strike altitude used by MASK is zero feet AGL and the MSL output is blanked.

If MASK performs correctly, the results should conform to those obtained by using equation 4.1. For antenna heights of 200, 100 and 50 feet and KA

equal to four-thirds earth radius the resulting radar horizons are, respectively, 17.4, 12.3 and 8.7 nautical miles from the sites. As an aid in distance measurement it should be noted that the grid marks on the MASK output in this case are spaced ten nautical miles apart in latitude and approximately seven miles apart in longitude, with each display element occupying an area approximately .5 by .35 nautical miles. A brief inspection of Figure 4.2 shows clearly that the output conforms to the predictions obtained using equation 4.1.

#### D. TERRAIN MASKING TEST

The second verification procedure makes use of the fact that the tallest pyramid is exactly twice the height of the next shorter one. In order to perform this test the data base must be made to behave like a flat earth. This allows the use of some simple geometric relations to test MASK's calculations. Creation of this situation only requires that a value of -156 be used for the value of  $dN/dh$ . This produces a terrain model whose radius of curvature is about 160 times that of the earth, effectively flattening the data base.

The test data base has a transformation interval of 9 arcseconds and a southwest corner location of 46 degrees north and 123 degrees west. This produces a data base 60 by approximately 42 nautical miles with grid markings spaced every 15 minutes of arc. The pyramid height multiplier is equal to ten, giving the northwest pyramid a height of 500 meters (1640 feet) and the northeast a height of 1000 meters (3280 feet).

The test scenario is depicted in Figure 4.3. The site is located to the north of the two tallest pyramids. The distance from the site to a point on the plane directly beneath each peak is defined as  $B$  and is the

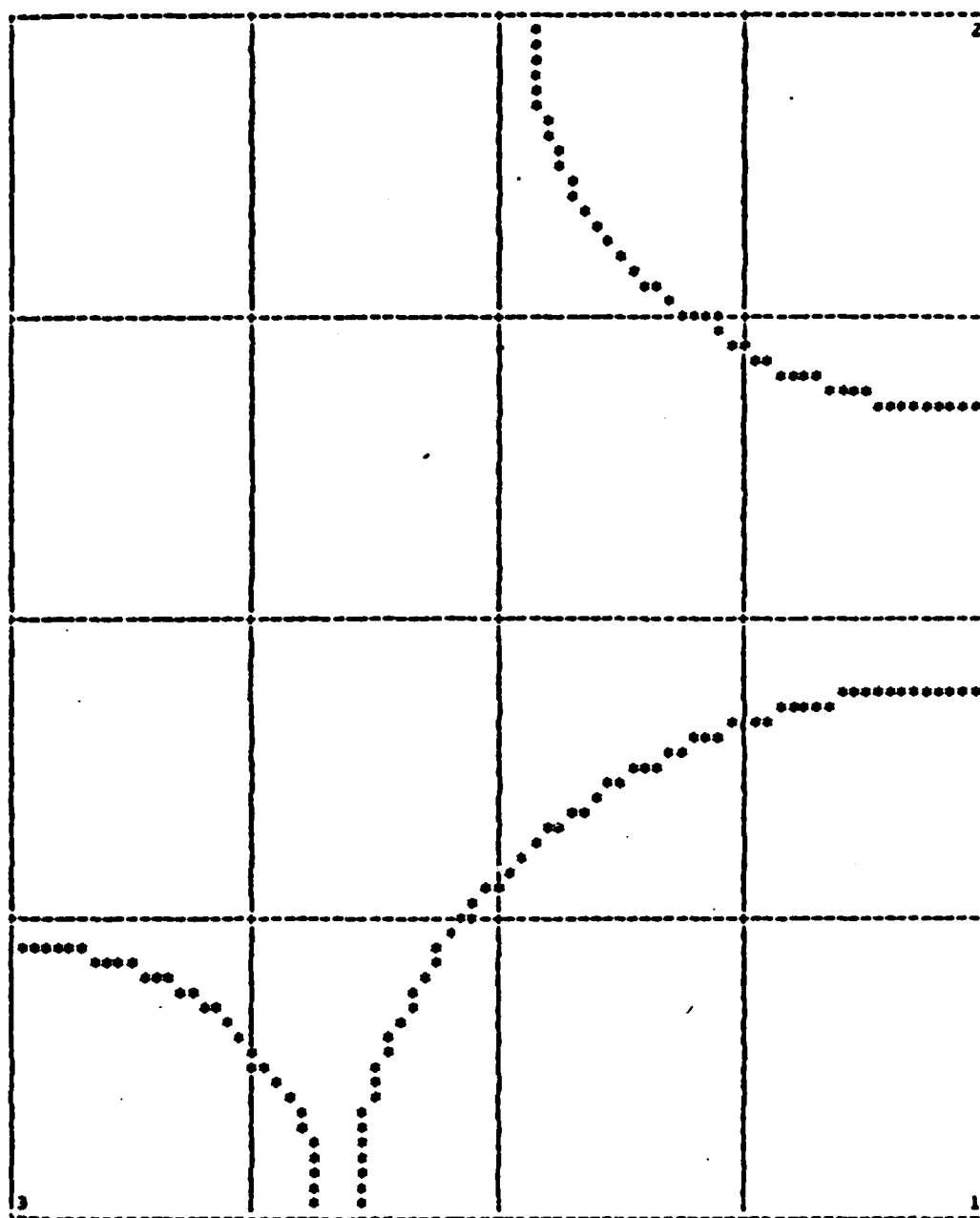


Figure 4.2 Radar Horizon Test Results

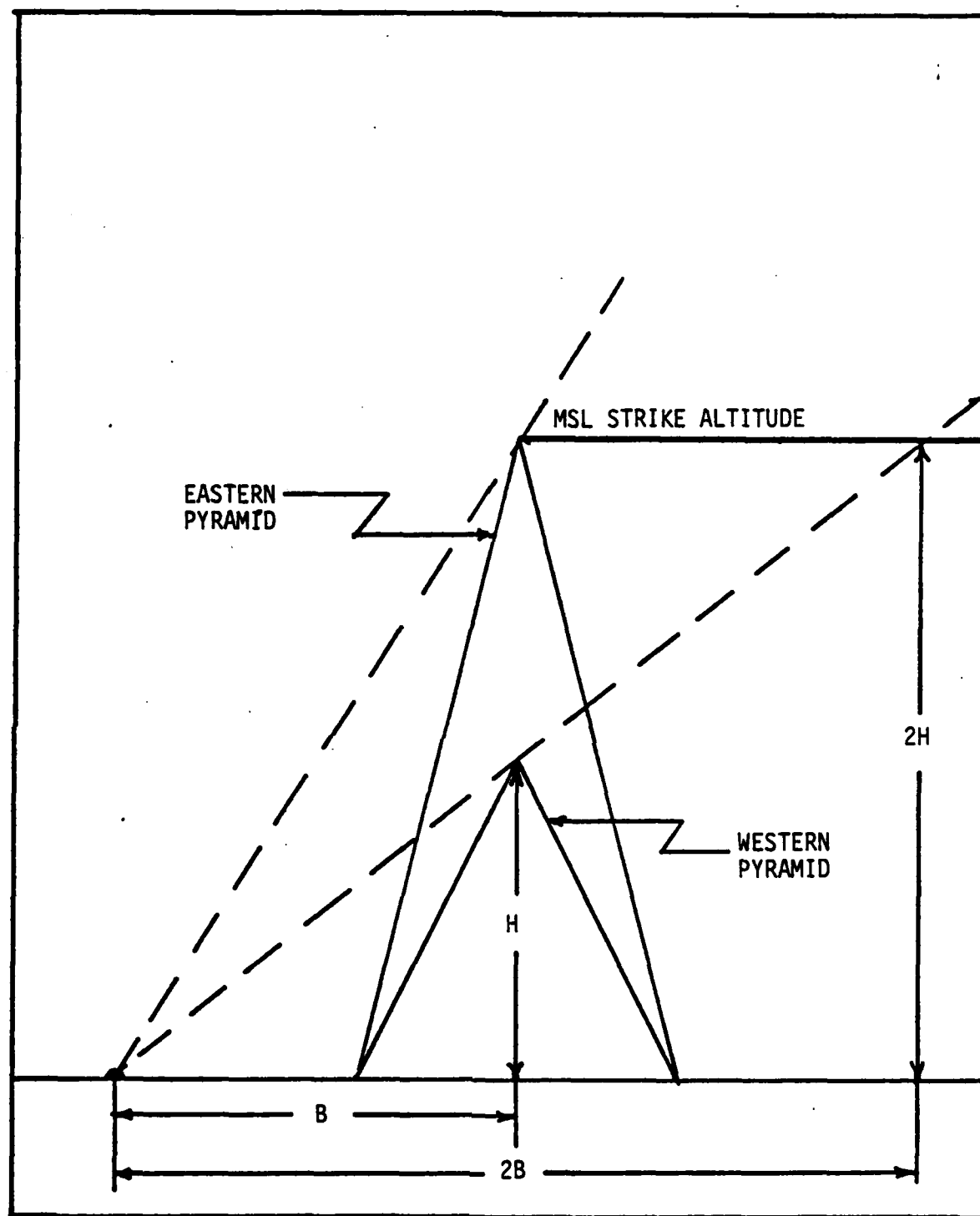


Figure 4.3 Terrain Masking Test Scenario



same for both pyramids. The height of the shorter pyramid is  $H$ , and the height of the taller one is  $2H$ . The altitude of the target aircraft is also  $2H$ , so that there is no separation between the target and the taller peak when the aircraft passes over it. Each pyramid is illuminated by the site and casts a V-shaped radar shadow at the given MSL altitude of  $2H$ . In the case of the taller pyramid, the apex of the shadow is located exactly at the peak and the ground distance from site to apex equals  $B$ . In the case of the shorter pyramid, the apex of its shadow meets the MSL altitude at a greater distance south of the peak. By using similar triangles it can be seen that since the height of the shorter pyramid is  $H$ , the distance required for the shadow to reach a height of  $2H$  is exactly  $2B$ , or twice the distance encountered in the case of the tallest pyramid. If MASK performs correctly, this relationship should be duplicated on the MSL display.

For this test MASK uses a site location of 46 degrees, 55 minutes north and 122 degrees, 30 minutes west, which equates to midway between the two northern peaks and 17.5 minutes north of a line connecting the two. The site elevation is set to zero,  $dN/dh$  is  $-156$ , ducting height is 99999 and the strike altitude is set at 3280 feet MSL ( $2H$ ). The AGL display is not needed. The output from this run is shown in Figure 4.4. The MSL display is annotated to show the locations of the two northern peaks and the lines from the radar site to the apex of each shadow. Note that the apexes do, in fact, lie on the lines extending from the site through the peaks of the pyramids. In addition, the apex of the eastern shadow is located at the position of the eastern peak, as desired. The apex of the western shadow is located at a distance away from the site equal to twice

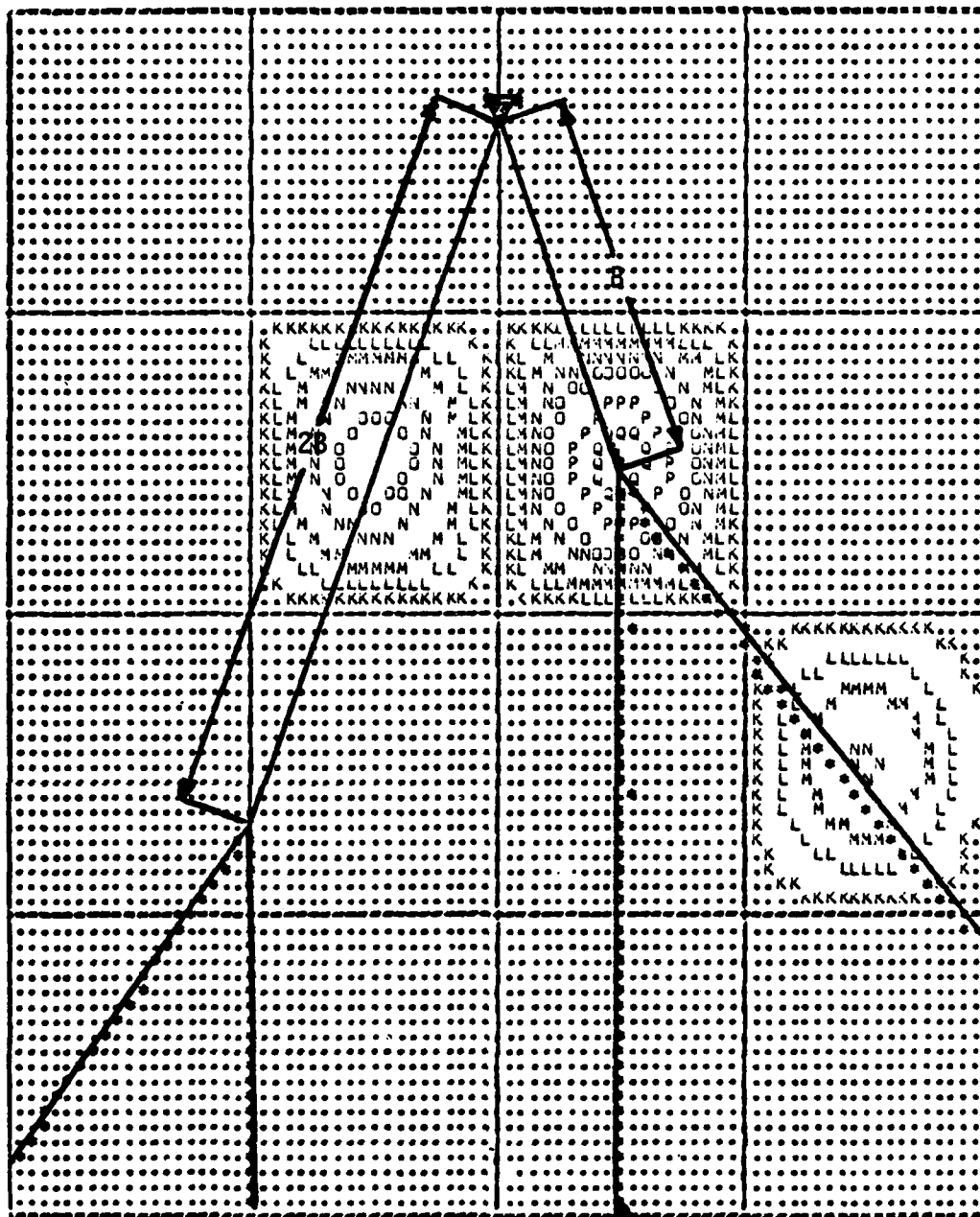


Figure 4.4 Terrain Masking Test Result

the distance from the site to the eastern apex. Clearly, the situation predicted by the test scenario is duplicated by the MASK output.

Other verification methods are, no doubt, possible. However, these two tests are sufficient to show that MASK does accurately perform its calculations using the test pattern as a data base.

## V. EXAMPLE PROGRAM PROCEDURES

### A. GENERAL

This chapter presents examples of the procedures required to execute a MASK program. The sequence runs from accessing the DTED tape, through the transformation and combining steps and finally to the execution of MASK. In addition, a section is devoted to interpreting the MASK output. Following the procedural review, several examples of MASK output are shown to illustrate the effects of varying MASK input parameters. All computer programs referred to in this section are contained in Appendix A. All procedures refer to executing the various programs using the IBM 3033 system at the Naval Postgraduate School. Single quotation marks are used to denote that the text within the quotes is to be entered as an input value or used as a name.

### B. SCENARIO

This example of MASK supports a hypothetical air strike against the Deception Pass highway bridge which links Whidbey Island in Puget Sound to the mainland. The bridge is located at latitude 0482400 north, longitude 1223900 west. The bridge is defended by a surface-to-air missile system located at latitude 0482000 north, longitude 1223900 west. The radar has two PRF's which do not operate simultaneously, but are used for different ranges to targets. The long range PRF is 1250 pulses per second. The exact site elevation is unknown and the mast height is estimated to be 20 feet. In addition to the SAM radar, there is an early warning (EW) radar near Bellingham, at latitude 0484800 north, longitude

1223200 west. It has a 100 foot mast height and a PRF of 400. The IREPS computer predicts a value of  $dN/dh$  equal to -050, indicating no ducting but slightly greater than normal refraction.

The strike leader has proposed that the attacking aircraft take off from their base at Tumwater, rendezvous at 7000 feet with chaff, jamming and anti-radiation strike elements and proceed north to bomb the bridge. Prior to reaching the immediate target area the bombers are to descend to 200 feet above ground level while the other strike elements maintain 7000 feet MSL, in order to decoy the defenses and launch anti-radiation missiles. The route of flight must allow the low altitude bombers to get as close to the bridge as possible while avoiding radar detection. The strike leader needs to know how soon his bombers must descend, how close they can get to the bridge without being detected and where the other elements must be positioned to be most effective.

The planning procedure for MASK is to examine the target area at high resolution and then expand the area coverage as required to encompass the early warning radar to the north and the rendezvous point located near Tumwater at latitude 0470500 north, longitude 1225500 west. This requires the sequential use of a 20 by 20 minute square data base centered on the SAM site, a 40 by 40 minute data base covering both radar sites, a one degree square data base with a southwest corner point at 48 north, 123 west and a two by two degree data base running from 47 to 49 north and 122 to 124 west. In practice, all of these data bases would probably not be required, but this example accounts for most of the operations that a user is likely to perform.

### C. TAPE DATA TRANSFER

By referring to Figure 3.3, the user finds that the tapes required are S-798 and S-796, which cover the latitude bands from 47 to 49 degrees north. The data files required are file numbers 2 and 5 on each tape. The file containing the data at the target is in S-796, number 5 and is the first file to be transferred. The other three files will only be needed for the largest of the data bases.

#### 1. PROFILE Exec

The PROFILE exec performs three operations which are required in preparation for the transfer of tape data. It defines a file called DSN S1086 DATA which is used to transfer the tape data into MVS on a temporary C disk and another file called TAPE DATA D1 which stores the data on the user's temporary D disk as it is transferred from MVS to the user. A final operation is the definition of the temporary D disk which has 20 cylinders of capacity and can hold three full DTED data files. Two final operations are required to be performed by the user. The first is to link to MVS by entering 'LINK MVS 1E3 291 RR' and the second is to access 291 as the C disk by entering 'ACC 291 C'. After the tape transfer is complete the user should release the C disk by entering 'REL 291 (DET'.

#### 2. GETTAPE

The actual tape transfer to MVS is accomplished using the GETTAPE program. The user must edit the job control language (JCL) in three areas of the program. The first change is in the fifth line where 'VOL=SER=xxxx' appears. The 'xxxx' must be changed to the tape volume number desired. In this case it is changed to S796. The next change is in line six where 'LABEL=(xx,BLP)' appears. The file number is inserted here, so in this

case '05' is used. The last change depends on whether or not this is the user's first tape transfer operation of the day. In line eight 'DISP=(xxx, KEEP)' appears. If this is the first transfer of the day, the user must enter 'NEW', but for all subsequent transfers for that day 'OLD' must be entered. If this change is not made for the later transfers, a duplicate label JCL error will cause the transfer to abort. Once these changes are made GETTAPE is submitted and the transfer takes place. Progress of the job in the batch system may be monitored by entering 'INQ GETTAPE' to which the computer responds with a coded message indicating the current state of the job. The user is notified of the completion of transfer when two bold messages appear on the screen indicating that two files have been spooled to his reader. To read the files, 'RDR' is entered after which the computer asks for a filename and filetype for each file. These names are not important since the files will be erased shortly, so 'X X' and 'Y Y' may be used. The files will be transferred to the user's A disk and can be browsed using the FLIST commands. A successful transfer results in a file which reads '1DATA SET UTILITY-GENERATE-PROCESSING ENDED AT EOD'. The second file is a summary of the transfer operation, the only important line of which is the sixth line below the GETTAPE JCL code. A successful transfer is indicated if this line reads 'STEP WAS EXECUTED-COND CODE 0000'. Once the transfer occurs, the command 'MOVEFILE' is entered to transfer the data from MVS to the D disk. At this time the C disk may be released unless further transfers are planned. The DTED file containing the degree square of data now resides on the D disk and is accessible to the transformation program.

## D. DATA TRANSFORMATION

### 1. TRANS

All transformations are done using the TRANS program which is executed by the FLY EXEC. FLY compiles, loads and runs the program in addition to defining the MASK DATA D1 file into which TRANS loads the transformed data base.

The first MASK DATA file required is the high resolution data centered on 0482000 north, 1223900 west. This data base will span 20 minutes of latitude and longitude, so the appropriate southwest corner is ten minutes south and west of the center or 0481000 north, 1224900 west. The desired transformation interval is three arcseconds.

TRANS is executed by entering 'FLY TRANS'. The FLY exec then displays the compilation messages and FILEDEFs currently in effect. The first input prompt message asks for the desired transformation interval to be entered in columns 1-2. A brief explanation is provided to remind the user of the permissible interval values and the resulting data base dimensions. The user enters '03'.

The next message requests the latitude and longitude of the parent DTED file's southwest corner. The first entry specifies the hemisphere of latitude and the input required is either 'NN' for north of the equator or 'S' for south. The user enters 'NN'. The next prompt requests the latitude value of the corner in degrees, minutes and seconds (DDMMSS). The user enters '0480000'. The next two messages ask for the hemisphere and value of the longitude of the corner. The user enters 'W' and then '1230000'.



The last two entries requested are the latitude and longitude of the southwest corner of the area to be transformed. In all cases, the hemisphere specification is the same as that of the parent data base, so only the values are requested. The user enters '0481000' and then '1224900'.

TRANS executes and produces the desired MASK DATA file which is stored on the user's D disk. At this time, MASK may be executed. For the sake of organization, however, the user may desire to perform the transformations for all of the required data bases prior to running MASK. If another transformation is to be made prior to executing MASK it is imperative that the existing MASK DATA D1 file be renamed. Otherwise, it will be overwritten by successive transformations. In this example the three arcsecond data base is renamed 'M03 DATA D1' and the next transformation is begun.

The next MASK DATA file to be created uses a six arcsecond interval with a southwest corner chosen so that both the SAM and EW radars fall inside the resulting 40 minute square of data.

As mentioned earlier, some of the transformations in this example may, in practice, be omitted. For example, the user may opt to forego the six arcsecond transformation and go to the nine arcsecond one for the next data base. The terrain characteristics and the tactical situation will determine which data bases are required for any given strike. It is recommended, however, that the three arcsecond data base be used first for each planning evolution since it provides the highest resolution and gives the most accurate value for the site elevation.

The six and nine arcsecond transformations are performed in exactly the same manner as the first one. In order to ensure that both radars are included in the six arcsecond data base a southeast corner is

chosen at 0481000 north, 1225200 west. This data base is renamed 'M06 DATA D1'. The nine arcsecond data base uses 0480000 north, 1230000 west as its corner location and is renamed 'M09 DATA D1'. This last data base covers the largest area which can be produced by TRANS alone. The remaining two by two degree data base requires the use of COMBIN.

## 2. COMBIN

### a. Overview

The procedure for using COMBIN consists of four separate operation. The first is the transfer of the desired DTED data from tape to the D disk. Since one DTED file has already been transferred, three more remain. Next, the data is transformed at an interval greater than nine. Following this, the individual files are assigned to specific FILEDEFS based on their relative geographic positions. Lastly, COMBIN is executed and produces a MASK DATA D1 file incorporating the data from all of the component files.

### b. Tape Transfer

Tape transfer is accomplished exactly as before, except that the GETTAPE JCL must be updated to conform to the desired tape volume and file numbers and the disposition must be amended to 'OLD,KEEP'. In this example, the user need not change the volume number right away since the S-796 tape is used again, but the file label number must be changed from '05' to '02'. To transfer the remaining two files on tape S-798, the volume identifier must, of course, be changed.

As a practical matter the tape transfer of the second DTED file should be postponed momentarily. The reason is that the first TAPE DATA D1 file is still on the D disk and will be overwritten if a subsequent

tape file is transferred. The most efficient procedure is to transfer the first file as previously described, then amend the GETTAPE JCL for the next file and submit GETTAPE. During the time required for GETTAPE to transfer the tape file to MVS the user performs the appropriate transformation of the existing TAPE DATA D1 file and renames the resulting MASK DATA D1 file. By this time, the prompt message should arrive indicating that the second file is ready to be moved from MVS to the D disk. If the file is sent to MVS before the user is ready for it, the file will remain in MVS until the user has completed the last transformation. In any event, the new file will not be transferred onto the D disk until the user commands 'MOVEFILE', at which time the new file will overwrite any previous data on the TAPE DATA D1 file. Following the 'MOVEFILE' command the user again amends the GETTAPE JCL and renews the cycle which continues until all required files have been processed.

#### c. Transformation

The second operation in the combining procedure is the transformation of the TAPE DATA D1 file. This is accomplished using TRANS as before, except that the transformation interval is increased. For this example an interval of 18 is used during the combining process. Upon commanding 'FLY TRANS' a message will appear asking for the interval. The user enters '18'. The latitude and longitude of the corners of both the parent DTED file and the desired area of transformed data are entered, keeping in mind that when transforming data for use by COMBIN the corner position of the transformed data base will always be the same as the parent file. The MASK DATA file produced by TRANS is, in this case, one quarter the size of a normal MASK DATA file.

#### d. FILEDEF Assignment

The next operation is FILEDEF assignment. The user must assign each transformed file to an appropriate FILEDEF based on the geographic position of the file relative to its neighbors. In the combining process FILEDEFs are assigned sequentially from west to east starting with the northern squares and moving southward. In the current two by two degree example, the data from S-796 number 2 is assigned to FILEDEF 11, S-796 number 5 to FILEDEF 12, S-798 number 2 to FILEDEF 13 and S-798 number 5 to FILEDEF 14. Combinations of more squares follow the same pattern with the northwestern file assigned the lowest FILEDEF number and the southeastern one the highest. The FILEDEFs for all permissible data bases up through a five by five degree square are contained in the FLY EXEC. FILEDEFs 11-14 are reserved for the two by two square, 15-30 for the four by four and 31-55 for the five by five. Each component file is identified according to the pattern 'Mxyyyzz DATA D1', where 'xx' is the southwest corner latitude in degrees, 'yyy' is the longitude and 'zz' is the interval of transformation used. In this example, FILEDEF 11 reads 'M4812418 DATA D1', FILEDEF 12 reads 'M4812318 DATA D1' and so on. Therefore, the first 18 arcsecond data file transformed in this example is renamed 'M4812318 DATA D1' prior to transferring the next file from MVS. After this operation the first TAPE DATA D1 file is no longer needed and may be ~~overwritten~~ or erased as desired.

#### e. Combining Files

At this point in the example all four DTED files have been sequentially transferred from tape, transformed and assigned to appropriate FILEDEFs. The user now enters 'FLY COMBIN'. The first prompt message is

a summary of the required transformation and FILEDEF assignments just described. The next message requests the transformation interval used on the component files. The user enters '18' in this case. The next four messages ask for the hemispheres and values of the latitude and longitude of the southwest corner of the desired combined data base. In this example the user enters the four responses 'NN', '0470000', 'W' and '1240000'. COMBIN then combines the previously transformed component files and produces a MASK DATA file on the D disk. In order to differentiate this data base from the others the nomenclature 'Cxyyyzz DATA D1' is used where 'xx' and 'yyy' are the latitude and longitude of the data base southwest corner and 'zz' is the number of degree squares contained in the file. In this case, the user renames the file 'C4712404 DATA D1'. There are now four data bases of varying resolution stored on the D disk ranging from the 20 by 20 minute square to the two by two degree combined data base.

## E. EXECUTING MASK

### 1. Input Data

The user is now prepared to execute MASK. The high resolution M03 DATA D1 file is selected for processing first and is renamed 'MASK DATA D1'. The user commands 'FLY MASK' and the input prompt messages begin. The first four messages request the hemispheres and values of the latitude and longitude of the first radar site. The user inputs the four separate responses 'NN', '0482000', 'W' and '1223900'. The next message asks for the elevation of the first site in feet MSL. If the elevation is not known, the user enters '-9999'. In this example '-9999' is the correct response. The next message asks for the first site antenna mast height above the ground. If this value is unknown a response of '-99' sets the height to a value of

five meters. In this example, '020' is entered. The last radar site parameter requested is the first site radar PRF. If the user does not desire a maximum unambiguous range limit imposed, the proper response is '-999'. In this example the correct entry is '1250' since this PRF provides the longest range capability. The next message asks whether or not the user wants to enter additional radar sites. If so, the response is '1'; otherwise a '0' is entered. The user enters '1', since the EW radar remains to be input and the radar input parameter sequence is repeated. The correct entries for the second site are 'NN', '0484800', 'W', '1223200', '-9999', '100' and '0400'. Since a third radar site is not desired, the user enters '0' in response to the additional site message.

The strike altitudes are input next. The first message in this phase asks for the AGL strike altitude in columns 1-4. If no AGL display is desired '-999' is entered. Since the AGL display is needed the user enters the proposed strike altitude of '0200'. The next message requests the MSL altitude desired. If no MSL display is desired '-9999' is entered. The MSL display is needed in this example so '07000' is entered.

The refractive inputs are entered at this point. The prompt message requests the value of  $dn/dh$  in N-units per kilometer including the sign and lists -156 as the minimum permissible value. A value of -039 is used for the standard radar refractive gradient and -020 is the value used to obtain standard day optical refractive effects. Since the IREPS program predicts a  $dn/dh$  of -050 through 7000 feet MSL, '-050' is entered. The next message asks for the ducting height. This value is used as the upper altitude bound for applying the input value of  $dn/dh$ . At altitudes above this value,  $dn/dh$  automatically reverts to the standard value of -039. If IREPS had predicted ducting, the user would input the predicted height, but

AD-A136 771

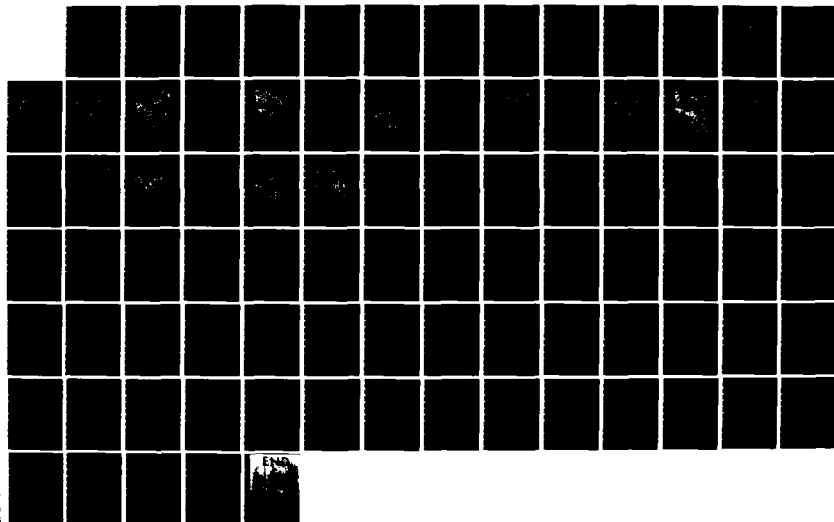
MASK: A TACTICAL AID FOR PLANNING AIR STRIKES AGAINST  
RADAR DEFENDED LAND TARGETS(U) NAVAL POSTGRADUATE  
SCHOOL MONTEREY CA D B MCKINNEY SEP 83

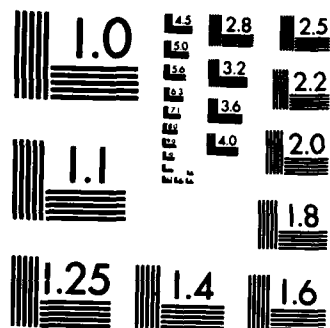
2/2

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NL





MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS-1963-A



since this is not the case the user enters the upper altitude for which  $dN/dh$  was calculated or '07000'.

The last input required is the selection of the topographic display. If the user desires the display, a '1' is entered. Otherwise, a '0' is used. In this case the user enters '1'.

MASK now begins its calculations based on the inputs. For each two seconds of CPU run time the word 'CRANKING' appears on the screen. When the calculations for any given site are finished a message will appear on the screen stating, 'CALCULATIONS COMPLETE FOR x OF y RADAR SITES', where 'x' is the number of sites processed thus far and 'y' is the total number requested. When 'x' equals 'y' the calculations for all sites are complete and the results are stored in the MASK OUT D1 file. To browse the output, the user enters 'FLIST \*\* D' and uses standard FLIST commands. To print the output from FLIST, the command 'PRINT /CC' is used. After running MASK using the high resolution data base, MASK DATA D1 is renamed 'M03 DATA D1' and M06 DATA D1 is renamed 'MASK DATA D1'. MASK is again executed with the new data base and the output is spooled to the printer. This sequence is repeated for each of the data bases in turn and then the output is analyzed. It is prudent in most cases not to erase data bases after they have been used by MASK, since it is likely that some additional runs will be required due to strike altitude modifications based on the initial output or additional intelligence on the threat.

## 2. Output Analysis

### a. Topographic Displays

The topographic display consists of an 80 by 80 character matrix displaying terrain features and a short legend explaining the elevation code. Figure 5.1 shows the elevation code legend. All

CODED TOPOGRAPHIC MAP OF AREA  
 SOUTHWEST CORNER IS W 1230 000 NN 4800 00  
 GRID SPACING=15 MINUTES.

SYMBOL	LEGEND ELEVATION (METERS)
•	SEA LEVEL
K	50
L	100
M	200
N	300
O	500
P	700
Q	900
R	1100
S	1300
T	1500
U	1800
V	2100
W	2400
X	2700
Y	3000
Z	3000 PLUS

Figure 5.1 Topographic Display Legend

elevation values are in meters above sea level. The code symbol represents the upper limit of the elevation. For example, the '.' represents all areas which are at or below sea level, while the 'K' represents all areas which are above sea level but less than or equal to 50 meters. The only exception to this rule is the symbol 'Z' which represents areas greater than 3000 meters. Areas which are blank fall in the same elevation bin as the lowest symbol which borders on them. Blank areas correspond to areas where the terrain variation is very slight such as broad valleys or plains.

In the runs of MASK four separate topographic displays were created at various levels of resolution. The first of these was a high resolution 20 by 20 minute display centered on the SAM radar site. This display is shown in Figure 5.2. The display has been annotated to show the radar site in the center of the display and the target bridge due north of the site. This display shows the relatively flat terrain in the immediate vicinity of the site. The ground elevation rises gradually to the south, more steeply to the east and some substantial elevation changes are indicated by the denser code on the northern side of the bridge. The shoreline is easily discernable. Each symbol in the display is approximately one quarter of a nautical mile in height and each grid box is five nautical miles long and approximately three and a third nautical miles wide.

The next topographic display created was the 40 by 40 minute area which included both radar sites and is shown in Figure 5.3. This display covers four times the area of the previous one and gives a better idea of the overall nature of the terrain surrounding the target. The islands to the northwest of the bridge are seen to rise steeply to

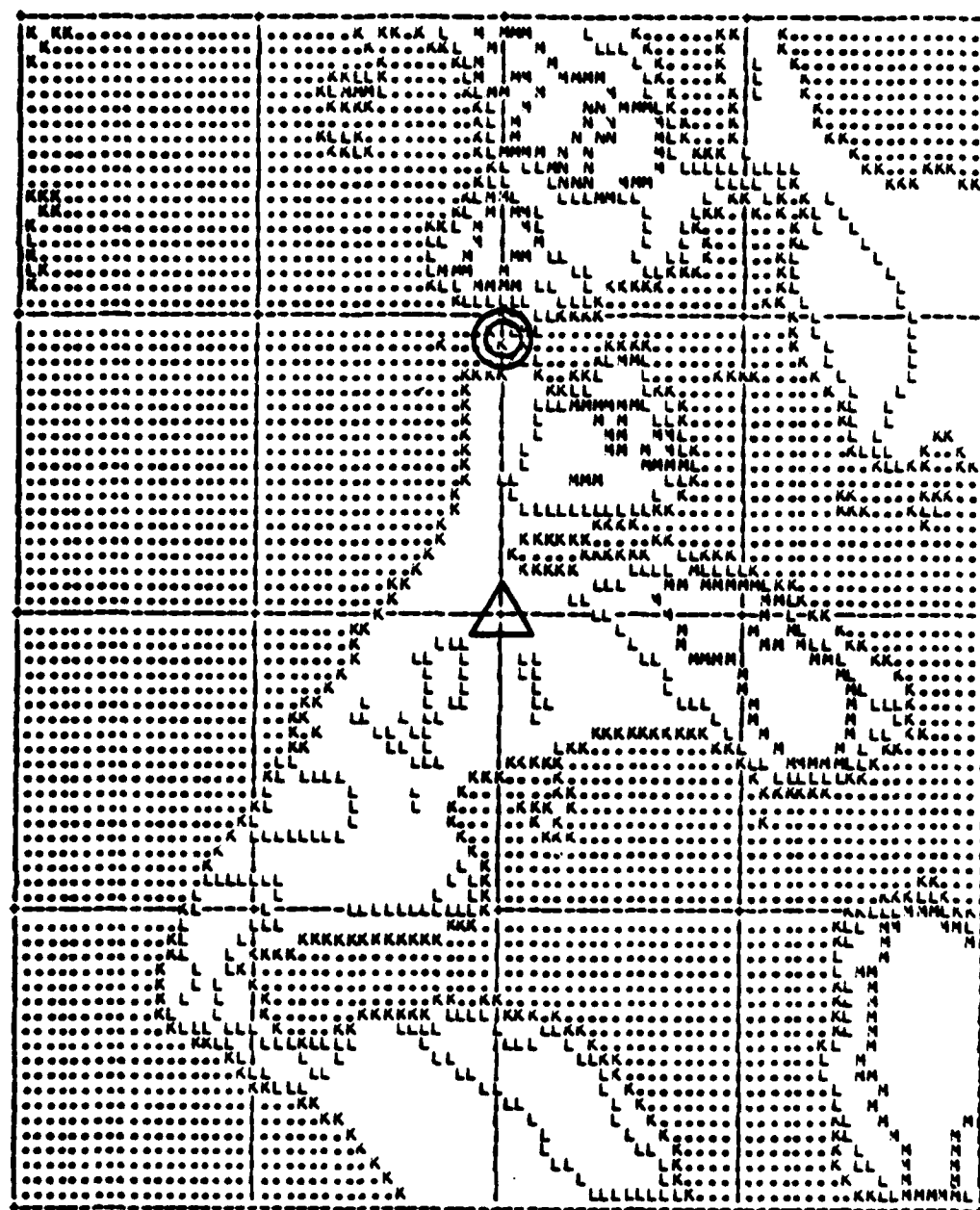


Figure 5.2 20 Minute Square Topographic Display

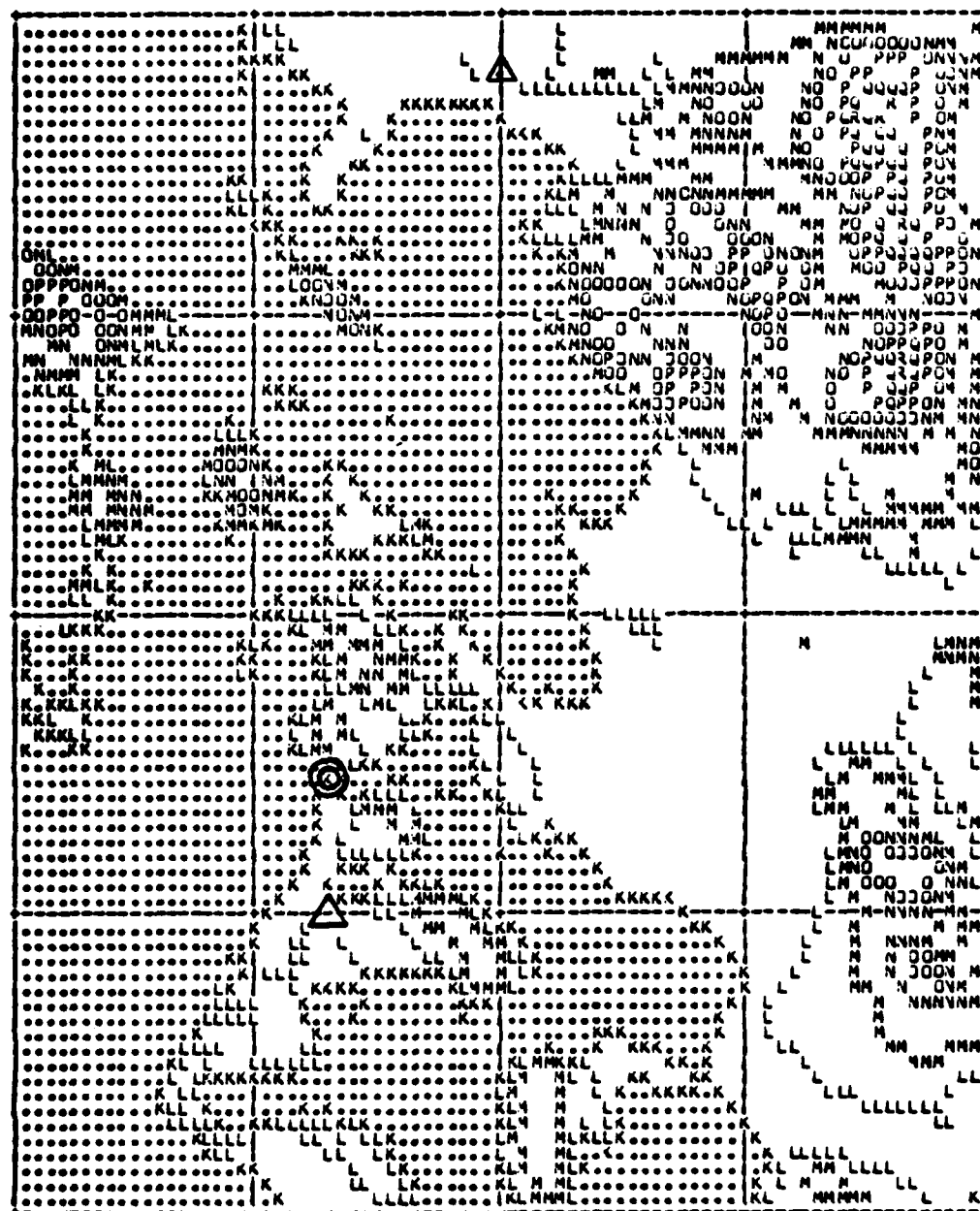


Figure 5.3 40 Minute Square Topographic Display

elevations as high as 700 meters (2300 feet) above the sea. The mainland is essentially flat with a prominent mountainous area in the northeast corner and a lower set of hills near the southeast corner. These are the foothills of the Cascade Mountains.

The next topographic display is shown in Figure 5.4. It covers an area nine times the size of the first and again shows the flat coastal areas with mountainous terrain to the east. A major river valley separates the two areas of high terrain and extends eastward from the coast halfway up the display. Another area of steep terrain has appeared across a straight from the radar site in the southwest corner of the display.

The final topographic display covers a two by two degree square area and is shown in Figure 5.5. The mountainous area which first appeared in the southwest corner of the previous display has emerged as a significant mountain range rising steeply from the sea. This is the Olympic Peninsula. The area of water to the west of the site extending to the eastern edge of the display is the Strait of Juan de Fuca and is about 15 miles wide. The channel to the south of Whidbey Island is the southern portion of Puget Sound. This channel passes by Seattle one quarter of the way up from the bottom of the display and reaches nearly to the hypothetical rendezvous point in the middle of the bottom of the display. The southeastern tip of Vancouver Island occupies the northwest corner of the display.

These four displays will be used in conjunction with the AGL and MSL masking displays. The masking displays contain no terrain information by themselves and are designed to be traced directly onto the topographic displays for interpretation. An alternate method is to make

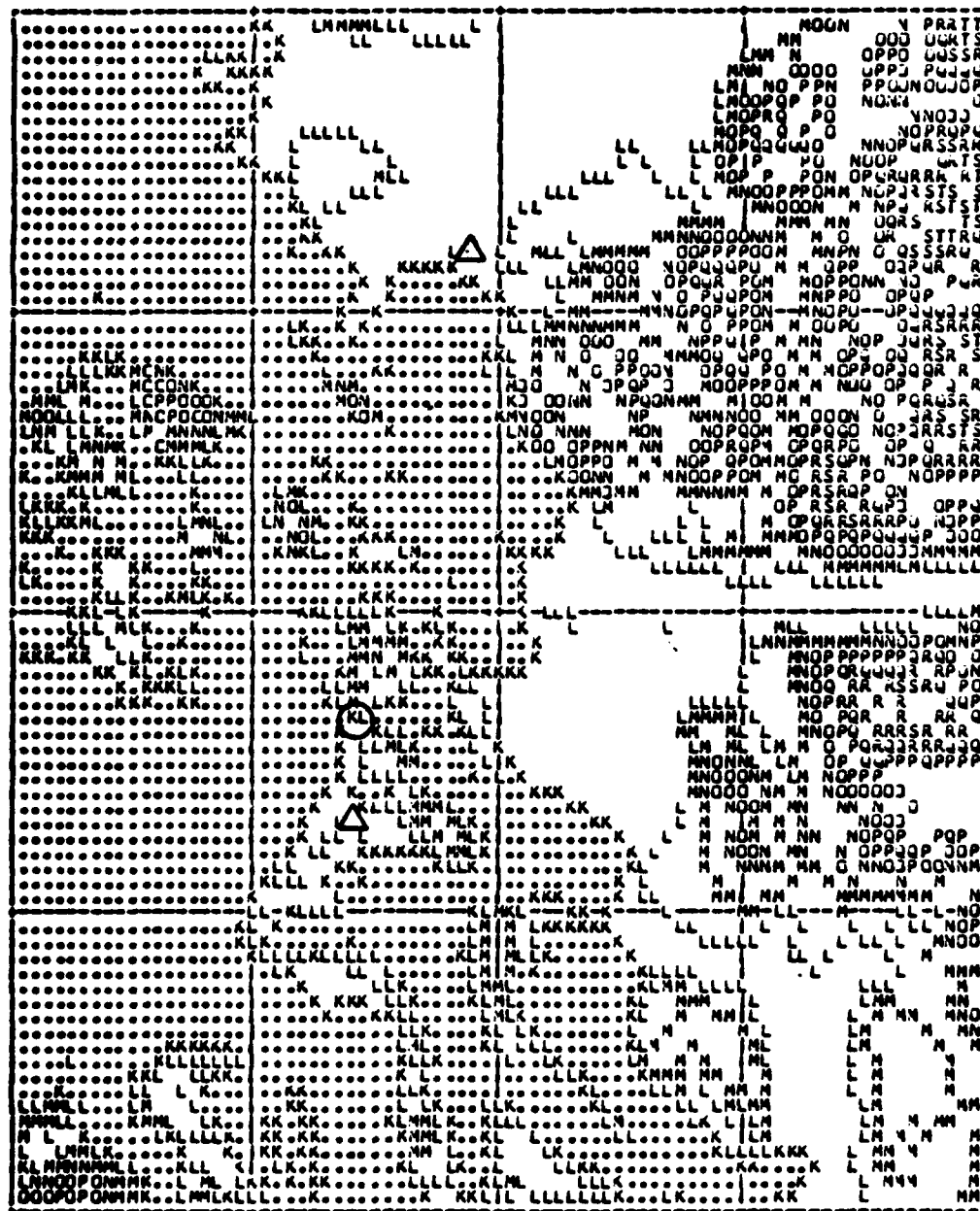


Figure 5.4 60 Minute Square Topographic Display





transparent overlays of the masking displays and place them over the topographic displays. In the remaining examples the figures shown will be combinations of the masking envelopes and the appropriate topographic displays since the envelopes by themselves are not very informative.

#### b. AGL Displays

The AGL display consists of an 80 by 80 element matrix and a descriptive page. The descriptive page contains information describing the parameters of the display, radar site parameters and a brief legend of the display matrix symbols. Figure 5.6 is the descriptive page for the first run of MASK in this example.

The AGL masking envelope for the first MASK run is shown in Figure 5.7. The envelope is based on information only from the SAM radar site. It can be clearly seen that the radar coverage extends primarily to the northwest of the site, with the areas to the south and east being masked by rising terrain. The target lies just on the border of the envelope and appears to be approachable from the east. The small unmasked area to the north of the target is formed by an isolated peak which rises steeply from the surrounding terrain. This run of MASK will be the most accurate of any in this example due to the relatively high density of data points in any given area. It will become apparent later that the interpolated value of site elevation varies between the different resolution data bases. For this reason, the user should note the elevation values from the high resolution runs and use them as inputs in following runs as required. In any event, the information from this display indicates that a strike approaching at 200 feet AGL from the south or east will be undetected until just prior to reaching the target.

**RADAR COVERAGE DISPLAY FOR STRIKE AT 200 FEET ABOVE GROUND LEVEL**

**I. DISPLAY PARAMETERS**

**SOUTHWEST CORNER OF DISPLAY: LATITUDE= 481030 NN  
LONGITUDE=1225200 W**

**GRID SPACING=10 MINUTES**

**CELL RESOLUTION: LATITUDE= 0.5005 NM  
LONGITUDE= 0.3297 NM**

**REFRACTIVE GRADIENT = -50**

**REFRACTIVE DUCT HEIGHT (FT) = 7000**

**II. RADAR SITE PARAMETERS**

SITE #	LATITUDE	N/S	LONGITUDE	E/W	ELEVATION (FEET)	PRF
1	482000	NN	1223900	W	69.21	1250
2	484800	NN	1223200	W	237.80	430

**III. LEGEND**

**##=NUMBERED RADAR SITE LOCATION**

**==ENVELOPE WITHIN WHICH AN AIRCRAFT FLYING AT  
THE SPECIFIED ALTITUDE WILL BE UNMASKED  
AND INSIDE THE RADAR MAXIMUM UNAMBIGUOUS RANGE.**

**Figure 5.6 Typical AGL Descriptive Output Page**

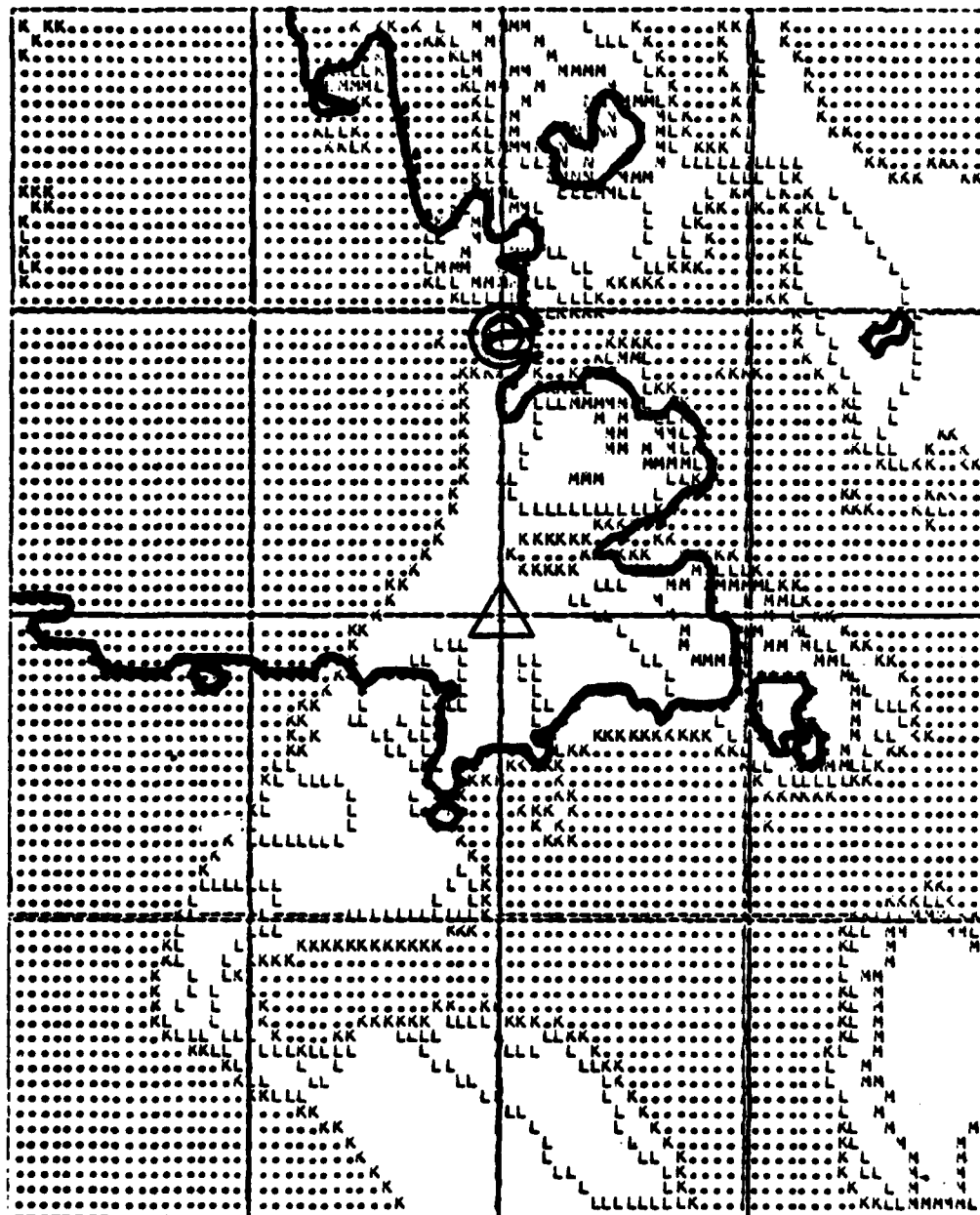


Figure 5.7 20 Minute Square AGL Display

The AGL display from the second run is shown in Figure 5.8. This display includes the masking envelopes formed by both of the radars. The most critical change in this display is the addition of an area of coverage to the east of the target provided by the EW radar. The positioning of the EW radar allows it an unimpeded field of view directly south over the water. In addition, it has increased the coverage on that part of Whidbey Island directly east of the site, making an undetected approach virtually impossible. Still, the time that the aircraft must spend in the SAM envelope is short. The area over the mainland is predominantly free of coverage due to the masking of the EW radar by the high terrain in the northwest corner. Other masked areas are caused primarily by the vertical extent of the islands to the north of the target. In particular a large, roughly diamond shaped area of masking is shown over water in the upper left of the display. This area is masked by the long thin island which forms its northeastern side. Masking boundaries in the upper half of the display are seen to extend radially from the location of the EW site. This effect is even more pronounced in Figure 5.9 which is an envelope of the coverage of the EW radar only, using the 60 by 60 minute data base. The other point of interest in Figure 5.9 is that the additional area of coverage on Whidbey Island to the east of the SAM site which first appeared in Figure 5.8 is due to the EW radar. The SAM coverage is confined to that area depicted in Figure 5.7.

The next AGL display is from the third run and is shown in Figure 5.10. There are no significant tactical points contained in this display, other than to show that the AGL coverage does not extend any farther south than was shown in Figure 5.8. From the point of view of

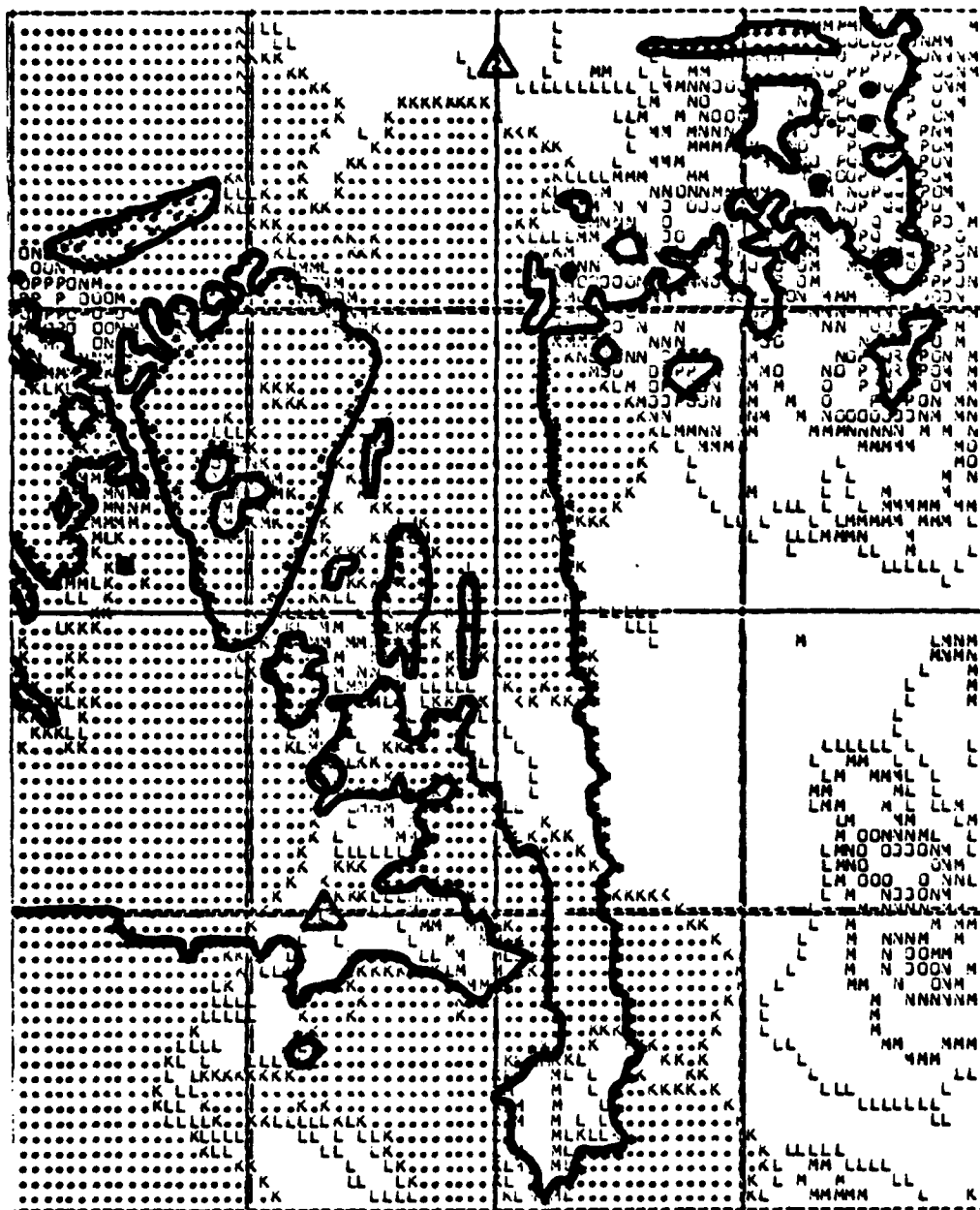


Figure 5.8 40 Minute Square AGL Display

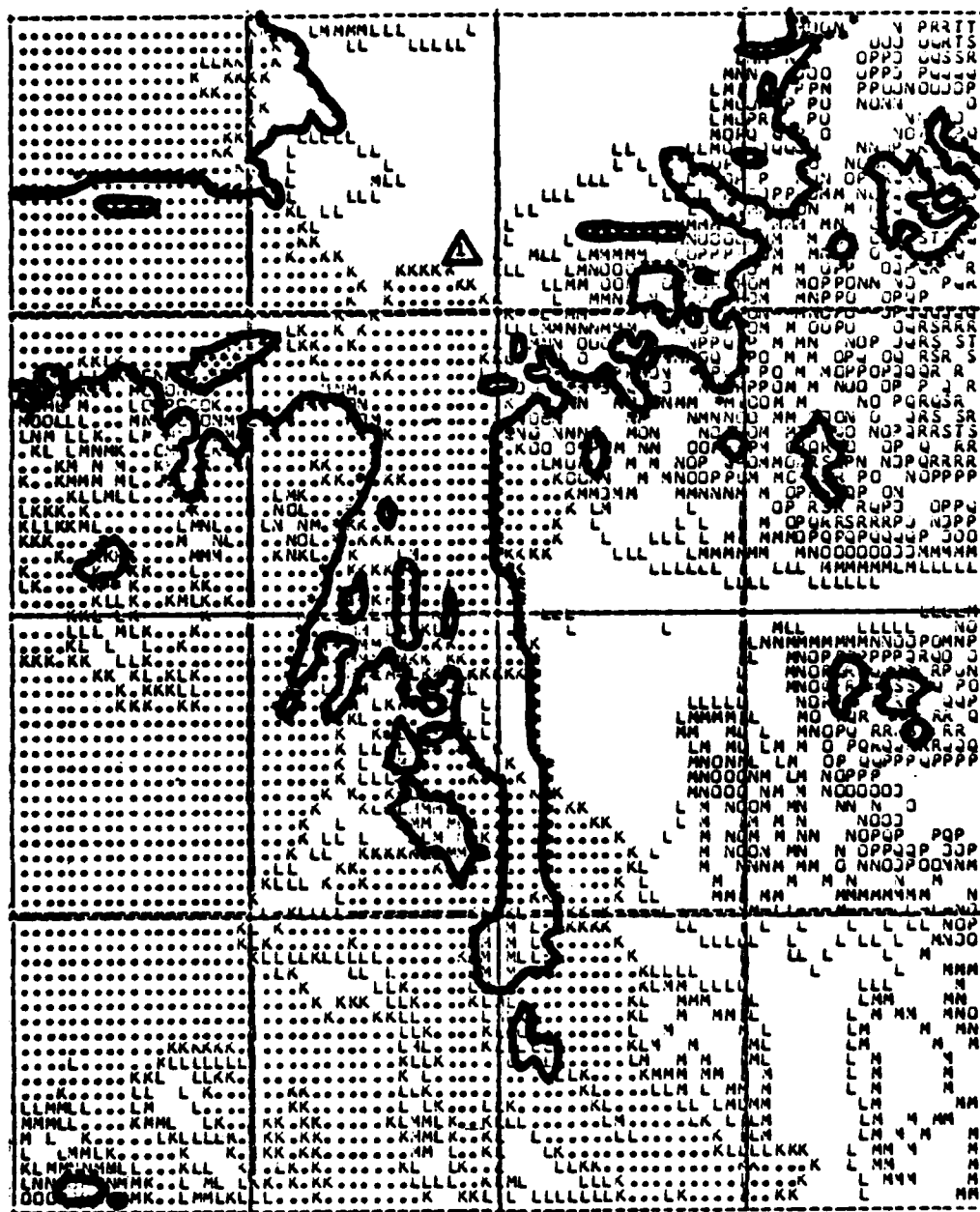


Figure 5.9 AGL Masking Envelope for EW Site Only

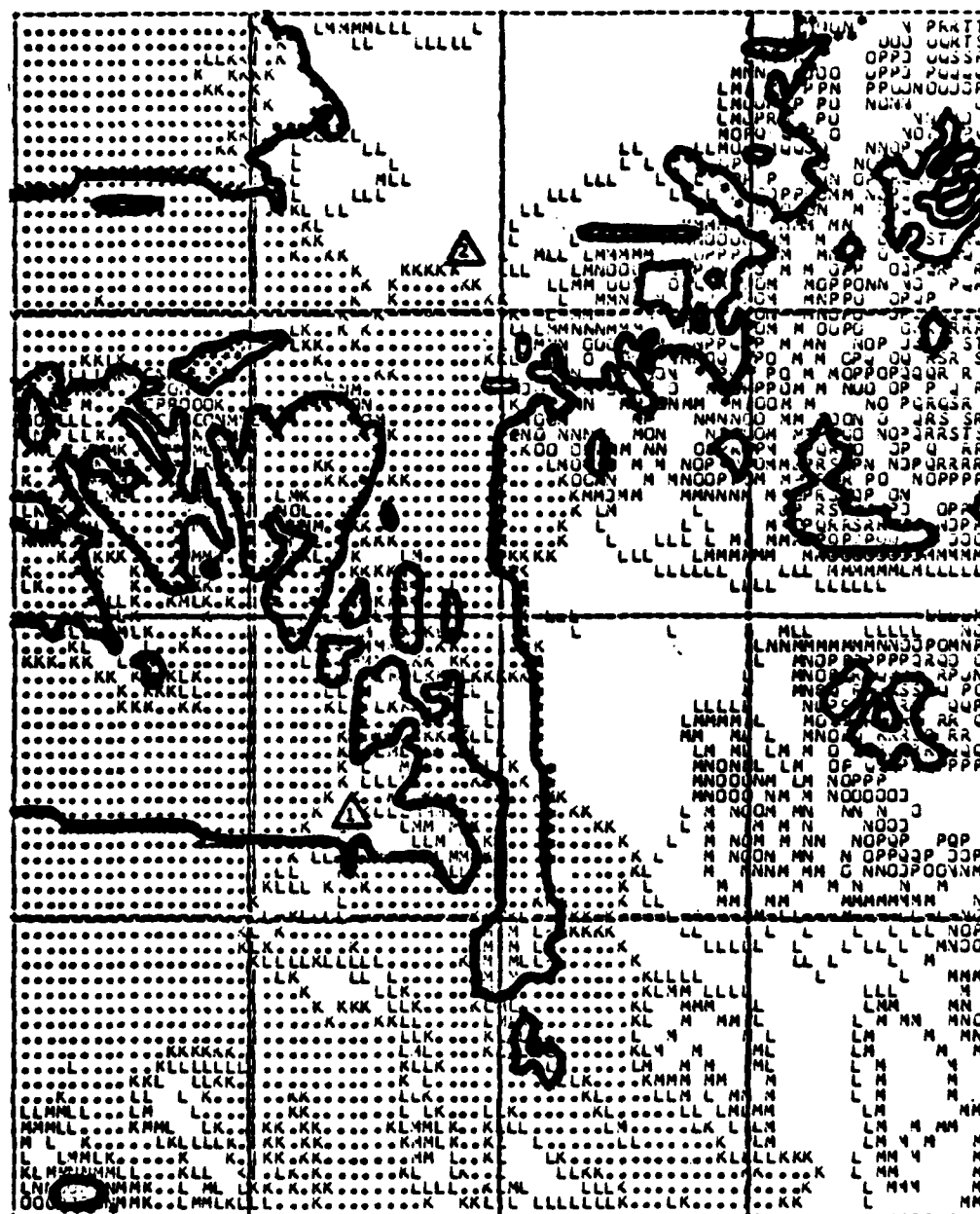


Figure 5.10 60 Minute Square AGL Display

MASK performance it is significant to note that the shapes of the envelopes have not changed appreciably even though the data base resolution has decreased by a factor of nine from that in Figure 5.7. The details of some of the envelopes have begun to fade due to the display resolution, but on the macro scale the same basic planning information shown in Figure 5.7 is also contained in Figure 5.10, which covers nine times as much area. This trend is continued in Figure 5.11 which is the final AGL display. Much of the detail shown in the earlier AGL displays is gone, but the tactical picture has been preserved. It is obvious from this last display that the bombers should approach generally from the south and east.

A suggested strike route of flight is to proceed up Puget Sound at 200 feet hugging the eastern shore until reaching a point 15 miles east-southeast of the bridge. The strike should then turn directly towards the bridge accelerating in preparation for weapon delivery maneuvers. After weapon release the aircraft should regain low altitude and exit the target area with a right turn to the east-northeast until passing the coastline. At this time they may turn south and return to base.

#### c. MSL Displays

The MSL display contains the same general information described in the AGL display discussion, except that the masking envelope is determined by the MSL masking height and the MSL strike altitude is used. The only difference in the display symbology is the addition of the special symbol for areas of terrain which exceed the strike altitude.

In the example, the 7000 foot MSL strike altitude produced MSL displays which were blank in all runs except the one which used the



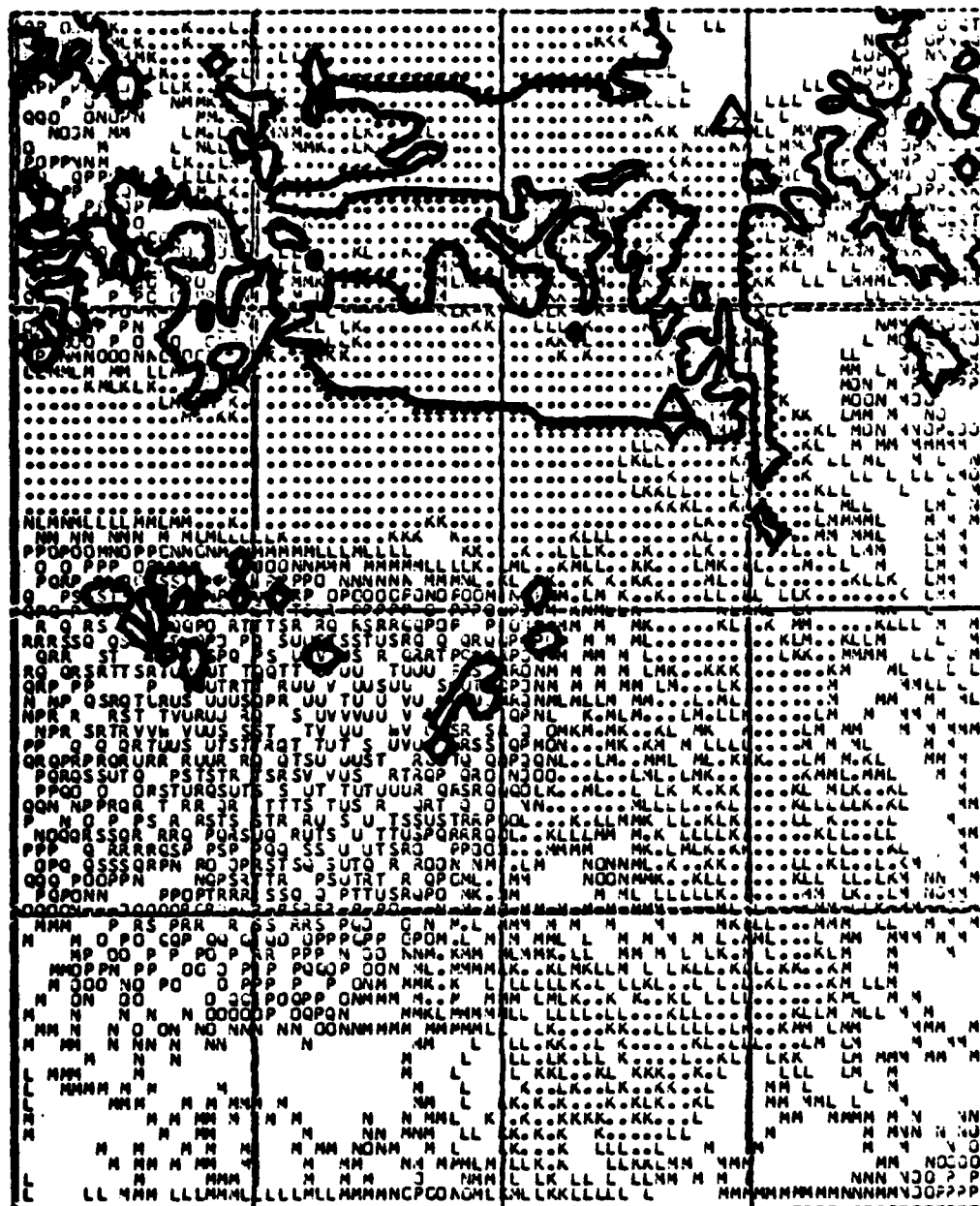


Figure 5.11 Two Degree Square AGL Display

2 by 2 degree data base. This means that the strike aircraft were inside the masking envelopes at 7000 feet at any point on the MSL displays during each of the first three runs. Figure 5.12 shows the MSL display from the last run. This display clearly shows that the 7000 foot strike altitude creates a masking envelope which covers all of the displayed area above 48 degrees. The area in the southwest corner of the display shows a large area of masking due to the obstruction provided by the Olympic Mountains. An unmasked corridor extends southward from the radar sites to the southern border of the display. This clear area results primarily from the fact that much of the area due south of the sites is water or low lying coastal tidal flats. It should be noted that the rendezvous area near the middle of the southern border of the display is shown to be masked at 7000 feet. This will permit the strike elements to rendezvous outside the detection area of the EW radar and thus deny the defense any early strike composition information.

#### d. Conclusions

Based strictly on the displays obtained thus far the following conclusions may be made. First, the strike can rendezvous at 7000 MSL outside of the defense's detection capability. Second, any movement to east from the rendezvous area will take the aircraft into an unmasked area at 7000 MSL. Third, the AGL display clearly shows that the aircraft can penetrate nearly to the target at 200 feet AGL while avoiding detection of any kind. Last, the SAM radar area coverage is restricted solely to the northwest quadrant.

A suggested strike tactic based on MASK's output is to send the bombers on the profile discussed in the AGL display discussion and

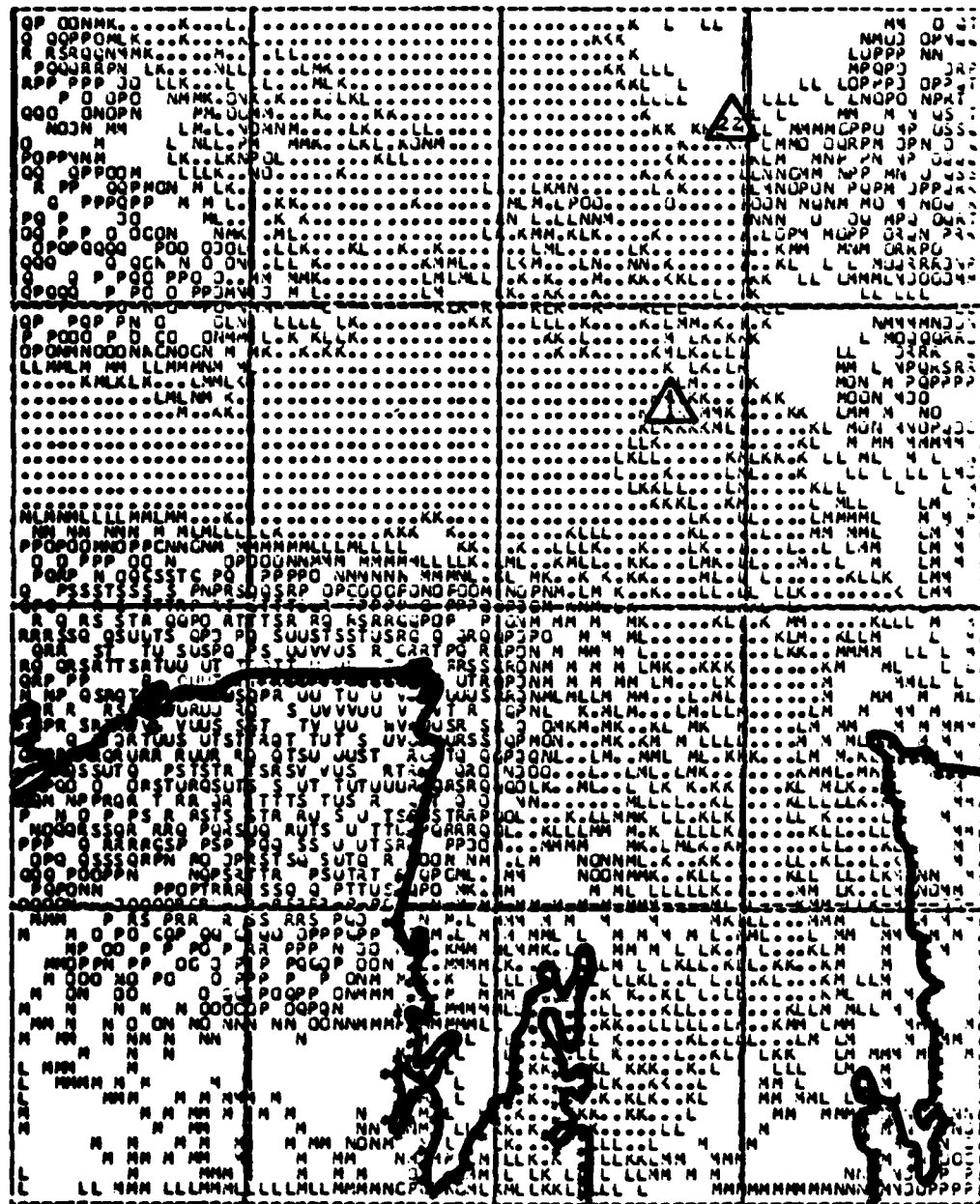


Figure 5.12 Two Degree Square MSL Display

send the chaff, jammers and anti-radiation assets to the northwest. The bombers should descend immediately in order to escape initial detection as they head northeast. The other elements should proceed at 7000 feet to arrive at the point on the MSL display where the area of masking in the southwest corner is closest to the target. The sudden appearance of this decoy force in concert with the use of chaff and jamming will attract the attention of the defense to the southwest while the bombers achieve surprise from the east. The speeds of the various elements should be planned to place the decoy force so that it appears on the victim radar displays shortly before the bombers make their final turn inbound to the target.

Additional MASK runs may be desired in order to more precisely define the point at which the bombers must be at low altitude. Examples of such additional runs are presented in the following section and reveal that the bombers may remain at a comfortable altitude of 2000 MSL until very close to the target if they follow the previously described strike profile.

#### F. ADDITIONAL EXAMPLES

##### 1. General

This section presents several examples which illustrate the effects of changing certain parameters during the input phase of MASK. For clarity and ease of comparison, all examples use only the EW site as a basis for constructing the masking envelopes.

##### 2. Antenna Height Variation

The first comparisons show the effect of varying the radar antenna height. Figure 5.13 shows the masking envelope for a 200 foot AGL target

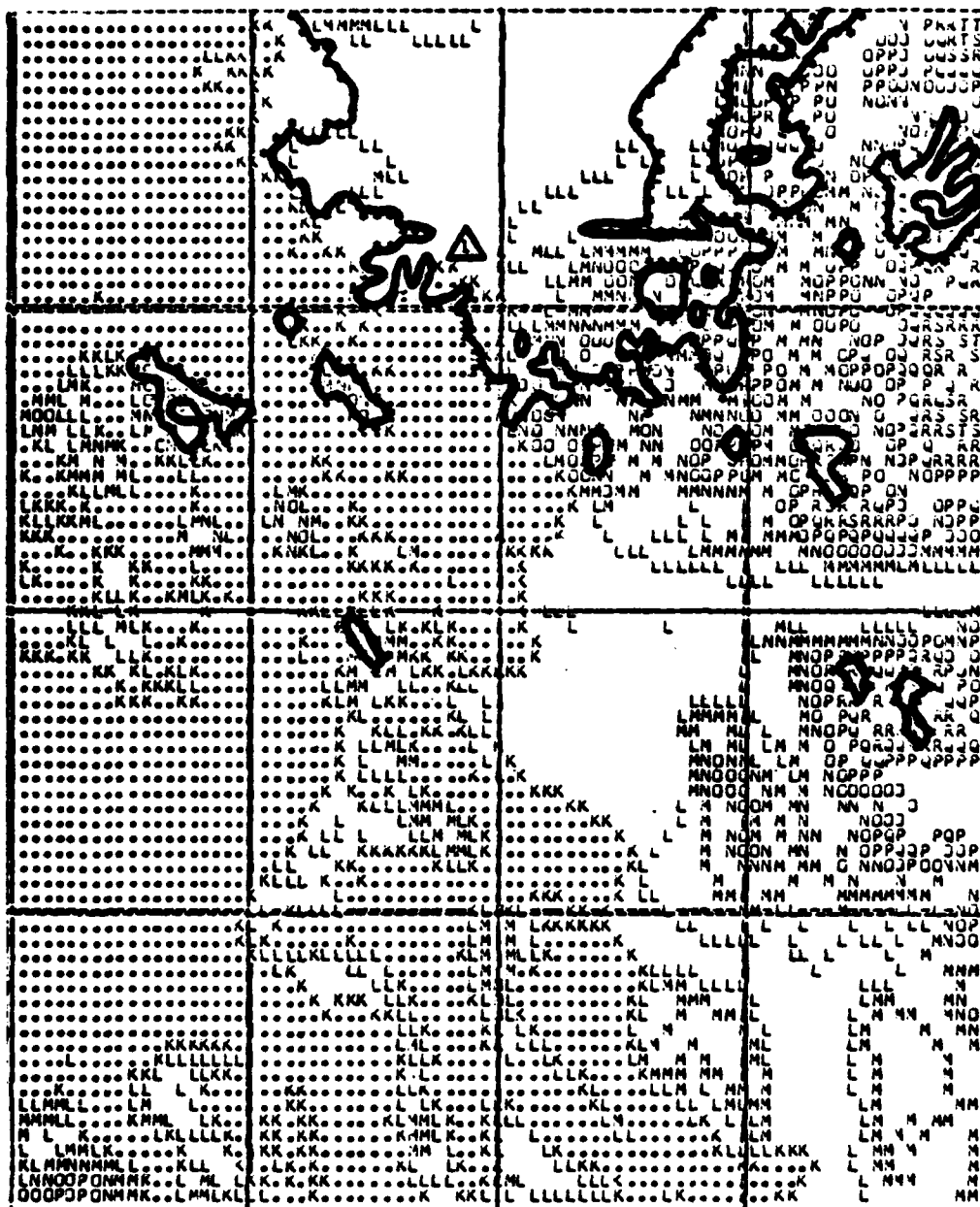


Figure 5.13 Low Antenna Height Example

against the EW site with the following parameters: display coverage is 60 by 60 minutes, PRF is 400,  $dn/dh$  is -050, duct height is 7000 MSL and antenna height is 20 feet AGL. Figure 5.14 is an identical display, except that the antenna has been raised to 100 feet AGL. The most pronounced effect is to markedly increase the coverage to the west and south. However, the large masked areas remain to the southwest and southeast. Figure 5.15 shows a 2 by 2 degree display of the same situation in which the radar antenna has been raised to an altitude of 5000 feet MSL to simulate an airborne surveillance capability. The coverage of the radar has vastly expanded in this example. The entire area shown in Figure 5.14 is contained in the four northeastern grid blocks of Figure 5.15 and indicates that the only areas of significant masking are found in and behind the mountains of the Olympic and Cascade ranges.

### 3. PRF Variation

The next example shows the effect of changing the radar PRF, thereby changing the maximum unambiguous range of the radar. The baseline example is Figure 5.14 in which a PRF of 400 is used. Figure 5.16 shows the same display except that the PRF has been increased to 5000. Theoretically, this value produces a maximum unambiguous range of approximately 16.2 nautical miles. Examination of Figures 5.14 and 5.16 show that the two displays are identical except that Figure 5.16 is truncated at a displayed range of 16.5 nautical miles, the difference from the theoretical value being due to the resolution of the display.

### 4. Refractive Effects

Changes in the refractive gradient are illustrated in the next examples. The baseline case used is Figure 5.13, in which -050 is used

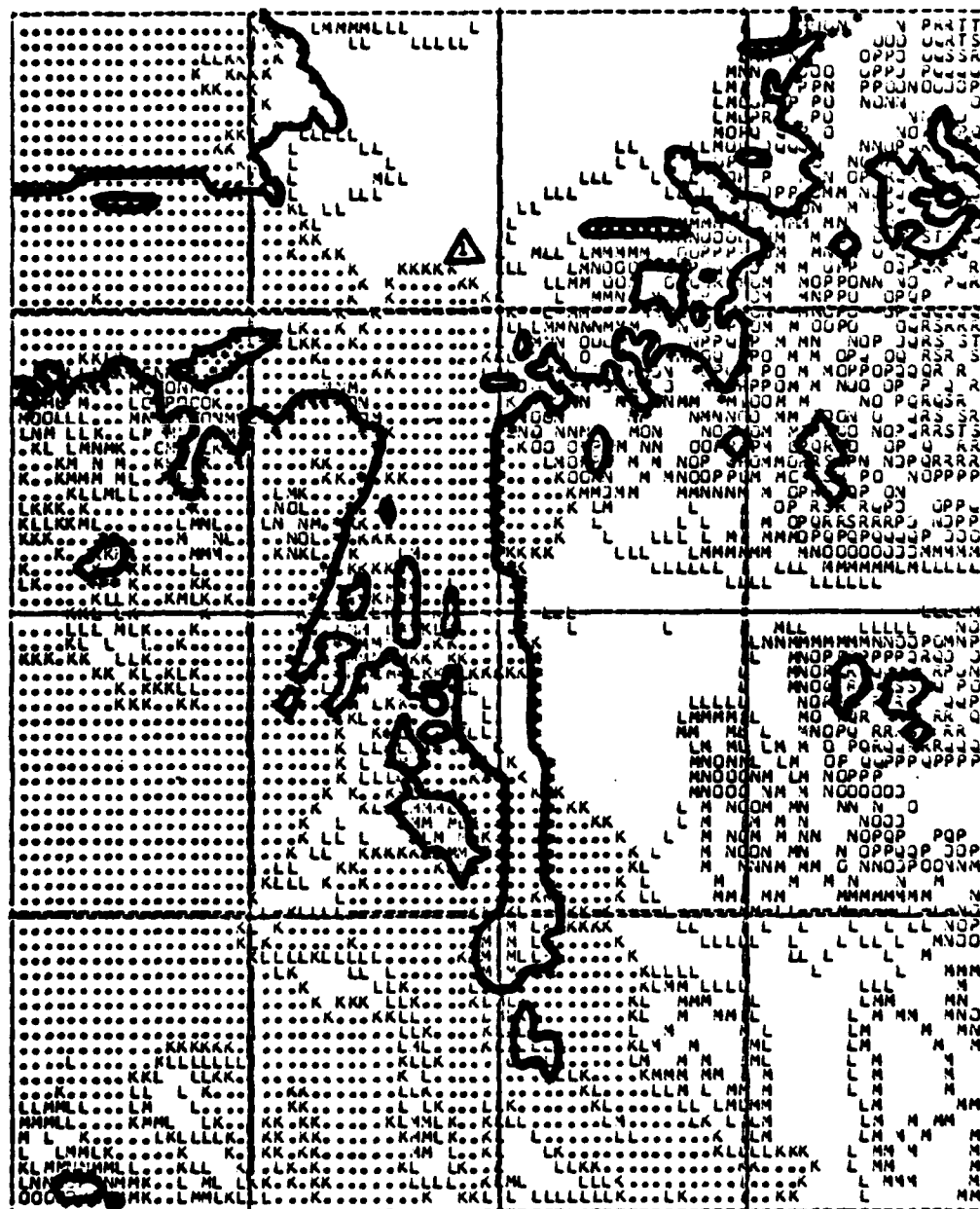


Figure 5.14 Medium Antenna Height Example

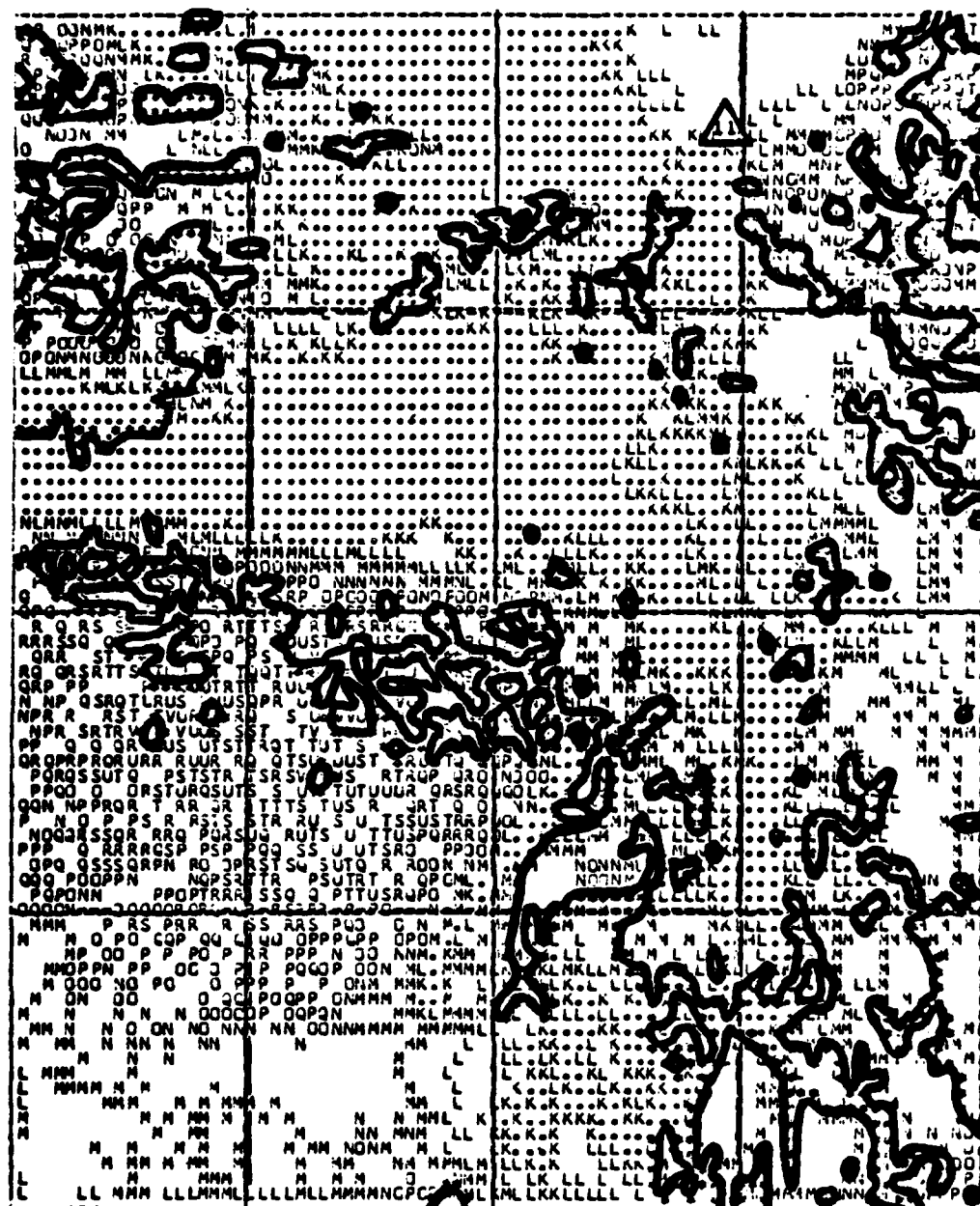


Figure 5.15 Airborne Antenna Height Example



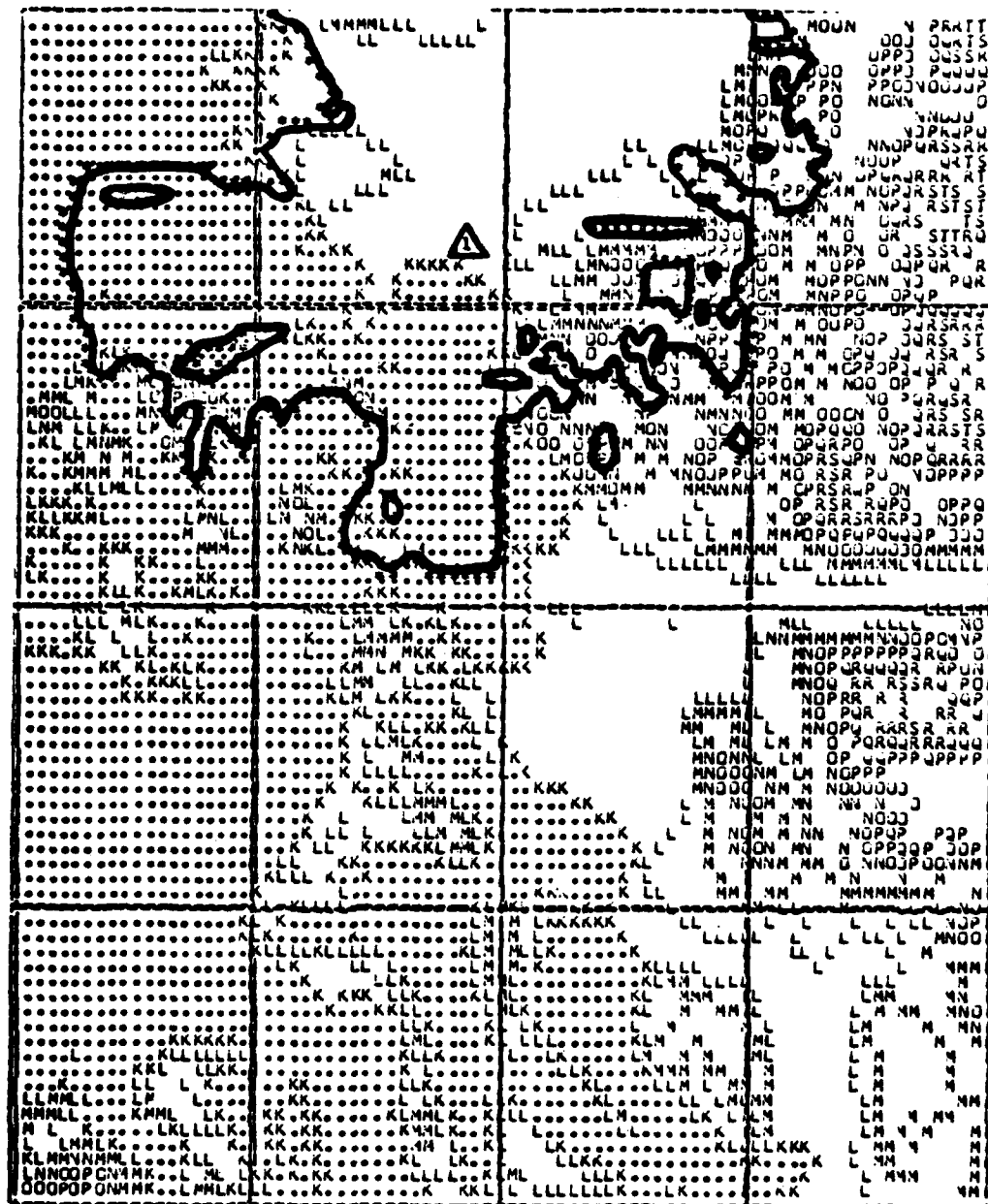


Figure 5.16 PRF Limitation Example

as a value for  $dN/dh$ . Figure 5.17 is an identical case except that  $dN/dh$  has been changed to  $-020$  which is the value used to simulate standard day optical propagation. With a few minor exceptions the displays appear to be identical and only careful examination shows that some of the masking boundaries are closer to the site in the optical case. This is not a very surprising result since both values of  $dN/dh$  fall in the 'normal' propagation range and the radar coverage is primarily limited to short ranges by the low antenna height. In the next example, a noticeable change takes place and serves to further explain the similarity of Figures 5.13 and 5.17. This example is shown in Figure 5.18. All parameters are identical to Figures 5.13 and 5.17 except that  $dN/dh$  has been changed to  $-150$ , thereby simulating extreme superrefraction approaching ducting. In this case it is apparent that little change has taken place at short distances from the site, while more significant changes occur at greater distances. This, of course, is exactly what should be happening since the propagation of waves at short ranges is well approximated by a flat earth model ( $dN/dh = -156$ ). It is only at somewhat greater distances that the effects of refraction begin to alter the radar propagation significantly. This further reinforces the idea that terrain masking is in large part a function of the characteristics of the terrain and is only modified by refraction.

#### 5. Strike Altitudes

The last set of examples shows the effect of changing the AGL and MSL strike altitudes. The baseline case for the AGL displays is Figure 5.13, in which an AGL strike altitude of 200 feet is used. Figure 5.19 shows the same situation except that the AGL altitude is set at 600 feet. The first impression made by the comparison is that both masking envelopes

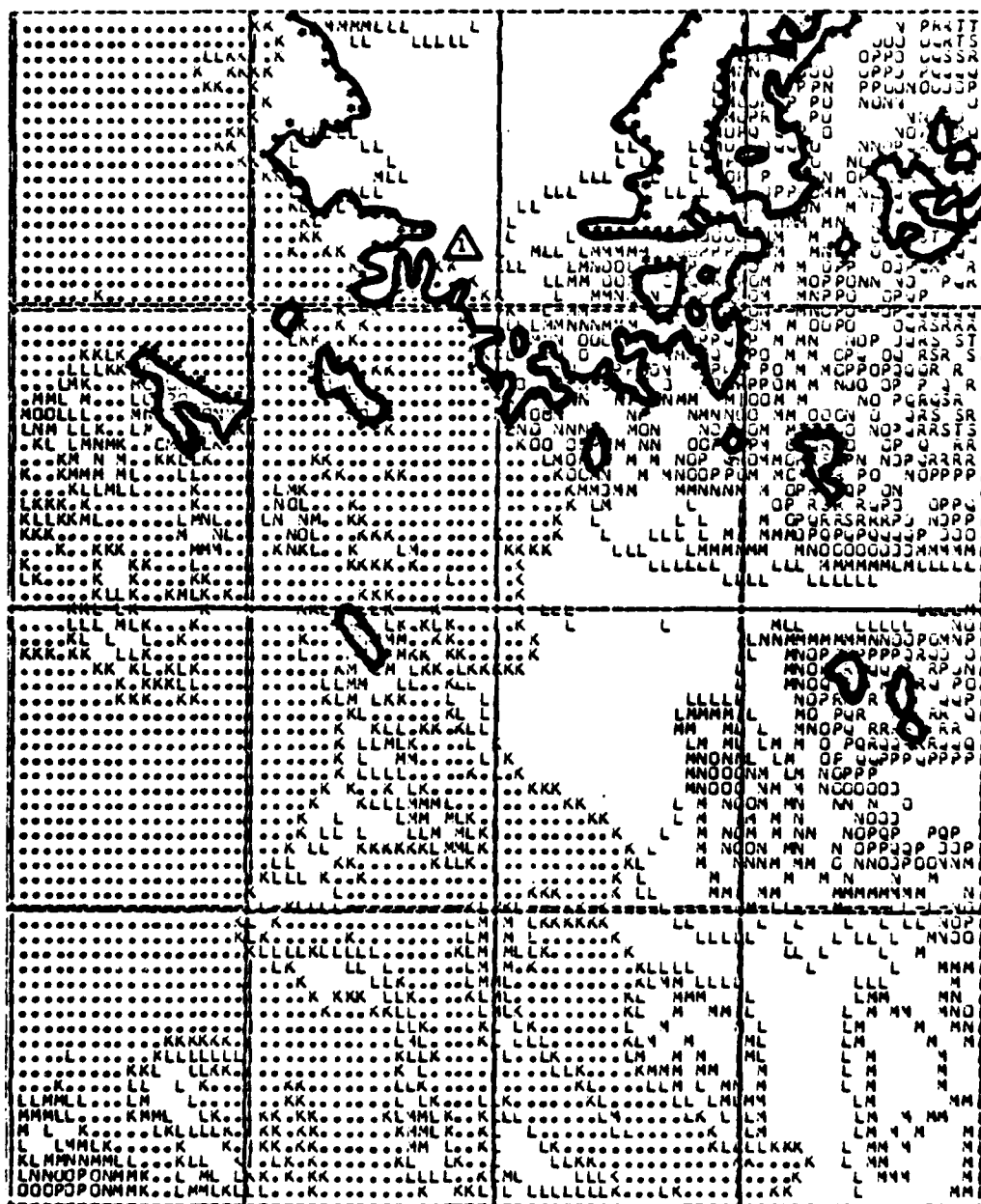


Figure 5.17 Optical Refraction Examples

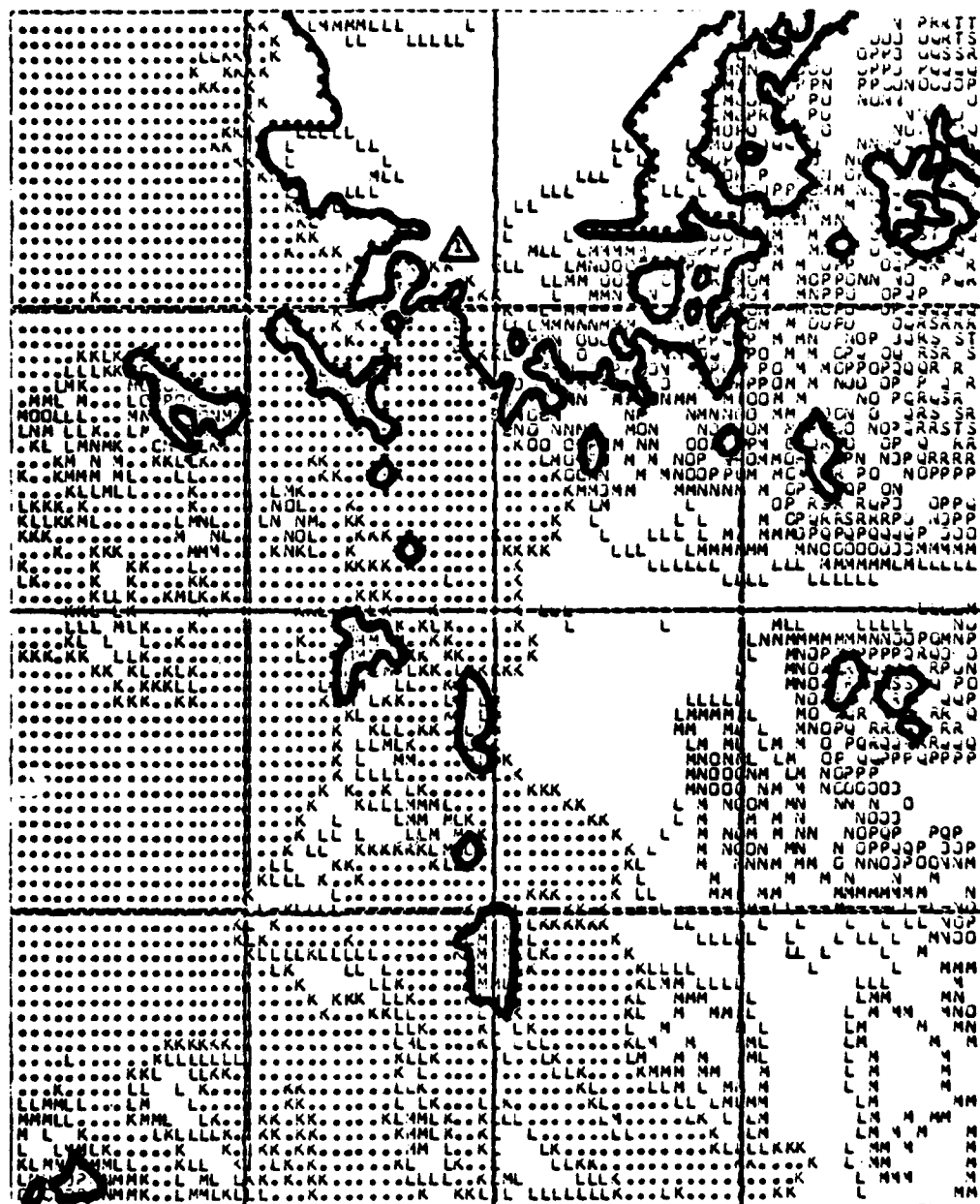


Figure 5.18 Superrefractive Gradient Example

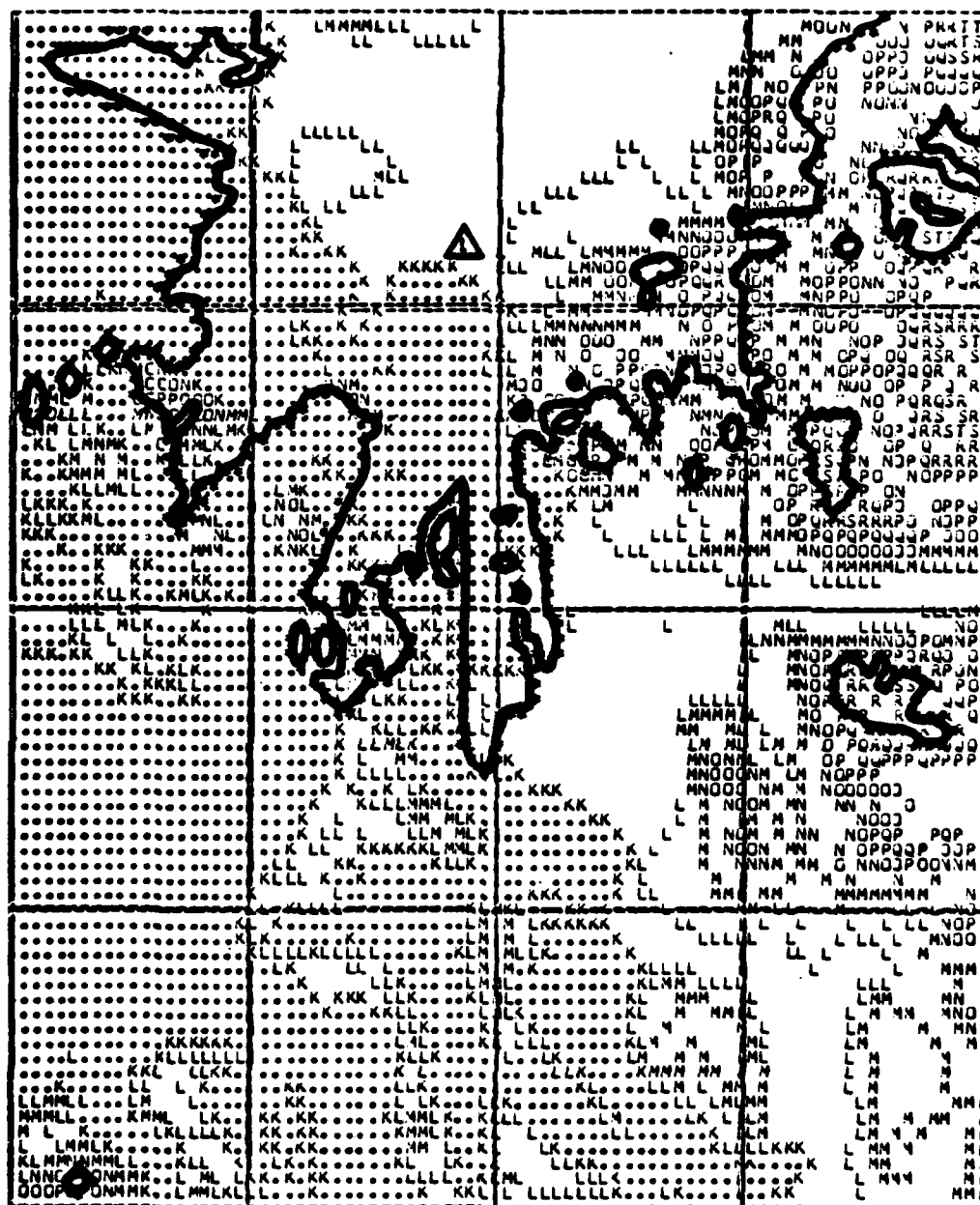


Figure 5.19 600 Foot AGL Strike Example

have the same general shape and the major difference is that the 600 AGL example envelope is larger. The same terrain features caused both envelopes so this development is not so unexpected. Perhaps the most significant result of this comparison is that some areas of the masking envelopes have not changed appreciably. This is especially evident in the area to the southeast of the site. This particular finding is in agreement with the earlier observation that the terrain to the southeast of the EW site was a major obstruction to the radar's coverage.

The comparison of MSL altitudes is illustrated in Figures 5.20 and 5.21. These two examples use radar and refractive inputs identical to those in Figure 5.14. The displayed area is 2 by 2 degrees which allows an additional comparison with Figure 5.12 which is the MSL display from the last run in the hypothetical strike example. Figure 5.20 uses an altitude of 5000 feet MSL resulting in a noticeable reduction in the coverage afforded in the 7000 MSL case. The appearance of a large number of '0' symbols in the southeast of the display indicates the existence of terrain in this area exceeding 5000 feet MSL. Figure 5.21 uses an altitude of 2000 MSL. The trend indicated in Figure 5.20 continues as the coverage envelope shrinks toward the EW site and more '0' symbols are formed where the terrain exceeds 2000 feet MSL. By using Figures 5.12, 5.20 and 5.21, it is possible to determine points along the route of flight of the bomber element at which the aircraft must descend to remain masked. Figure 5.21 shows clearly that the aircraft need not descend below 2000 MSL during most of the transit to and from the target area.

These examples have by no means covered all of the possible combinations of effects which can be processed by MASK. However, they do

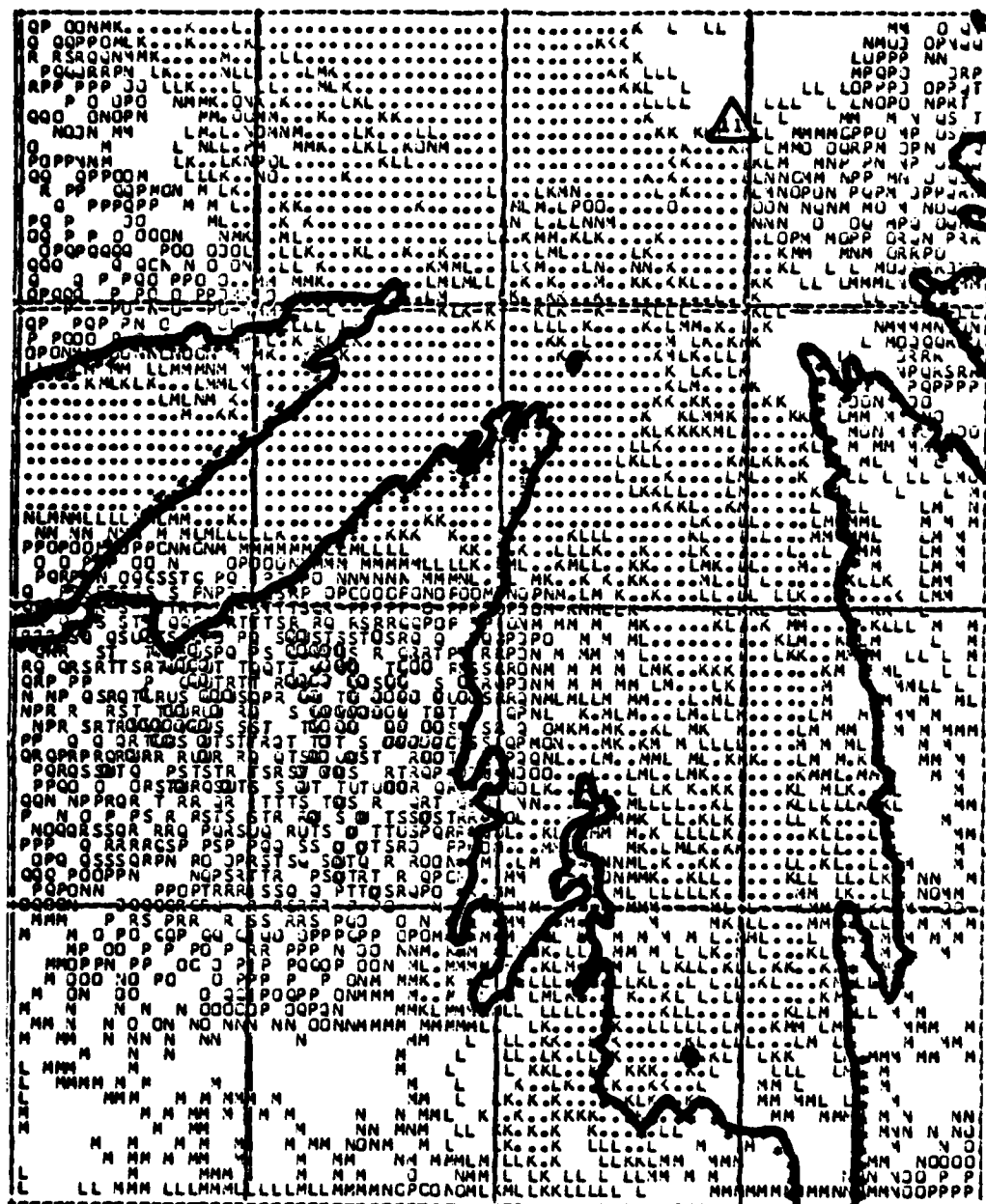


Figure 5.20 5000 Foot MSL Strike Example

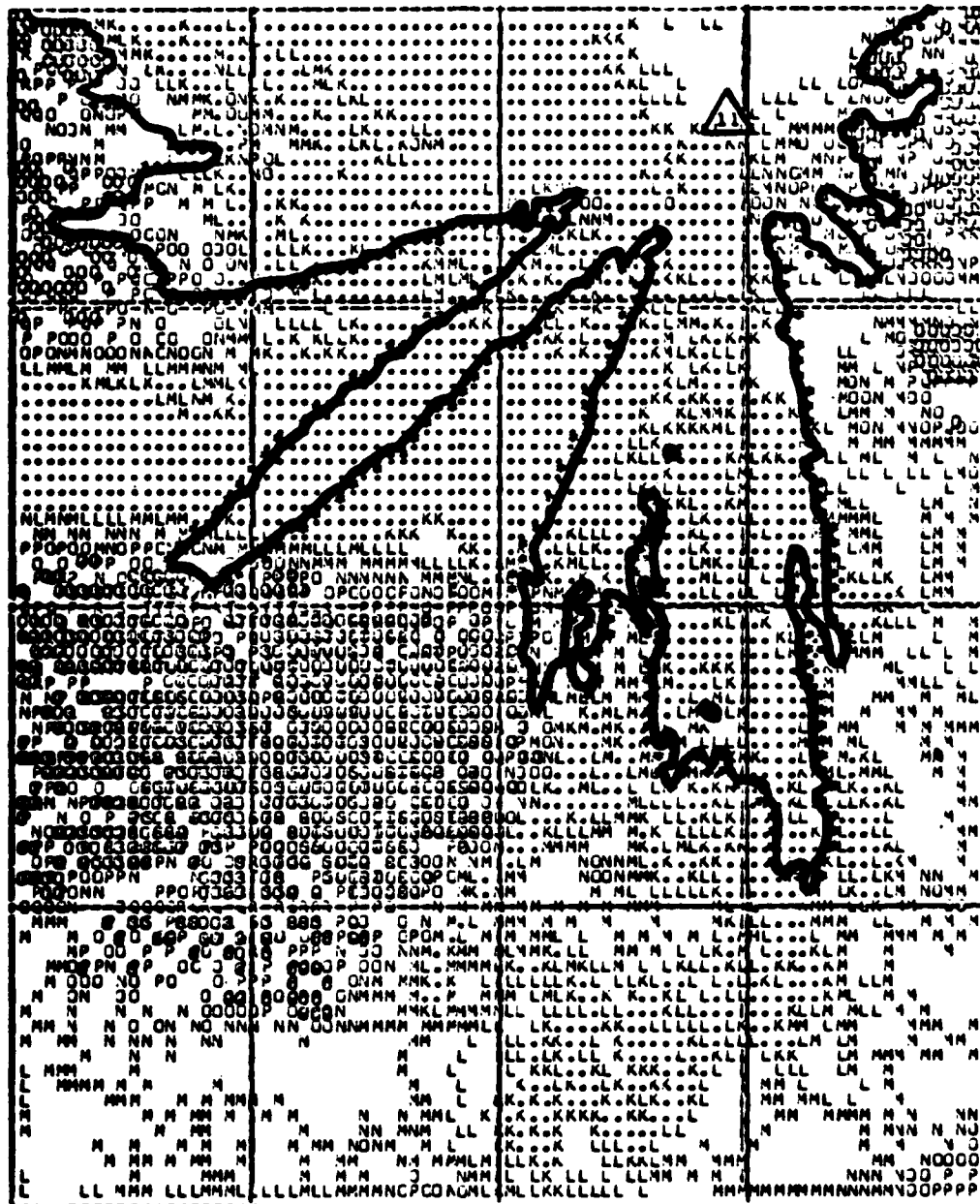


Figure 5.21 2000 Foot MSL Example



illustrate some of the more important changes brought about by altering the input values used in MASK.

## VI. CONCLUSIONS AND RECOMMENDATIONS

MASK was developed as a thesis project. As a result, the programming expertise brought to bear on the subject was necessarily limited. The author makes no apology for this but recognizes it as a fact. More efficient programming methods are, no doubt, available for processing the data used in the masking calculations. In particular, the tedious means of combining several DTED files for large area coverage needs to be streamlined. This and other program refinements could easily occupy a student in pursuit of a thesis topic.

Additional recommendations are dependent on the final selection of a standard shipboard general purpose digital computer. Although the HP 9000 appears to be the current favorite, this is by no means a certainty. Depending on which system is ultimately procured a number of steps must be accomplished to implement MASK aboard ship. The source code must be translated if the shipboard computer cannot use FORTRAN. At a minimum in the case of the HP 9000, the program must be slightly modified to conform to the UNIX operating system. This can be done at the Naval Postgraduate School using the VAX system already installed in Spanagel Hall.

Additional work needs to be done on the graphic displays. The displays created for MASK were designed to be printed using only a line printer without any exotic graphics capability. The newer systems available have various graphics capabilities which would improve the clarity of the MASK displays and eliminate manual operations such as tracing envelopes onto the topographic displays. The output generating code will,

of necessity, require extensive modification depending on the particular system procured by the Navy. This is another area for consideration as a thesis topic in computer science.

Finally, some systems must be developed to supply user organizations with the required data bases, either in an already transformed status or as raw DTED tape files. The capability now exists at NPS to perform the required data base transformations, but the same programs are not likely to be compatible with smaller systems.

Given that the steps mentioned above are taken, MASK has the capability to significantly upgrade the effectiveness of the Navy's tactical air striking forces. Installed on each CV, MASK will allow the strike mission planner to more easily devise routes of flight to reduce the susceptibility of attacking forces to enemy air defenses. MASK will provide the capability to respond to urgent tasking in a timely manner without sacrificing the accuracy required to perform thorough preflight mission planning. The end result will be a greater probability of survival for our attacking aircraft and a consequent increase in the weight of ordnance delivered to the target. On an equal cost basis, it is unlikely that any other single improvement can increase the effectiveness of sea based air power more than the introduction of computer aided mission planning tools such as MASK.

Mention has already been made of the applicability of MASK to the air defense planning problem. In particular, Marine Corps air defense network planners could use MASK to compare alternative missile battery deployment patterns prior to landing the assets ashore. This capability would speed the establishment of organic area air defenses and could additionally be used to plan for contingency redeployment of air defense assets in case some of the systems were destroyed or rendered inoperative.

Additional applications of MASK in the areas of electronic warfare, airborne early warning, remotely piloted drone control and communications planning are numerous. The salient point is that MASK can fulfill an outstanding operational requirement to upgrade shipboard mission planning capabilities in order to meet an ever increasing air defense threat. Ignoring this requirement serves only to limit the effectiveness of the Navy's tactical air forces.

## APPENDIX A

### SOURCE CODE LISTING

The programs contained in this appendix are listed in the order in which they would normally be used in executing MASK. For example, the PROFILE EXEC is listed first followed by the FLY EXEC and then by the tape transfer programs and so on.



80 BLKSIZE 80 RECFM FB)  
2414 BLKSIZE 12070 RECFM FB)  
2414 BLKSIZE 12070 RECFM FB)

81 TEXT  
TEMP DATA 01



```

CCCCCCCCC THE TSCN, JCL PROGRAM, IT ACCESSES A GIVEN TAPE VOLUME CTS000010
C AND READS A TABLE OF CONTENTS FOR THE TAPE. CTS000020
CCCCCCCCC MCKINNEY, CLASS=E CTS000030
//MCKINNEY JOB (1086,0001), MCKINNEY, CLASS=E CTS000040
//*MAIN, ORG=NPVGM1,1086P CTS000050
// EXEC TSCAN, VOLIN=S798, DCBIN=3, UNITIN=3400-3 CTS000060
// CTS000070
// CTS000080
// CTS000090

```

```

CCCCCCCCC THIS IS THE GETTAPERS JCL PROGRAM, IT ACCESSES A GIVEN TAPE VOLUME
C AND FILE AND TRANSFERS IT TO MV5004.
CCCCCCCCC GETTAPERS JCL PROGRAM, IT ACCESSES A GIVEN TAPE VOLUME
//GETTAPES JOB (1086,0001),MCKINNEY,CLASS=E
// *MAIN ORG=NP GVM 1.1086P
// EXEC PGM=IEBGENER
//SYSPRINT DD DISP=OLD,UNIT=3400-3,VOL=SER=S796,
//SYSPUT1 DD DSN=DSNAME,DATA LABEL=(05,BLPI),
// DSN=DSNAME,RECFM=F,BLKSIZE=2414,BLEN=3,
//SYSPUT2 DD DISP=(NEW,KEEP),UNIT=3350,VOL=SER=MVS004,
// DSN=DSNAME,RECFM=F,SPACE=(12070,1204,0),
// DSN=DSNAME,RECFM=F,BLKSIZE=12070,LRECL=2414)
//SYSPIN DD *
/*

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GET000010
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70  CONTINUE
DO 90 M=151,200
DO 100 N=151,200
T(M,N)=((200-M)*(200-N))/50
CONTINUE
100 CONTINUE
DO 90 M=151,200
DO 100 N=151,200
T(M,N)=((200-M)*(200-N))/50
CONTINUE
110 CONTINUE
DO 90 M=151,200
DO 100 N=151,200
T(M,N)=((200-M)*(200-N))/50
CONTINUE
120 CONTINUE
DO 90 M=151,200
DO 100 N=151,200
T(M,N)=((200-M)*(200-N))/50
CONTINUE
130 CONTINUE
DO 90 M=151,200
DO 100 N=151,200
T(M,N)=((200-M)*(200-N))/50
CONTINUE
140 CONTINUE
DO 90 M=151,200
DO 100 N=151,200
T(M,N)=((200-M)*(200-N))/50
CONTINUE
150 CONTINUE
DO 90 M=151,200
DO 100 N=151,200
T(M,N)=((200-M)*(200-N))/50
CONTINUE
160 CONTINUE
DO 90 M=151,200
DO 100 N=151,200
T(M,N)=((200-M)*(200-N))/50
CONTINUE
170 CONTINUE
DO 90 M=151,200
DO 100 N=151,200
T(M,N)=((200-M)*(200-N))/50
CONTINUE
180 CONTINUE
DO 90 M=151,200
DO 100 N=151,200
T(M,N)=((200-M)*(200-N))/50
CONTINUE
190 CONTINUE
DO 90 M=151,200
DO 100 N=151,200
T(M,N)=((200-M)*(200-N))/50
CONTINUE
200 CONTINUE
DO 90 M=151,200
DO 100 N=151,200
T(M,N)=((200-M)*(200-N))/50
CONTINUE
210 CONTINUE
DO 90 M=151,200
DO 100 N=151,200
T(M,N)=((200-M)*(200-N))/50
CONTINUE
220 CONTINUE
DO 90 M=151,200
DO 100 N=151,200
T(M,N)=((200-M)*(200-N))/50
CONTINUE
230 CONTINUE
DO 90 M=151,200
DO 100 N=151,200
T(M,N)=((200-M)*(200-N))/50
CONTINUE
240 CONTINUE
DO 90 M=151,200
DO 100 N=151,200
T(M,N)=((200-M)*(200-N))/50
CONTINUE
250 CONTINUE
DO 90 M=151,200
DO 100 N=151,200
T(M,N)=((200-M)*(200-N))/50
CONTINUE

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* SQUARE DATA BASES WITH THE /° FOLLOWING DIMENSIONS IN MINUTES: 2
* 0.40, 1.60, 1.20, 2.40, 3.00. /°
  READ(5,110) INTVL
  FORMAT(11,12)
  WRITE(5,120)
  110
  120
  * OF THE INPUT DMAAC /° DATA BASE IN THE FOLLOWING CORNER
  * IN COLUMNS 1-2 DEPENDING ON WHETHER /° THE CORNER IS ABOVE OR BELOW
  * THE EQUATOR. /°
  READ(5,130) NS
  FORMAT(1,12)
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  CCCC CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
  C    FOR LATITUDES LESS THAN 50 DEGREES DTED INTERVAL IS THREE
  C    CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
  IF((NS.EQ.NN.AND.3LAT/10000.GE.50).OR.(NS.NE.NN.AND.6LAT/10000.GE.
  *51)) GO TO 10
  DB INT=3
  GO TO 30
  CCCC CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
  C    FOR LATITUDES FROM 50 TO 75, DTED INTERVAL IS SIX
  C    CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
  IF((NS.EQ.NN.AND.3LAT/10000.GE.75).OR.(NS.NE.NN.AND.6LAT/10000.GE.
  *76)) GO TO 25
  DB INT=6
  GO TO 30
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*OF THE COMBINED: DATA BASE IN THE FOLLOWING FORMAT:NN OR SS IN C
*OLUMNS 1-2 DEPEND ON WHETHER: THE CORNER IS ABOVE OR BELOW TH
*E EQUATOR.
  130 READ(5,130)NS
      FORMAT(1A2)
  140 WRITE(5,140)
      FORMAT(1A2)
  150 READ(5,150)DLAT
      FORMAT(1A2)
  160 WRITE(5,160)
      FORMAT(1A2)
  170 READ(5,170)EM
      FORMAT(1A1)
  180 WRITE(5,180)
      FORMAT(1A1)
  190 READ(5,190)DLO
      FORMAT(1A1)
  200 WRITE(5,200)
      FORMAT(1A1)
  210 READ(5,210)DLO
      FORMAT(1A1)
  220 WRITE(5,220)
      FORMAT(1A1)
  230 READ(5,230)DLO
      FORMAT(1A1)
  240 WRITE(5,240)
      FORMAT(1A1)
  250 READ(5,250)DLO
      FORMAT(1A1)
  260 WRITE(5,260)
      FORMAT(1A1)
  270 READ(5,270)DLO
      FORMAT(1A1)
  280 WRITE(5,280)
      FORMAT(1A1)
  290 READ(5,290)DLO
      FORMAT(1A1)
  300 WRITE(5,300)
      FORMAT(1A1)
  310 READ(5,310)DLO
      FORMAT(1A1)
  320 WRITE(5,320)
      FORMAT(1A1)
  330 READ(5,330)DLO
      FORMAT(1A1)
  340 WRITE(5,340)
      FORMAT(1A1)
  350 READ(5,350)DLO
      FORMAT(1A1)
  360 WRITE(5,360)
      FORMAT(1A1)
  370 READ(5,370)DLO
      FORMAT(1A1)
  380 WRITE(5,380)
      FORMAT(1A1)
  390 READ(5,390)DLO
      FORMAT(1A1)
  400 WRITE(5,400)
      FORMAT(1A1)
  410 READ(5,410)DLO
      FORMAT(1A1)
  420 WRITE(5,420)
      FORMAT(1A1)
  430 READ(5,430)DLO
      FORMAT(1A1)
  440 WRITE(5,440)
      FORMAT(1A1)
  450 READ(5,450)DLO
      FORMAT(1A1)
  460 WRITE(5,460)
      FORMAT(1A1)
  470 READ(5,470)DLO
      FORMAT(1A1)
  480 WRITE(5,480)
      FORMAT(1A1)
  490 READ(5,490)DLO
      FORMAT(1A1)
  500 WRITE(5,500)
      FORMAT(1A1)
  510 READ(5,510)DLO
      FORMAT(1A1)
  520 WRITE(5,520)
      FORMAT(1A1)
  530 READ(5,530)DLO
      FORMAT(1A1)
  540 WRITE(5,540)
      FORMAT(1A1)
  550 READ(5,550)DLO
      FORMAT(1A1)
  560 WRITE(5,560)
      FORMAT(1A1)
  570 READ(5,570)DLO
      FORMAT(1A1)
  580 WRITE(5,580)
      FORMAT(1A1)
  590 READ(5,590)DLO
      FORMAT(1A1)
  600 WRITE(5,600)
      FORMAT(1A1)
  610 READ(5,610)DLO
      FORMAT(1A1)
  620 WRITE(5,620)
      FORMAT(1A1)
  630 READ(5,630)DLO
      FORMAT(1A1)
  640 WRITE(5,640)
      FORMAT(1A1)
  650 READ(5,650)DLO
      FORMAT(1A1)
  660 WRITE(5,660)
      FORMAT(1A1)
  670 READ(5,670)DLO
      FORMAT(1A1)
  680 WRITE(5,680)
      FORMAT(1A1)
  690 READ(5,690)DLO
      FORMAT(1A1)
  700 WRITE(5,700)
      FORMAT(1A1)
  710 READ(5,710)DLO
      FORMAT(1A1)
  720 WRITE(5,720)
      FORMAT(1A1)
  730 READ(5,730)DLO
      FORMAT(1A1)
  740 WRITE(5,740)
      FORMAT(1A1)
  750 READ(5,750)DLO
      FORMAT(1A1)
  760 WRITE(5,760)
      FORMAT(1A1)
  770 READ(5,770)DLO
      FORMAT(1A1)
  780 WRITE(5,780)
      FORMAT(1A1)
  790 READ(5,790)DLO
      FORMAT(1A1)
  800 WRITE(5,800)
      FORMAT(1A1)
  810 READ(5,810)DLO
      FORMAT(1A1)
  820 WRITE(5,820)
      FORMAT(1A1)
  830 READ(5,830)DLO
      FORMAT(1A1)
  840 WRITE(5,840)
      FORMAT(1A1)
  850 READ(5,850)DLO
      FORMAT(1A1)
  860 WRITE(5,860)
      FORMAT(1A1)
  870 READ(5,870)DLO
      FORMAT(1A1)
  880 WRITE(5,880)
      FORMAT(1A1)
  890 READ(5,890)DLO
      FORMAT(1A1)
  900 WRITE(5,900)
      FORMAT(1A1)
  910 READ(5,910)DLO
      FORMAT(1A1)
  920 WRITE(5,920)
      FORMAT(1A1)
  930 READ(5,930)DLO
      FORMAT(1A1)
  940 WRITE(5,940)
      FORMAT(1A1)
  950 READ(5,950)DLO
      FORMAT(1A1)
  960 WRITE(5,960)
      FORMAT(1A1)

```

```

290      CONTINUE
      GO TO 1200
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
C      THE ASSEMBLY OF SIXTEEN FILES BEGINS HERE
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
36      READ(15,200)K
      DO 310 J=1,100
        READ(15,210)(L(I,J),I=1,100)
310      CONTINUE
      READ(16,200)K
      DO 330 J=101,200
        READ(16,210)(L(I,J),I=1,100)
330      CONTINUE
      READ(17,200)K
      DO 340 J=201,300
        READ(17,210)(L(I,J),I=1,100)
340      CONTINUE
      READ(18,200)K
      DO 360 J=301,400
        READ(18,210)(L(I,J),I=1,100)
360      CONTINUE
      READ(19,200)K
      DO 380 J=1,100
        READ(19,210)(L(I,J),I=101,200)
380      CONTINUE
      READ(20,200)K
      DO 400 J=101,200
        READ(20,210)(L(I,J),I=101,200)
400      CONTINUE
      READ(21,200)K
      DO 420 J=201,300
        READ(21,210)(L(I,J),I=101,200)
420      CONTINUE
      READ(22,200)K
      DO 440 J=301,400
        READ(22,210)(L(I,J),I=101,200)
440      CONTINUE
      READ(23,200)K
      DO 460 J=1,100
        READ(23,210)(L(I,J),I=201,300)
460      CONTINUE
      READ(24,200)K
      DO 480 J=101,200
        READ(24,210)(L(I,J),I=201,300)
480      CONTINUE
      READ(25,200)K
      DO 500 J=201,300
        READ(25,210)(L(I,J),I=201,300)

```

```

COM00970
COM00980
COM00990
COM01000
COM01010
COM01020
COM01030
COM01040
COM01050
COM01060
COM01070
COM01080
COM01090
COM01100
COM01110
COM01120
COM01130
COM01140
COM01150
COM01160
COM01170
COM01180
COM01190
COM01200
COM01210
COM01220
COM01230
COM01240
COM01250
COM01260
COM01270
COM01280
COM01290
COM01300
COM01310
COM01320
COM01330
COM01340
COM01350
COM01360
COM01370
COM01380
COM01390
COM01400
COM01410
COM01420
COM01430
COM01440

```

```

500 CONTINUE
    READ(26,200)K
    DO 520 J=301,400
        READ(26,210)(L(I,J),I=201,300)
    CONTINUE
520 READ(27,200)K
    DO 540 J=1,100
        READ(27,210)(L(I,J),I=301,400)
    CONTINUE
540 READ(28,200)K
    DO 560 J=101,200
        READ(28,210)(L(I,J),I=301,400)
    CONTINUE
560 READ(29,200)K
    DO 580 J=201,300
        READ(29,210)(L(I,J),I=301,400)
    CONTINUE
580 READ(30,200)K
    DO 600 J=301,400
        READ(30,210)(L(I,J),I=301,400)
    CONTINUE
600 GO TO 1200
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
C THE ASSEMBLY CF TWENTY-FIVE FILES BEGINS HERE
C CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
45 READ(31,200)K
    DO 620 J=1,80
        READ(31,210)(L(I,J),I=1,80)
    CONTINUE
620 READ(32,200)K
    DO 640 J=81,160
        READ(32,210)(L(I,J),I=1,80)
    CONTINUE
640 READ(33,200)K
    DO 660 J=161,240
        READ(33,210)(L(I,J),I=1,80)
    CONTINUE
660 READ(34,200)K
    DO 680 J=241,320
        READ(34,210)(L(I,J),I=1,80)
    CONTINUE
680 READ(35,200)K
    DO 700 J=321,400
        READ(35,210)(L(I,J),I=1,80)
    CONTINUE
700 READ(36,200)K
    DO 720 J=1,80
        READ(36,210)(L(I,J),I=81,160)

```

```

COMO1450
COMO1460
COMO1470
COMO1480
COMO1490
COMO1500
COMO1510
COMO1520
COMO1530
COMO1540
COMO1550
COMO1560
COMO1570
COMO1580
COMO1590
COMO1600
COMO1610
COMO1620
COMO1630
COMO1640
COMO1650
COMO1660
COMO1670
COMO1680
COMO1690
COMO1700
COMO1710
COMO1720
COMO1730
COMO1740
COMO1750
COMO1760
COMO1770
COMO1780
COMO1790
COMO1800
COMO1810
COMO1820
COMO1830
COMO1840
COMO1850
COMO1860
COMO1870
COMO1880
COMO1890
COMO1900
COMO1910
COMO1920

```

```

720 CONTINUE
    READ(37,200)K
    DO 740 J=81,160
        READ(37,210)(L(I,J),I=81,160)
    CONTINUE
740 READ(38,200)K
    DO 760 J=161,240
        READ(38,210)(L(I,J),I=81,160)
    CONTINUE
760 READ(39,200)K
    DO 780 J=241,320
        READ(39,210)(L(I,J),I=81,160)
    CONTINUE
780 READ(40,200)K
    DO 800 J=321,400
        READ(40,210)(L(I,J),I=81,160)
    CONTINUE
800 READ(41,200)K
    DO 820 J=1,80
        READ(41,210)(L(I,J),I=161,240)
    CONTINUE
820 READ(42,200)K
    DO 840 J=81,160
        READ(42,210)(L(I,J),I=161,240)
    CONTINUE
840 READ(43,200)K
    DO 860 J=161,240
        READ(43,210)(L(I,J),I=161,240)
    CONTINUE
860 READ(44,200)K
    DO 880 J=241,320
        READ(44,210)(L(I,J),I=161,240)
    CONTINUE
880 READ(45,200)K
    DO 900 J=321,400
        READ(45,210)(L(I,J),I=161,240)
    CONTINUE
900 READ(46,200)K
    DO 920 J=1,80
        READ(46,210)(L(I,J),I=241,320)
    CONTINUE
920 READ(47,200)K
    DO 940 J=81,160
        READ(47,210)(L(I,J),I=241,320)
    CONTINUE
940 READ(48,200)K
    DO 960 J=161,240
        READ(48,210)(L(I,J),I=241,320)

```

```

COMO1930
COMO1940
COMO1950
COMO1960
COMO1970
COMO1980
COMO1990
COMO2000
COMO2010
COMO2020
COMO2030
COMO2040
COMO2050
COMO2060
COMO2070
COMO2080
COMO2090
COMO2100
COMO2110
COMO2120
COMO2130
COMO2140
COMO2150
COMO2160
COMO2170
COMO2180
COMO2190
COMO2200
COMO2210
COMO2220
COMO2230
COMO2240
COMO2250
COMO2260
COMO2270
COMO2280
COMO2290
COMO2300
COMO2310
COMO2320
COMO2330
COMO2340
COMO2350
COMO2360
COMO2370
COMO2380
COMO2390
COMO2400

```







HLR	I	HEIGHT OF CLOSEST DATA BASE ELEMENT TO THE SOUTH- HEIGHT OF THE RADAR SITE	CMA500490
HT	I	HEIGHT IN METERS OF ANY POINT (M,N) IN THE MASK	CMA500500
HUL	I	DATA BASE CLOSEST DATA BASE ELEMENT TO THE NORTH- HEIGHT OF THE RADAR SITE	CMA500510
HUR	I	HEIGHT OF THE CLOSEST DATA BASE ELEMENT TO THE NORTH- HEIGHT OF THE RADAR SITE	CMA500520
I	R	EAST OF THE RADAR SITE MATRIX X EQUIVALENT VALUE OF THE LATITUDE OF THE RADAR SITE	CMA500530
IADIS	I	AGL DISPLAY MATRIX -- DIMENSIONED AT (80,80)	CMA500540
IMDIS	I	MSL DISPLAY MATRIX -- DIMENSIONED AT (80,80)	CMA500550
II	I	INTEGER VALUE OF 'I'	CMA500560
INTVL	R	TRANSFORMATION INTERVAL OF DATA BASE IN ARCSECONDS MATRIX X EQUIVALENT VALUE OF THE LONGITUDE OF THE RADAR SITE	CMA500570
J	I	INTEGER VALUE OF 'J'	CMA500580
JJ	I	INDEX VARIABLE FOR SITE NUMBER	CMA500590
KMAX	I	TOTAL NUMBER OF SITES INPUT THUS FAR	CMA500600
L	I**2	ELEVATION DATA DATA BASE MATRIX -- DIMENSIONED AT (400,400)	CMA500610
LIH	R	INTERPOLATED HEIGHT OF RADAR SITE IN METERS	CMA500620
LK	I	INDICATOR VARIABLE FOR TOPO DISPLAY SELECTION	CMA500630
M	I	INDEX VARIABLE FOR ROWS OF MASK DATA BASE	CMA500640
MAXV	DP	RADIAN MEASURE OF LOOK ANGLE BETWEEN VERTICAL AND THE CP AS SEEN BY THE RADAR ANTENNA	CMA500650
MHT	R	OUTPUT VALUE OF ANTENNA HEIGHT ABOVE MSL IN FEET	CMA500660
MMAX	I	MAX VALUE OF 'M' -- CURRENTLY 400	CMA500670
MODD	I	MOD(M, DISRES) -- TAKES VALUES 1, 6, 11, 16, ... 396	CMA500680
MPPLAT	R	NUMBER OF METERS BETWEEN ELEVATION DATA POINTS IN LATITUDE	CMA500690
MPPLON	R	NUMBER OF METERS BETWEEN ELEVATION DATA POINTS IN LONGITUDE	CMA500700
MSL	R	MSL STRIKE ALTITUDE IN METERS	CMA500710
MJR	R	MAXIMUM UNAMBIGUOUS RANGE OF RADAR IN METERS	CMA500720
N	I	INDEX VARIABLE FOR COLUMNS OF MASK DATA BASE	CMA500730
NMAX	I	MAX VALUE OF 'N' -- CURRENTLY 400	CMA500740
NODD	I	MOD(N, DISRES) -- SAME VALUES AS MODD	CMA500750
NS	I	INDICATOR VALUE FOR HEMISPHERE OF LATITUDE OF RADAR SITE	CMA500760
ORIG	R	HEIGHT OF ANTENNA IN METERS ABOVE SEA LEVEL	CMA500770
PI	R	VALUE OF PI	CMA500780
PRF	I	PULSE REPEATITION FREQUENCY OF RADAR	CMA500790
R	I	FOUR-THIRDS EARTH RADIUS IN METERS	CMA500800
RAJ	R	FUNCTION WHICH CONVERTS DEGREES TO RADIAN	CMA500810
RD	I	EQUIVALENT EARTH RADIUS IN METERS PRODUCED BY USING ONOH	CMA500820
RE	I	ACTUAL EARTH RADIUS IN METERS	CMA500830
			CMA500840
			CMA500850
			CMA500860
			CMA500870
			CMA500880
			CMA500890
			CMA500900
			CMA500910
			CMA500920
			CMA500930
			CMA500940
			CMA500950
			CMA500960



```

610 WRITE(5,610)K  

    FORMAT(1X,'INPUT RADAR SITE # ',I1,' LONGITUDE (DDMMSS) STARTING  

    *//, IN COLUMN 1,)  

    READ(5,810)RLON(K)  

    810 FORMATT(17)  

    WRITE(5,640)K  

    640 FORMATT(1X,'INPUT RADAR SITE # ',I1,' ELEVATION (FT MSL) OR -9999,  

    *//, IF UNKNOWN),RIGHT JUSTIFIED IN COLUMNS 1-5,)  

    READ(5,840)RHF(K)  

    840 FORMATT(15)  

    WRITE(5,650)K  

    650 FORMATT(1X,'INPUT RADAR # ',I1,' MAST HEIGHT (FT) OR -99 (IF UNKNOW  

    *NN),/ , RIGHT JUSTIFIED IN COLUMNS 1-3,)  

    READ(5,850)RMHF(K)  

    850 FORMATT(13)  

    WRITE(5,655)K  

    655 FORMATT(1X,'TO OBTAIN CALCULATIONS BASED ON UNAMBIGUOUS RANGE',/IX,  

    * (PULSE RADARS ONLY), INPUT RADAR # ',I1,' PULSE REPETITION',/FMA  

    *REQUENCY (PRF) RIGHT JUSTIFIED, INTEGER VALUED IN COLUMNS 1-4,/.  

    *FOR RADARS USING TWO PRFS SIMULTANEOUSLY, ENTER THE ABSOLUTE',/DI  

    *REFERENCE BETWEEN THE HIGHER AND LOWER PRFS. IF JNAMBIGUOUS',/RA  

    *GE CALCULATIONS NOT DESIRED, ENTER -999.,)  

    READ(5,855)PRF(K)  

    855 FORMATT(14)  

    WRITE(5,660)K  

    660 FORMATT(1X,'IF YOU WANT TO ENTER ADDITIONAL RADAR SITES ENTER 1,OTHER  

    *WISE ENTERED 0,/, THE MAXIMUM NUMBER OF SITES ALLOWED IS 9 AND YOU  

    *AVE ENTERED ',I1,' SO FAR.,)  

    READ(5,860)ADD  

    860 FORMATT(11)  

    IF (ADD.NE.1.OR.K.GT.8) GO TO 2  

    K=K+1  

    GO TO 1  

    CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC  

    THIS IS THE END OF THE RADAR SITE INPUT LOOP. THE REST OF THE  

    C INPUT DATA APPLIES TO ALL SITES ENTERED BY THE USER.  

    CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC  

    2 WRITE(5,670)  

    670 FORMATT(1X,'INPUT STRIKE ALTITUDE IN FEET AGL RIGHT JUSTIFIED',IX,/M  

    *IN COLUMNS 1-4: INPUT -999 IF NO AGL MASKING FIGURES REQUIRED.,)  

    READ(5,870)FAGL  

    870 FORMATT(14)  

    WRITE(5,680)  

    680 FORMATT(1X,'INPUT STRIKE ALTITUDE IN FEET MSL RIGHT JUSTIFIED',IX,/M  

    *IN COLUMNS 1-5: INPUT -9999 IF NO MSL MASKING FIGURES REQUIRED.,)  

    READ(5,880)FMNL  

    880 FORMATT(15)  

    WRITE(5,690)

```



```

CCCCCCCCC SP=INTVL/3)*5
RE=6372815
RD=IRND(FLOAT(RE)/(1.0+(FLOAT(DNDH)*FLOAT(RE)+1.0 E-9)))
R=IRND(FLOAT(RE)*1.330321)
PI=2.0*ARSI/(1.0)
MSL=FLOAT(FMSL)/3.28084
AGL=FLOAT(FAGL)/3.28084
DNMAX=80
DMMAX=80
DO 11 DM=1, DMMAX
DO 12 DN=1, DMMAX
IADIS(DM,DN)=Z
IMDIS(DM,DN)=Z
CONTINUE
11 CONTINUE
12 CCCCCCCCC THE TOPOGRAPHIC DISPLAY IS CREATED BY LOOK
CCCCCCCCC IF DESIRED, THE TOPOGRAPHIC DISPLAY IS CREATED BY LOOK,
CCCCCCCCC IF(ILK.EG.) CALL LOOK(NMAX,MMAX,GWS,DLAT,DLOD,DISRES,SP),
CCCCCCCCC THE SITE NUMBER LOOP STARTS HERE AND IS INCREMENTED USING THE
C INDEX VARIABLE K. THE PRF FOR SITE K IS COMPUTED AS A FIRST STEP.
CCCCCCCCC THE MAXIMUM UNAMBIGUOUS RANGE (MUR) IS COMPUTED AS A FIRST STEP.
CCCCCCCCC DO 15 K=1,KMAX
IF (PRF(K).EQ.-99) PRF(K)=100
MUR=2.0*FLOAT(PRF(K))
CCCCCCCCC SITE *K IS LOCATED IN THE DATA BASE MATRIX IN LAT, LONG AND ALT.
CCCCCCCCC CALL LOCATE(EW(K),RLON(K),NS(K),RLAT(K),RHT(K),INTVL,DLOD,
*DLAT,I,J,MMAX,RHF(K),RMHF(K)),
CCCCCCCCC ELEVATION IS INTERPOLATED HERE
C SITE *K ELEVATION IS INTERPOLATED HERE
CCCCCCCCC I=INT(I)
JJ=INT(J)
DJ=I-I
DI=J-J
IF (II+1.GT.MMAX.OR.JJ+1.GT.NMAX) GO TO 13
HUL=L(II,JJ)
HLL=L(II+1,JJ)
HLR=L(II+1,JJ+1)
LIH=L(II+1,JJ+1)
*LL*(1.0-DJ)+FLOAT(HLR)*DJ)))+(DI*(FLOAT(H
MAS02410
MAS02420
MAS02430
MAS02440
MAS02450
MAS02460
MAS02470
MAS02480
MAS02490
MAS02500
MAS02510
MAS02520
MAS02530
MAS02540
MAS02550
MAS02560
MAS02570
MAS02580
MAS02590
MAS02600
MAS02610
MAS02620
MAS02630
MAS02640
MAS02650
MAS02660
MAS02670
MAS02680
MAS02690
MAS02700
MAS02710
MAS02720
MAS02730
MAS02740
MAS02750
MAS02760
MAS02770
MAS02780
MAS02790
MAS02800
MAS02810
MAS02820
MAS02830
MAS02840
MAS02850
MAS02860
MAS02870
MAS02880

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[illegible]



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76  CONTINUE
DO 78 DM=2, DNMAX
DO 79 DN=2, DNMAX
IF (IMDIS(DM,DN).EQ.Z)IMDIS(DM,DN)=X
CONTINUE
79  CONTINUE
80  CONTINUE(6,960)
WRITE(6,990)FMSL,DLAT,GNS,DLON,GWE,SP,RESLAT,RESLON,DNDH,DHF
FORMAT(18,'RADAR COVERAGE DISPLAY FOR STRIKE AT',I5,' FEET ABOVE
SEA LEVEL',I7,I5,'I, DISPLAY PARAMETERS',I7,I5,'SOUTHWEST CORNER
OF DISPLAY: LATITUDE=',I7,I5,'LONGITUDE=',I7,I5,'NMMAS04910
* SPACING=',I2,' MINUTES',I7,I5,'CELL RESOLUTION: LATITUDE=',I7,I5,'NMMAS04920
* 2IX, LONGITUDE=',I7,I5,'NM',I7,I5,'REFRACTIVE GRADIENT =',I4,I5,'MAS04930
* REFRACTIVE DUCT HEIGHT (FT) =',I5,I7,I5,'RADAR SITE PARAMETER SMAS04940
* //5X, SITE #',I4,'LATITUDE',I2X,'N/S',I4X,'LONGITUDE',I2X,'E/W',I4X,MAS04950
* ELEVATION (FEET)',I7,I5,'PRF',I7,I5,MAS04960
DO 991 K=1, KMAX
WRITE(6,991)K,RLAT(K),NS(K),RLON(K),EM(K),MHT(K),PRF(K)
991  CONTINUE
992  CONTINUE(6,992)
WRITE(6,992)I7,I5,'III. LEGEND',I7,I5,'#-NUMBERED RADAR SITE LOCATION',I7,I5,'
* 75X, #-ENVELOPE WITHIN WHICH AN AIRCRAFT FLYING AT',I7,I5,'THE SPECIMAS05010
* FIRED ALTITUDE WILL BE UNMASKED',I7,I5,'AND INSIDE THE RADAR MAXIMUM UMAS05020
* NAMBIGUOUS RANGE',I7,I5,'-AREAS WHERE TERRAIN ELEVATION EXCEEDS AMAS05030
* AIRCRAFT',I7,I5,'ALTITUDE',I7,I5,MAS05040
WRITE(6,960)
WRITE(6,980)(IMDIS(1,DN),DN=1, DNMAX),A
DO 80 DM=2, DNMAX
DO 81 DN=2, DNMAX
WRITE(6,980)(IMDIS(DM,DN),DN=1, DNMAX),B
80  CONTINUE
81  CONTINUE(6,980)A,(CHAR(DN),DN=1,79),A
CONTINUE
STOP
END

```



```

20      CONTINUE
30      CONTINUE
40      CONTINUE
50      CONTINUE
60      CONTINUE
70      CONTINUE
80      CONTINUE
90      CONTINUE
100     CONTINUE
110     CONTINUE
120     CONTINUE
130     CONTINUE
140     CONTINUE
150     CONTINUE
160     CONTINUE
170     CONTINUE
180     CONTINUE
190     CONTINUE
200     CONTINUE
210     CONTINUE
220     CONTINUE
230     CONTINUE
240     CONTINUE
250     CONTINUE
260     CONTINUE
270     CONTINUE
280     CONTINUE
290     CONTINUE
300     CONTINUE
310     CONTINUE
320     CONTINUE
330     CONTINUE
340     CONTINUE
350     CONTINUE
360     CONTINUE
370     CONTINUE
380     CONTINUE
390     CONTINUE
400     CONTINUE
410     CONTINUE
420     CONTINUE
430     CONTINUE
440     CONTINUE
450     CONTINUE
460     CONTINUE
470     CONTINUE
480     CONTINUE
490     CONTINUE
500     CONTINUE
510     CONTINUE
520     CONTINUE
530     CONTINUE
540     CONTINUE
550     CONTINUE
560     CONTINUE
570     CONTINUE
580     CONTINUE
590     CONTINUE
600     CONTINUE
610     CONTINUE
620     CONTINUE
630     CONTINUE
640     CONTINUE
650     CONTINUE
660     CONTINUE
670     CONTINUE
680     CONTINUE
690     CONTINUE
700     CONTINUE
710     CONTINUE
720     CONTINUE
730     CONTINUE
740     CONTINUE
750     CONTINUE
760     CONTINUE
770     CONTINUE
780     CONTINUE
790     CONTINUE
800     CONTINUE
810     CONTINUE
820     CONTINUE
830     CONTINUE
840     CONTINUE
850     CONTINUE
860     CONTINUE
870     CONTINUE
880     CONTINUE
890     CONTINUE
900     CONTINUE
910     CONTINUE
920     CONTINUE
930     CONTINUE
940     CONTINUE
950     CONTINUE
960     CONTINUE
970     CONTINUE
980     CONTINUE
990     CONTINUE
1000    CONTINUE

```

[illegible]



```

60      IF (RMHF.NE.-99) GO TO 70
          RMHT=5.0
          GO TO 80
70      RMHT=FLOAT(RMHF)/3.28084
80      CONTINUE
          RETURN
          END

```

```

LOC 00490
LOC 00500
LOC 00510
LOC 00520
LOC 00530
LOC 00540
LOC 00550

```



```

SUBROUTINE LATSCN MPPLON,MPPLAT,I,J,M,N,SH,ORIG,MAXV,R,NMAX,I,J,JJ,LAT000010
*DI RD OH
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
THIS IS THE CP AND THE SUBROUTINE. IT SCANS ALONG THE LINE OF SIGHT
ANGLE OF THE LINE OF SIGHT AT ALL INTERMEDIATE SAMPLE POINTS. THE
LARGEST OF THESE IS RETURNED TO THE MAIN PROGRAM AS MAXV.
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
VARIABLE LISTING: ONLY THOSE VARIABLES NOT CONTAINED IN THE MAIN
PROGRAM VARIABLE LISTING ARE EXPLAINED BELOW.
NAME TYPE FUNCTION
ALPH DP HALF ANGLE SUBTENDED BY GROUND DISTANCE BETWEEN THE
BETA DP SITE AND THE SAMPLE POINT. THE EQUIVALENT HEIGHTS
OF THE SITE AND THE SAMPLE POINT
C1 I BINARY INDICATOR, BASED ON CP QUADRANT
C2 I OPPOSITE OF C1.
D R GROUND DISTANCE BETWEEN TWO ADJACENT LINES. ONE M-
UNIT APART CONNECTED BY A LINE OF SLOPE SH
D1 DP DOUBLE PRECISION VALUE OF 1
D2 DP DOUBLE PRECISION VALUE OF 2.
DDK DP DOUBLE PRECISION VALUE OF .DK.
DEL K INCREMENTAL DISTANCE WHOSE MAGNITUDE IS .DI. AND
WHOSE SIGN DEPENDS ON THE CP QUADRANT
DIST DP EQUIVALENT FLAT EARTH DISTANCE FROM SITE TO SAMPLE
POINT
DK R GROUND DISTANCE FROM SITE TO SAMPLE POINT
DORIG DP DOUBLE PRECISION VALUE OF .ORIG.
DP1 DP DOUBLE PRECISION VALUE OF PI.
DR DP DOUBLE PRECISION VALUE OF .R.
DRD DP DOUBLE PRECISION VALUE OF .RD.
H1 DP EQUIVALENT FLAT EARTH ELEVATION OF RADAR SITE
H2 DP EQUIVALENT FLAT EARTH ELEVATION OF SAMPLE POINT
HT R INTERPOLATED ELEVATION VALUE OF SAMPLE POINT
K I INDEX VARIABLE USED IN SELECTING SAMPLE POINTS
KK I VARIABLE EQUAL IN MAGNITUDE TO .K. WITH SIGN
DEPENDENT ON CP QUADRANT
KMAX I MAX VALUE OF .K.
QL I ELEVATION VALUE OF DATA BASE ELEMENT IMMEDIATELY
WEST OF THE SAMPLE POINT
QR I ELEVATION VALUE OF DATA BASE ELEMENT IMMEDIATELY
EAST OF THE SAMPLE POINT
SV DP ELEVATION ANGLE BETWEEN THE SITE AND ANY SAMPLE
POINT MEASURED IN RADIAN FROM THE VERTICAL
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC

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[illegible]



```

SUBROUTINE LONSCN(MPPLON,MPPLAT,I,J,M,N,SH,CRIG,MAXV,R,MMAX,II,JJ,LON000010
*DJ,RD,DH)
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
THIS IS THE LONSCN: SUBROUTINE: IT HAS A LOGIC FLOW WHICH IS
IDENTICAL TO LATSCN: EXCEPT THAT IT SCANS THE MATRIX GENERALLY IN
AN EAST-WEEN DIRECTION, INSTEAD OF NORTH-SOUTH. DUE TO THE SIMILARI-
TIES BETWEEN THE TWO, LONSCN WILL NOT BE ANNOTATED. THE VARIABLE
LISTING IS ALSO OMITTED SINCE THE ONLY CHANGE IN VARIABLES IS THAT A
FEW OF THEM USE 'L' INSTEAD OF 'K' IN THE NAME.
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
INTEGER*2 L(400,400)
COMMON L
REAL MPPLON,MPPLAT,SH,D,DL,HT,I,J,DJ,DEL,ORIG,DH
DOUBLE PRECISION BETA,DDL,DH1,DORIG,D2,SV,MAXV,DR,DRD,ALPH
DOUBLE PRECISION D1,DPI,DIST,H1,H2
INTEGER M,N,K,LL,PU,PL,LMAX,C1,C2,I,J,JJ,R,RD
IF(I.NE.FLOPM)GO TO 10
D=MPPLON
GO TO 20
D= SORT(MPPLON**2+(SH*MPPLAT)**2)
LMAX=IABS(INT(FLOAT(N)-J))
IF(LMAX.LT.1) GO TO 40
IF(M-I1.GE.0) GO TO 20
C1=0
C2=1
GO TO 30
C1=1
C2=0
GO TO 40
K=1,LMAX
IF(N-JJ.LT.0)LL=K
IF(N-JJ.GE.0)LL=-K
IF(M-C1-INT(FLOAT(LL)*SH).GE.1.AND.M+C2-INT(FLOAT(LL)*SH).LE.MM
*AX) GO TO 35
IF(M-C1-INT(FLOAT(LL)*SH).GE.1) GO TO 31
HT=L(M+C2-INT(FLOAT(LL)*SH),N+LL)
GO TO 60
HT=L(M-C1-INT(FLOAT(LL)*SH),N+LL)
GO TO 60
PU=L(M-C1-INT(FLOAT(LL)*SH),N+LL)
PL=L(M+C2-INT(FLOAT(LL)*SH),N+LL)
IF(ABS((SH*FLOAT(LL))-FLOAT(INT(SH*FLOAT(LL))))).GT.1E-6) GO TO
*50
HT=(PU*C2)+(PL*C1)
GO TO 60
HT=FLOAT(C1*PL+C2*PU)-(((FLOAT(LL)*SH)-FLOAT(INT(FLOAT(LL)*SH))
)*FLOAT(PL-PU))
IF(LL.GT.0)DEL=DJ
IF(LL.LT.0)DEL=1.0-DJ

```

LON00490  
 LON00500  
 LON00510  
 LON00520  
 LON00530  
 LON00540  
 LON00550  
 LON00560  
 LON00570  
 LON00580  
 LON00590  
 LON00600  
 LON00610  
 LON00620  
 LON00630  
 LON00640  
 LON00650  
 LON00660  
 LON00670  
 LON00680  
 LON00690  
 LON00700  
 LON00710  
 LON00720

```

DL=D*(FLCAT(LMAX-K)+DEL)
IF(DL.LT.50.Q) GO TO 40
DDL=DL
D1=1.000
D2=2.000
DR=R
DRD=RD
DHT=HT
DP1=D2*DARSIN(D1)
DORIG=ORIG
IF(ORIG.GT.DM.OR.HI.GT.DH) GO TO 65
ALPH=DOL/(D2*DRD)
DIST=((D2*DRD)+DORIG+DHT)*DSIN(ALPH)
GO TO 70
ALPH=DDL/(D2*DR)
DIST=((D2*DR)+DORIG+DHT)*DSIN(ALPH)
H1=DORIG*DCOS(ALPH)
H2=DHT*DCOS(ALPH)
BETA=DATAN((H2-H1)/DIST)
SV=(CPI/C2)+BETA-ALPH
IF(SV.GE.MAXV) MAXV=SV
CONTINUE
RETURN
END
  
```

65

70

40

[illegible]













## LIST OF REFERENCES

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END

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